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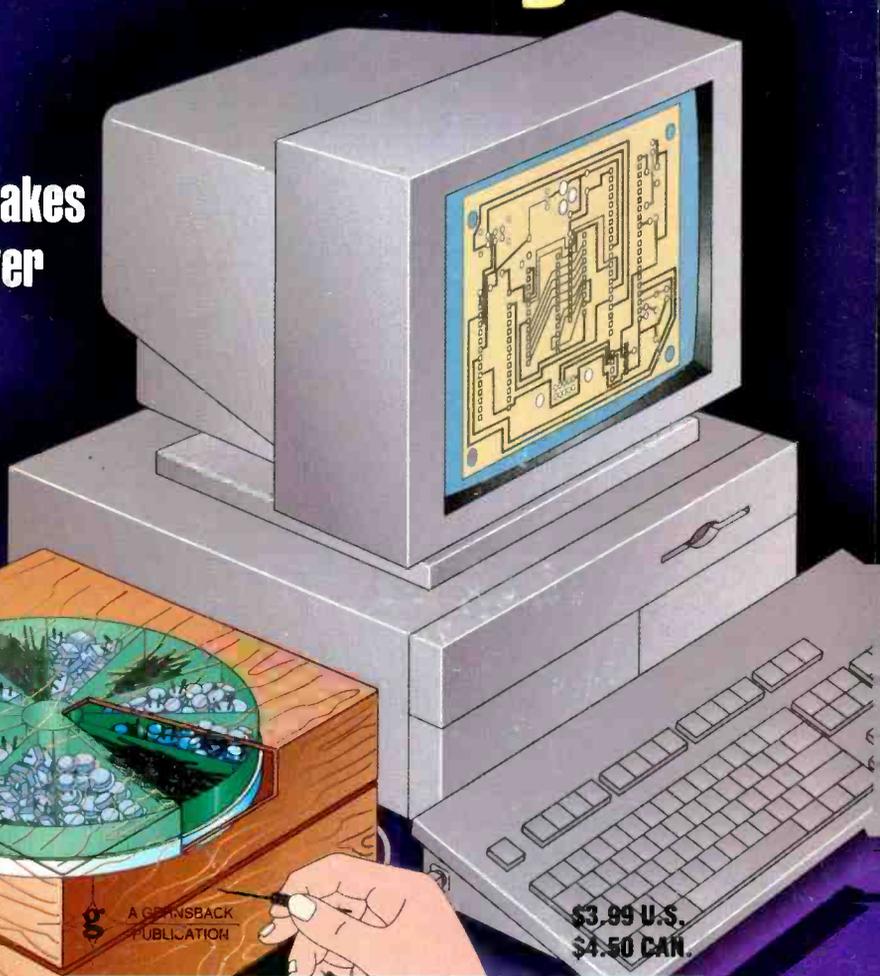
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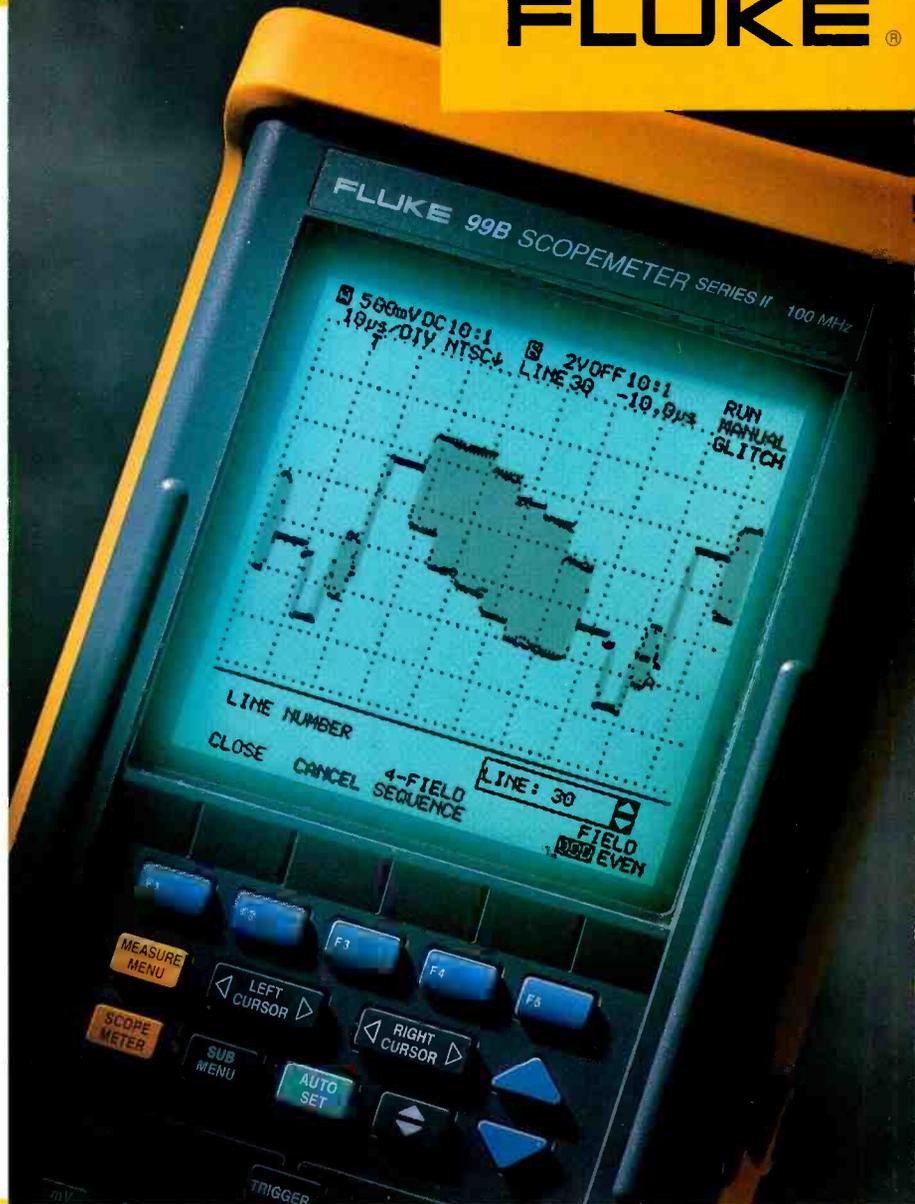
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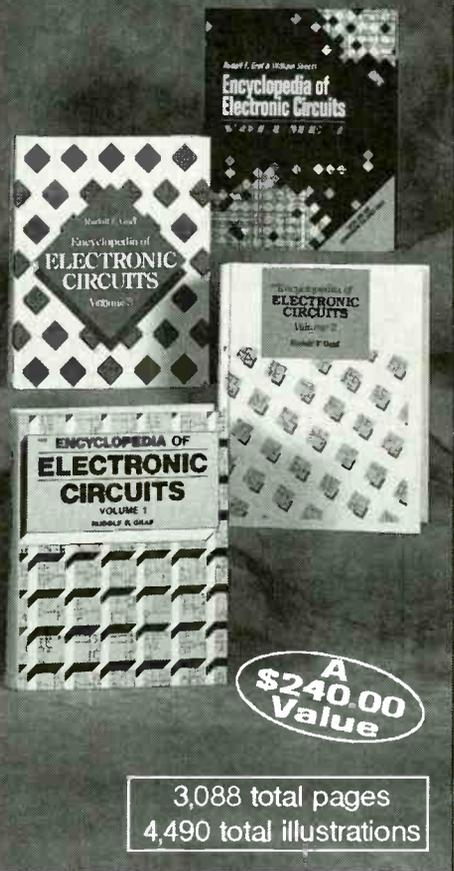
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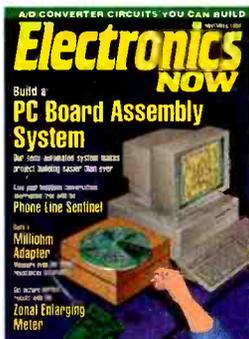
NOVEMBER 1996

ON THE COVER

33 BUILD THIS AUTOMATIC PARTS TRAY

The trend these days in industry is toward more and more automation. For example, in electronics, robotics is used to pick and place surface-mount components on printed-circuit boards with unerring accuracy. While such a level of automation is beyond the reach of almost any hobbyist, it is possible to bring some of its benefits to nearly any workbench. This month, we present the first part of a system that will, under computer control, greatly simplify the task of assembling PC boards. It is an automatic parts tray that brings to hand the next part to be mounted on the board. Coupled with a computer display that shows the location of that part on the board, project building may never be easier. Best of all, it is inexpensive to build and use.

— James J. Barbarello



BUILD THIS

40 MILLIOHM ADAPTER
Use it to accurately measure even the smallest resistance.
— Skip Campisi

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It is easier to use and gives better results than standard darkroom equipment.



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We put the finishing touches on this under-\$100 unit.
— Bob Kopski



53 PHONE LINE SENTINEL
Put an end to phone-call interruptions.
— Mordechai Saad

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The versatile 7107 A/D converter and display driver is a virtual voltmeter on a chip, but it can be used to do much more than just measure voltage, as you will see in this compendium of circuits that you can build and use.

— *Carl J. Bergquist*



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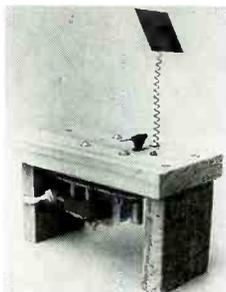
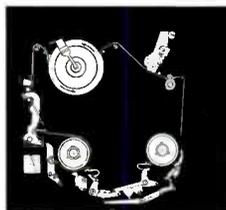
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EDITORIAL

Introducing www.gernsback.com

In my first editorial (September 1996), I mentioned that we were making our long awaited move onto the Internet. Well, that move is now largely complete and everyone here is extremely excited about it.

Our Web site, www.gernsback.com, hosts the home pages of both **Electronics Now** and our sister magazine, **Popular Electronics**. But there is also much more. By the time you read this, our FTP site will be up and running. There you will find all of the current and past story-related files for both titles.

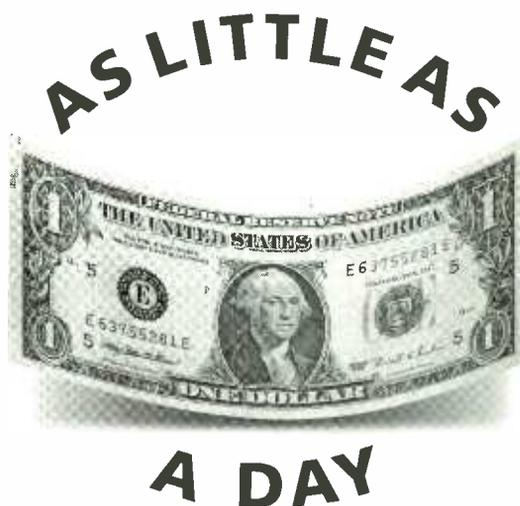
Also in the works is a searchable article index. Need to find out if or when we covered a specific topic? Just go to our site and you'll have your answer with just a few keystrokes. The system is undergoing testing now, and we hope to have it operational by early next year.

Also on the way are discussion forums. If you are looking for somewhere to discuss the pros and cons of a particular project, article, or issue, it's the place to go. You'll also be able to interact with other readers on just about any electronics-related topic.

Our Web site is also where you'll find late-breaking updates for our stories and projects. We, of course, publish significant corrections and updates as soon as we become aware of them. However, due to publishing schedules, it can sometimes take months for them to appear in print. Now, that information will be available to you almost as soon as we have it.

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Carl Laron
Editor



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VIDEO NEWS

WHAT'S NEW IN THE FAST-CHANGING VIDEO INDUSTRY

BY DAVID LACHENBRUCH

HDTV is on the Air

The first station to transmit digital high-definition TV is WRAL-HD, now broadcasting from Raleigh, North Carolina, on UHF Channel 23 under an experimental license from the FCC. That sister station of WRAL-TV mainly has been transmitting numbers for field measurements, but is sending full-bandwidth HDTV at its full authorized power of 100 kHz. The station plans to start transmitting actual video programs in the near future, using tapes provided by PBS and CBS. The station's executives have been talking with receiver manufacturers and are confident that HDTV sets will be in area stores by next spring.

Two more HDTV stations were due shortly at our deadline. The industry's model high-definition station, being financed by the Electronic Industries Association (EIA) and the Maximum Service Television trade association, was scheduled to take to the air soon at NBC's WRC-TV in Washington, D.C. Washington-based WETA, a PBS affiliate, is also building an HDTV counterpart, due on the air this year. The first HDTV receivers are expected to sell for more than \$2000.

Olympics in HDTV

At one time, the U.S. electronics and broadcasting community had planned to use the 1996 Summer Olympics in Atlanta as a showcase for American technology by broadcasting the games in HDTV. American HDTV slipped a cog as it wasn't quite ready. But the Olympics—390 hours of it—went on the air in HDTV anyway. It just wasn't American HDTV.

The Europeans and the Japanese collaborated to record 24 hours of Olympic competition daily in high definition.

Backed by a grant from the European Union, Germany's ZDF network covered the games in 1250-line high definition, while Japan's NHK used its 1125-line equipment.

ZDF's coverage was converted to 1125 lines and sent, along with NHK's coverage, by satellite to Japan, where it was broadcast using Japan's analog Hi-Vision system from satellite to homes. ZDF's coverage, along with the NHK signal, was also converted to a PALplus signal for transmission to Europe, where it was broadcast to virtually all European countries. PALplus is an improved-definition system that permits specially equipped widescreen TVs to show widescreen pictures with full definition, while other sets display the same widescreen image as a letterbox picture. The additional information required to bring the letterbox picture to 625-line quality is encoded digitally in the black area above and below the widescreen picture.

DBS Prices Falling

Prices of direct-to-home satellite equipment are falling rapidly, thanks to competition and subsidies by programmers. While the first digital satellite receivers for the DSS system—introduced under the RCA brand, using an 18-inch antenna—sold for \$600 and up, some prices are now as low as \$199. But there's a catch. The programming for these systems is available by subscription only. Obviously, those who install the equipment have to have programs. So the program providers increasingly are helping to subsidize equipment prices.

The first major move in that direction came from EchoStar, which was in a good position to undertake such a project because it sells both the programming and the hardware. It stunned its

competitors by offering a receiver and antenna for \$199 with the purchase of a year's programming at \$300. The promotion was so effective in test areas that it was offered nationwide last summer.

Not to be outdone, DSS, the biggest selling system, was planning a similar promotion. In it, DirecTV and U.S. Satellite Broadcasting, which supply programming for the DSS system, would give the equipment suppliers—including RCA, Sony, and Panasonic—a subsidy to bring the price down to \$399, and then send buyers a \$200 rebate in addition, effectively reducing the hardware price to \$199. While details have not been finalized at press time, the program should be in effect now, or starting soon, though perhaps in a somewhat different form.

The situation is reminiscent of what happened in the cellular-phone industry, where service providers are subsidizing phone instrument prices. The DBS competition hasn't yet gotten to the point where the receiver is free—but stay tuned.

WebTv Becomes Contagious

There is absolutely no evidence that combining the 1990's fad of Web browsing with the television fad begun in the 1950's is a workable idea, but profit-starved TV manufacturers and Silicon Valley entrepreneurs are joining forces to test the idea in a large-scale way.

Probably the most persuasive force in that direction is WebTV Network, which has signed Sony and Philips (Magnavox) to supply set-top boxes to let consumers surf the Internet on their large-screen TVs from their easy chairs. The box provides on-line access and e-mail service to TV users, and has a slot for smart-card financial transactions.

The box will cost somewhere between \$200 and \$400.

The box is connected to a phone jack and the TV's audio and video terminals. It contains a 33.6-kilobyte-per-second modem and a 64-bit Orion MIPS RISC microprocessor. WebTV features its own Internet guide and simple menus for navigation, along with parental-control software. Wireless and wired keyboards will be available as e-mail accessories, although mail can be authored using an on-screen depiction of a keyboard as well. Sony and Magnavox are expected to have the boxes in stores before year-end.

Other TV manufacturers are using different approaches. As reported here, Zenith is fielding a Net-browsing TV, but prefers the built-in approach to the separate set-top box. RCA's parent, Thomson Consumer Electronics, has been demonstrating prototypes of its "Genius Home Theater," which combines Internet access, e-mail, CD-ROM changer, and other computer features with a high-end 35-inch TV set. Thomson says that it might offer a simplified Web-browsing TV or attachment as well.



RCA'S "GENIUS THEATER" PROTOTYPE is one of a host of new PC/TVs.

Another TV manufacturer, Curtis Mathes, plans to introduce a combination computer and TV set. Computer manufacturer Gateway 2000 is already selling such a combination. Dubbed Destination, it includes a 31-inch TV set and an electronic program guide.

Actually, Toshiba probably foreshadowed the so-called "marriage" of PC and TV in 1994 with its "TIMM" (for Toshiba Integrated Multimedia Monitor), a 20-inch monitor and TV set designed for use both as a TV and a high-quality audio and video monitor for PCs. Unfortunately, it didn't sell particularly well.

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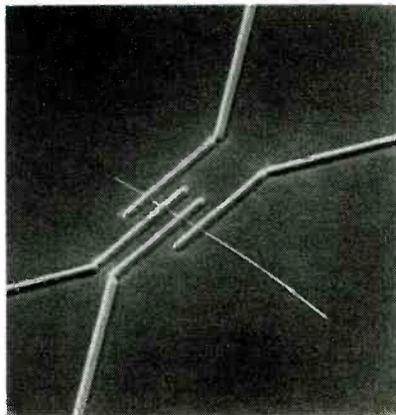
Measuring Individual Carbon Nanotubes

Researchers at NEC Corporation (Japan) and NEC Research Institute (Princeton, NJ) have succeeded in measuring electrical conductivity in individual carbon nanotubes. Using an evaluation method developed by scientists at NEC and Micrion Europe, they discovered that each nanotube has unique electronic properties, including both metallic and non-metallic behavior, and that the differences between nanotubes are far greater than expected. The results confirm that, at this scale, geometry and electronic properties are closely linked.

By attaching four 80-nanometer tungsten leads directly to individual nanotubes, and using a focused ion beam (FIB) system, the NEC scientists were able to achieve a more accurate and informative evaluation of the nanotubes' properties. It was learned that the current carrying capacity of nanotubes is extremely high, the temperature dependence of the conductivity greatly differs between nanotubes, different segments of a single nanotube do not always have the same temperature profile, and nanotubes have significant variation in resistivities.

The interest in carbon nanotubes has been stimulated by theoretical predictions that their electronic properties would be strongly modulated by small structural variations. In particular, the diameter and helicity of carbon atoms in the nanotube shell are believed to determine whether the nanotube is metallic or a semiconductor. Prior to the NEC method of measuring individual nanotubes, however, experimental evidence had been mainly linked to bulk measurements.

"This work opens up for the first time full electrical measurements on carbon nanotubes," said Dr. William Gear, president of NEC Research Institute. "These tubes may be able to function as



NEC RESEARCHERS MEASURE the electrical conductivity of individual carbon nanotubes by attaching four 80-nanometer-wide tungsten leads to each nanotube.

wires with a diameter about one hundredth the line-width used in current 16-megabit memory chips. Early results suggest that nanotubes can be fabricated with a very wide range of electrical properties.

Solar Success Story

Engineers from Sandia National Laboratories (Albuquerque, NM) played a key role in the development of Solar Two, a large pilot solar power plant that is capable of producing 10 megawatts of electricity—enough to supply power to 10,000 homes. The project was sponsored by the Solar Two Consortium, a group of ten organizations led by Southern California Edison Company, and the Department of Energy (DOE). At a June 5 dedication ceremony, presided over by DOE Secretary Hazel O'Leary, Solar Two was officially connected to the utility grid in Southern California.

Solar Two is unique in its use of molten salt to capture and store the sun's heat. The solar plant uses large, sun-tracking mirrors to concentrate sunlight on a receiver that sits atop a tower. The concentrated sunlight heats the molten

salt as it flows through the receiver. The hot liquefied salt is then piped away, stored, and used when needed to produce steam to drive a turbine/generator that produces electricity.

Solar Two's predecessor, Solar One, was a direct-steam solar generator that operated from 1982 to 1986. Solar One generated steam directly from water in its receiver, and was plagued by low energy-storage efficiency and interrupted operation from passing clouds. Solar Two, in contrast, can operate smoothly through intermittent clouds and continue generating electricity long into the night.

Sandia conducted large-scale experiments on the components needed in a molten-salt system at its Central Receiver Test Facility in Albuquerque. "Sandia played a key role in providing assistance by transferring molten-salt technology to the project, by leading the Technical Advisory Committee which oversaw all technical aspects of the project, and by supporting the design, construction, and startup of the plant through the outstanding efforts of its staff," said Gary Burch, director of the DOE's Thermal and Biomass Power Division.

IC Expo/96

Co-sponsored by Wescon, EE Times, Electronic Buyer's News, and OEM Magazine, IC Expo/96 is scheduled to take place as part of Wescon/96 on October 22-26, 1996, at the Anaheim Convention Center in Anaheim, California. The Wescon International Electronics Conference and Exhibition is a major OEM event for electronics, computer, and communications professionals.

The IC Expo/96 show-within-a-show, an extensive semiconductor trade exhibition, will celebrate the 25th anniversary of the microprocessor—and the 45th anniversary of Wescon—with a series of

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LETTERS

SEND YOUR COMMENTS TO THE EDITORS OF ELECTRONICS NOW MAGAZINE

L/C Meter Correction

In my article, "Build This Self-Calibrating L/C Meter" (*Electronics Now*, June 1996), I inadvertently submitted the incorrect schematic diagram. The schematic published was for an experimental unit that used a different display module and thus had different pinouts on the CPU-to-display interface. The PCB layout is correct, so any units built using a printed circuit board should be okay. This proves the saying, "To err is human, to really foul things up use a computer."

A copy of the correct schematic can be obtained by requesting it and sending a self-addressed, stamped envelope to the address below. The correct schematic is also available as `lcmsch.gif` on the Electronics Now BBS (516-293-2283).

NEIL HECKT

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New Product Correction

Thank you for mentioning HC Protek's D-980 digital Multimeter in the July "New Products" column. Unfortunately, two errors appeared. First, the DC accuracy specification was cited as 5%. The actual specification is 0.5%.

Our Web site URL was also incorrect. The correct URL is <http://www.techexpo.com/WWW/hcprotek>.

ROY TAFFARO

HC Protek Applications Engineer
Northvale, NJ

Non-Stereo Compressor

I would like to share my thoughts about the article, "Build a Stereo Compressor" (*Electronics Now*, August 1996). Although the two-channel compressor project will prove to be a fine addition to someone's audio-processing needs (Analog Devices makes great, innovative ICs), it is not a stereo compressor.

For the unit to operate in the stereo mode, both rectifier log converters from channels one and two would need to be summed into a single control voltage that would then feed directly to the VCAs of both channels in a strapped configuration, thereby preserving correct stereo imaging. By that I mean that any high-level peak appearing in only one channel will cause an equal amount of gain reduction in both channels, keeping the left/right balance correct.

Any two-channel processor, when connected to a stereo signal (*i.e.*, complete mix), would process the left and right channels independently. If a sudden loud signal appeared in only one channel, such as a lead instrument that was panned hard left or right within a total stereo mix, only that channel's VCA would respond, causing the overall level in that channel to decrease. That decrease in level to only one channel will cause image shifting. All mono information (bass drum, bass guitar, etc.) would sound off-center from the original mix.

As a two-channel compressor, I'm sure the unit will be a wonderful addition to an effects rack. As for stereo compressing a final mix, say from CD or DAT to a cassette format—no way!

RON TOZIER

Newton, KS

Laser Article Brought Into Focus

In reading the August installment of "Laser Experiments," I found what I

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Electronics Now Magazine,
500 Bi-County Blvd.,
Farmingdale, NY 11735

Due to the volume of mail we receive, not all letters can be answered personally. All letters are subject to editing for clarity and length.

believe to be several serious errors. First of all, a diffraction grating does not consist of thousands of very small parallel prisms per millimeter, as suggested. In actuality, a diffraction grating consists of many closely spaced parallel lines scored onto an aluminized plastic or polished glass surface. Those lines break up light into its component frequencies by the physical process of diffraction (the interference produced when light encounters an obstacle), as their name implies. Each scratch serves as a source of scattered light. Prisms operate through the entirely different process of refraction—the selective bending of different light wavelengths as they pass from one media (such as air) to another (such as glass). If gratings really operated as microscopic prisms as suggested, then they would have to be called refraction gratings!

Another type of grating consists of many parallel apertures or obstacles that ideally present a pass-block squarewave type pattern to the incident wave front. Yet another type (there are many), called a "blazed" grating, consists of grooves cut onto a glass surface whose serrated edges do resemble an array of prisms but which still operates by diffraction. Consult any standard physics or optics text for more details.

Another statement in the article suggested that the focusing of "light" is somehow more crisp and pronounced than that obtainable by other forms of electromagnetic energy such as "radio or sound." The big error here is that sound is *not* a form of electromagnetic energy. In addition, there is no fundamental difference between radio waves and visible light. They are both EM waves that differ only in their frequency. Radio waves are routinely focused by parabolic antennas and the like.

A further misconception was that placing black tapes around a bent glass rod would act as a shield to keep light from escaping out the sides. In reality,

the process called "Total Internal Reflection" is what keeps light trapped within the rod or optical fiber. To operate, the incident light rays must enter the rod at an angle less than some critical angle determined by the material of the rod or fiber and the surrounding medium. If the incident angle exceeds that value, or if the rod/fiber is bent too sharply, then light can indeed leave through the sides. However, black tape will not redirect the light back into the pipe or cause Total Internal Reflection to occur, as implied.

Several times in the article, the author mentioned that lasers are coherent and monochromatic, but still contain all the other colors in the visible spectrum (albeit in small quantities). Thus, the article continued, colored light can be produced by passing laser light through a prism or a frosted plastic sheet. While it is true that no laser is perfectly monochromatic (the frequency spectrum is predominantly distributed over a band known as the line width), its bandwidth is extraordinarily narrow. For a common He-Ne laser, the line width is roughly 1500 MHz, which might seem large compared to radio frequencies but is less than 1/1000 of

one percent of the visible light spectrum. Technically, all frequencies in that narrow band are of different "colors." But to suggest that a full-color spectrum can be obtained through refraction of laser light is nonsense. Lasers are called monochromatic or quasi-monochromatic for good reason. Any colors thus perceived are due to interactions with ambient sunlight or non-monochromatic room illumination.

The use of the word "sub-reflection" to describe the speckling effect produced by shining laser light off a diffuse surface is non-informative. The speckles are caused by a stationary interference pattern set up in the space in front of the surface. Due to the long coherence length of the laser light, individual reflections from the rough surface combine together coherently at each point in space with a random but stationary (non-changing) phase to create the speckles. When viewed in sunlight, the speckles might take on various colors.

While lenses are extremely important in optical science, the rules that govern the focusing of laser light (Gaussian beams) are not quite the same as those for non-coherent light. This

difference had disastrous consequences for some early designers of optical systems using lasers, who used the standard rules of geometrical optics and couldn't figure out why their systems failed to work! The interested reader can find a wealth of information on these topics in the many available books on lasers, optics, laser electronics, holography, and other related fields.

JAY RABKIN

Pasadena, CA

Audio System Integration Update

In "Audio Update" (*Electronics Now*, August 1996), Franklin Miller stated that it is optimum to match microphone impedance to the input impedance of the mixer. That is wrong. If the impedances are matched, the level will drop 6 dB and the signal-to-noise ratio will drop 3 dB. For condenser microphones with a built-in amplifier, there will be a bass roll-off and added distortion.

Instead, the input impedance should be at least ten times the source impedance. That mismatch is called a "bridging load."

DAVID HADAWAY

Rindge, NH

EN

WHAT'S NEWS

continued from page 8

industry events. Hundreds of exhibits will display many of today's most advanced microelectronics products and technologies by leading semiconductor manufacturers. Industry and editorial advisers have structured the event to meet the needs of technology professionals from the communications, computer, and high-end VLSI components industries, who need to know the latest in microprocessors, microcontrollers, memories, ASICs, and communications ICs.

The Applications Conference on Communications and Computer Technologies will provide extensive solutions-oriented presentations in a series of several one- and two-hour sessions. New and emerging technologies will be featured in multiple sessions throughout the conference.

Information about Wescon/96 and IC Expo/96 is available by phone (800-877-2668), fax (310-641-5117), e-mail (m.pothoff@ieee.org), and Web site (<http://www.wescon.com>).

Scholarship Donation

The Consumer Electronics Manufacturers Association (CEMA) announced that DeVry Institute has contributed \$60,000 in scholarships to the winners of the Electronics Products Servicing Competition, held June 27 at the 1996 Skills Championships in Kansas City, Missouri.

Throughout the year, students compete in local, regional, and state competitions sponsored by the Vocational Industrial Clubs of America (VICA). The competitions culminate in VICA's annual Skills USA Championships, which pit state title winners against each other. CEMA sponsors the electronic skills portion of the championships.

DeVry awarded scholarships to both the secondary and post-secondary winners of the electronics competition. Both scholarships, valued up to \$30,000, will cover full tuition to any of the DeVry Institutes in the United States. As a private, degree-granting higher-education system, DeVry, with 13 campuses throughout the United States and Canada, offers

bachelor's degree programs in electronics-engineering technology, computer-information systems, business operations, accounting, and telecommunications management, as well as an associate's degree program for electronics technicians.

"Consumer electronics manufacturers rely heavily on qualified technologists and technicians for the installation, servicing, and maintenance of their products," said Don Hatten, vice president, CEMA Product Services. "The generous DeVry scholarships will provide our two winners with a valuable education and an opportunity for promising careers once they graduate."

CEMA, through its Product Services Department, supports vocational education programs that offer training for those entering the servicing profession. CEMA also provides in-depth preparatory training for students seeking engineering degrees.

Information on CEMA is available via EIA/CEMA's World Wide Web Site at <http://www.eia.org/cema>. Information on DeVry programs can be accessed at <http://www.devry.com>.

EN

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PS-305 \$219.95, 0-30VDC, 0-5A

PS-305D \$399.95, dual, tracking
8110 \$289.95 0-60VDC, 0-3A
8112 \$399.95 0-60VDC, 0-5A
8108(8109) \$549.95(\$699.95) 0-60VDC, 0-3A(5A), dual, independent tracking, Low ripple
8102(8103) \$399.95(\$489.95) dual 0-30VDC/0-3A(5A), fixed 5VDC/3A, independent tracking operation, constant voltage and current, Slave/Master, Serial/Parallel connection.
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SM-6225B/C \$1999.95
 Freq Range: (AM)490KHz, (FM) 10-11.4MHz, Accuracy: ± 0.1%
 Marker: (AM)455KHz, ±5KHz, ±150KHz, (FM)10.7MHz, ±7.5KHz, ±150KHz

STEREO SCOPE OS-7505B \$369.00 trigger, 0-10MHz

ALIGNMENT SCOPE OS-7001A \$369.00 0-200KHz

AM/FM STD SIGNAL GEN.

SG-4110A \$1799.00
 Freq: 100KHz-110MHz
 Display: 6-digit LED
 Accuracy: ±(5x10-E5 ± 1 count)
 Resolution: 100Hz (100-34.99MHz), 1KHz (35MHz-110MHz)
 Output: -19dBm, -99dBu, 1dB steps, Impedance: 50Ω VSWR 1.2

NTSC TV COLOR BAR PAT. GEN.

CPC-1366A \$159.95
 VHF NTSC
 Freq.: 45.75, 175.25, 187.25 MHz
 RF Output: 10mV
 Impedance: 75 Ohm
 Video Output: BNC, 1Vp-p

SWR/RF POWER METER

310 \$89.95
 Freq Range: 1.8-150MHz
 RF Power: 0-4W/20W/200W
 SWR Measure: 1.0 - ∞, 4W min.
 Accuracy: 5%-10%, SO-239 plugs.
 Insertion Loss: 0.3dB

Input/Output Imp: 50Ω
320 \$89.95, 130-520MHz
330 \$119.95, 1.8-520MHz
SWR-3P \$26.95 1.7-150MHz,
 RF Power: 0.5-10W, 0.5W-100W
SWR-2P \$22.95, 1.7-30MHz, RF Power: 0.5-10W
mW RF Power Meter 340 \$219.00, 1.8-500MHz, 20mW - 2W

RF SIGNAL GENERATOR

SG-4160B \$124.95
 100KHz-150MHz up to 450MHz on 6 bands, 6 plug-in coils, 3rd harmonics, 6 ranges, AM modulation, RF Output: 100mVrms to 3-5MHz, Modulation: Int 1KHz AM, Ext. 50Hz-20KHz AM
 Audio Output: 1KHz, 1Vrms
 for internal & external signals. Specification see SG-4160B above.

SG-4162AD \$229.95, with Freq. Counter 1Hz-150MHz, 6 digits.

AUDIO GENERATOR

AG-2601A \$124.95
 10Hz-1MHz, 5 ranges;
 Output Level: sine wave 0-8Vrms, square 10Vp-p
 Output Impedance: 600 Ohm
 Distortion: <0.05% 500Hz-50KHz, <0.5% 50KHz-500KHz

AG-2603AD \$229.95, with Freq. Counter 1Hz-150MHz, 6 digits, for internal & external signals. Specification see AG-2601A above

FUNCTION GENERATOR

FG-2100A \$169.95
 0.2Hz-2MHz in 7 ranges, Sine, Square, Triangle, Pulse & Ramp
 Output: 5mVp-p-20Vp-p, 1% distortion.
 VCF 0-10V control freq to 1000:1

FG-2102AD \$229.95 generates signals same as FG-2100, 4-digit counter display, TTL & CMOS outputs, 30ppm ± 1 count accuracy
FG-2020B \$159.00 0.5Hz-500KHz, Sine, Square, Triangle.
(FG)2103 \$329.95, Digital sweep generator, 0.5Hz-5MHz in 7 ranges, Operating Mode: sweep, AM, gated burst, VCG.
 Freq. Counter: Int. 0.5Hz-5MHz, Ext. 5Hz-10MHz

FM STEREO MODULATOR

AG-2011A \$549.00
 RF SECTION:
 Carrier: 98MHz ± 2MHz,
 Output: 10mV, 1mV & 0.1mV
 COMPOSITE SIGNALS:
 Pilot: 19KHz ± 2Hz, 0.8Vrms
 INT. MODULATION: 400KHz, 1KHz ± 1%, 1Vrms, distortion < .5%, L-R Separation: >50dB
 EXT. MODULATION: Freq: 50Hz-15KHz
 L-R Separation: >45dB 100Hz-3KHz, >35dB 50Hz-15KHz

AC MILLIVOLT METER

MV-3100A \$159.95 wide band 5Hz-1MHz, 3 scales, mV, dB & dBm, 300μV-100V in 12 ranges, 10μV resolution, -70-40dB in 12 ranges, 0dB=1Vrms, 0dBm=0.775V, ±3% accuracy, Input impedance 10MΩ; Noise <2%; **MV-3201B \$309.95** dual channels, simultaneous measurement.

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 Vertical: 10mV/Div, Horizontal: 250mV/Div, 10Hz-100KHz in 4 ranges, 3 CRT: Internal and External Sync; Input 1MΩ/35pF
OS-7010A \$369.00 DC-10MHz
 5" CRT, 10mV/Cm-10V/Cm, 1MΩ
OS-622B \$344.95 20MHz/dual trace
OS-65J \$699.95 50MHz, dual, delay sweep, ALT trigger, TV syn
OS-6100B \$1329.95 100MHz, 4ch, 8 traces, delay sweep, best buy

GRID DIP METER

DM-4061 \$89.95 1.5-250MHz, 6 bands, 6 plug-in coils, 2 transistor, and 1 diode
 Modulation: 2KHz Sinewave, Crystal Oscillator: 1-15MHz
 Wave absorption meter Using 9VDC power supply

AUTO DISTORTION METER

DM-3104A \$799.95
 MEASUREMENT:
 Range: 0.01%-30%, 0.1/0.3/1/3/10/30% full scale.
 Freq: 400Hz±10%, 1000Hz±10%(HPF)
 Input: 3mV-100V, ratio measuring 20dB
 Auto Switching Ranges: Fundamental Freq. = (fo)±10%, Fund. Rejection: >80dB at (fo)±5%, >70dB at (fo)±10%, Harmonic Accuracy: ±0.5dB, 1R(fo)-20KHz
DM-3204 \$1,599.00 dual channels.

FREQUENCY COUNTER

FC-5250C \$119.95
 Freq Range: 10Hz-220MHz (HF)10Hz-20MHz (VHF)10MHz-200MHz
 Gate Time: 0.1 & 1sec
 Max. Input: 10Vp-p
 Input Sensitivity: 35mV 10Hz-200MHz Display: 7-digit LEDs
 Input Imped. (HF) 1M Ohm, (VHF) 50 Ohm

FC-5260A \$146.00
 10Hz-600MHz 7-digit LEDs
FC-5270 \$149.95
 10Hz-1.2GHz 8-digit LEDs
FC-5600B \$321.00
 10Hz-600MHz 10-digit LEDs
(FC)5700 \$329.95 10Hz-1.3GHz 10-digit LEDs

SIGNAL TRACER/INJECTOR

SE-6100 \$134.95
 TRACER: Gain Max 60dB
 Attenuation: 0/20/40/60dB
 Input Imped. 100K Ohm
 Output Imped. 600 Ohm
 Speaker: 8 Ohm
 INJECTOR: Freq: 1KHz
 Squarewave; Output Level: Continuously variable 0-4.5Vp-p

AUTO. CAPACITANCE METER

CM3300A \$139.00 10 ranges, 99.9pF - 99.9mF, fully automatic
 Resolution: 0.1pF lowest, 0.1% full scale.
 Accuracy: 0.5% of full scale ± 1 digit to 99.9μF, 1% of full scale ± 1 digit to 99.9μF
 Display: 3 digit LED
 Unit indicator: pF, nF, μF, mF. Overrange indicator.

WOW-FLUTTER METER

WF-3103A \$699.95
 Freq Range: 3KHz±10% JIS/CCIR, 3.15KHz±10% DIN.
 Range: 0.03/1/3/3% full scale.
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WF-3105A \$799.95, digital.
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EDS-8804 \$89.00 A/D and D/A converters.
EDS-8805 \$239.00 Servo and stepper motors.
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Electronic UHF Attenuator 085E (087E) \$399.00, DC-950MHz, Imp: 50(75)Ω, 1dB step.

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MT810 \$129, Hand held model, Power: 9VDC.

Q & A

READERS QUESTIONS, EDITORS ANSWERS

Electronic Dog Whistle

Q I would like to build a transmitter that emits a sound that only dogs can hear. It needs to be able to transmit approximately 100 to 150 yards. - J.S., Duluth, GA.

A Try the circuit in Fig. 1; it's an audio oscillator that adjusts from about 6 kHz to 25 kHz. The speaker is a piezo-electric tweeter; ordinary speakers aren't very efficient at those frequencies.

To check the oscillator, set R2 to its maximum resistance; you'll hear a loud squeal. Then adjust R2 to put the frequency above the range of human hearing. Use a pushbutton switch and train the dog to recognize a distinctive series of ultrasonic beeps.

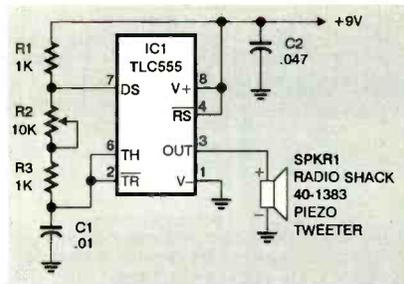


FIG. 1—THIS OSCILLATOR emits a tone that can be varied between 6 and 25 kHz. The higher frequencies can not be heard by most humans, although dogs can hear it just fine.

comparable to its weight in pounds.

Car batteries aren't rated in amp-hours because their total capacity isn't especially important; in fact they're designed never to be deeply discharged. What matters in a car battery is the total number of amps that it can deliver in cold weather ("cold cranking amps"), even though if you kept drawing current at that rate, the battery would go dead in just a couple of minutes.

What's an Amp-Hour?

Q Can you please explain to me the meaning of amp-hours, and how they are figured in reference to a car battery? — B. M. Huntsville, TX.

A Certainly. The amount of energy you can get out of a battery depends on its voltage (which is fixed), the number of amps that the load draws, and the number of hours before the battery runs down. Multiply the amps by the hours and you get amp-hours.

For example, a battery that can supply 3 amps for 4 hours has a capacity of 12 amp-hours ($3 \times 4 = 12$). The same battery could supply 1 amp for 12 hours, or 12 amps for 1 hour, or 2 amps for 6 hours, and so on.

To give you some realistic numbers, an alkaline D cell is good for about 10 amp-hours (which is actually quite impressive considering its small size). An alkaline 9-volt battery is only good for 0.4 amp-hour, but that's enough to power a 50-mA (0.05-amp) transistor radio for 8 hours. And here's a handy rule of thumb: The amp-hour capacity of a 12-volt lead-acid battery is roughly

NiCd Charging

Q I have seen a number of NiCd charger circuits like the one in Fig. 2. Are the values shown appropriate to charge the battery in 6 to 7 hours. If there is a rule of thumb to follow, it would be appreciated. — P. S. M., Eaton, IN.

A The charging current for an NiCd battery depends on its capacity in amp-hours (see the previous question) and how quickly you want it charged.

The old standard is to charge for 12 to 14 hours at a current of $C/10$ amps, where C is the capacity in amp-hours. For example, a 1.2-AH battery gets a charging current of 0.12 amp.

To charge a battery in 6 or 7 hours, you'll want to use twice as much current, i.e., $C/5$. That's about as fast as you can go without using special circuits to monitor the battery voltage and/or temperature.

Since you asked for a rule of thumb, we'll do an approximate calculation; greater precision would gain us nothing because there is so much variation between NiCd batteries.

For good current regulation, the AC voltage should be at least twice that of the battery. The resistance depends on the voltage drop, but since the current is only flowing half the time, the resistance should be only half the value given by Ohm's Law.

Here's a concrete example. Suppose you're charging a 7.2-volt, 1200-mAH (1.2-AH) battery pack from a source of 18 volts AC, and you want to charge in 6 to 7 hours at $C/5$. First, find the average charging current:

$$I = C/5 = 1.2/5 = 0.24 \text{ ampere}$$

Next, the resistance, using $R = E/I$ and then halving it:

$$R = 0.5 \times E/I = 0.5 \times (18 - 7.2)/0.24 = 22.5 \text{ ohms}$$

Finally, the resistor dissipation is found using $P = I^2 R$ with the average charging current:

$$P = I^2 R = (0.24)^2 \times 22.5 = 1.3 \text{ watts}$$

So a 22-ohm, 2-watt resistor will do the job just fine. You'll find that batteries of different voltages (such as 7.2 and 9.6 V) can often be charged in the same charger as long as their amp-hour ratings are similar. Also, you can charge a higher-

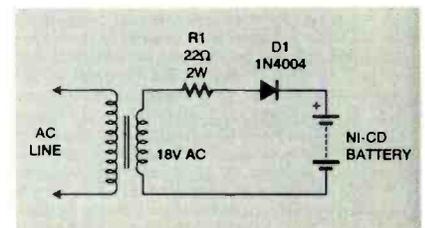


FIG. 2—WHILE THERE ARE many different NiCd-battery charger circuits, a simple resistor/diode combination like this one will do the job.

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November 1996, Electronics Now

amp-hour battery in a charger designed for batteries of lower capacity by prolonging the charging time.

Purists will no doubt note that we've ignored the diode voltage drop and the difference between RMS and average current. For all practical intents and purposes, they have no effect in this application.

NiCd Zapping

Q I have several non-functioning NiCd battery packs. I've found several battery zappers in Rudolf Graf's Encyclopedia of Electronic Circuits, but the circuits show widely varying zapping voltages and currents. How do I determine what voltage and current I need to use for this? — G. A. H., Santa Fe, NM.

A Unfortunately, NiCd zapping is not an exact science. In fact, manufacturers don't recommend it at all, because it never leaves a battery as good as new. But we all know that it works and can often enable you to get several more weeks' or months' use out of an otherwise defunct battery.

The purpose of zapping is to clear an internal short circuit by burning away small crystalline structures that have formed inside a cell. There are many different techniques. One method is to charge a 1000- μ F capacitor to about 12 volts, then apply it briefly to the battery terminals. Another is to charge the battery briefly with heavy current (2 or 3 amps) while watching the terminal voltage; chances are it will come up to normal after half a minute or so. Make sure the current is indeed limited to 3 amps, since higher currents can make the battery explode.

All of those techniques are hit-or-miss, and the battery usually develops the same problem again in a short time. But there's no harm in trying. If possible, you should open up the battery pack to test and "zap" the individual cells. Be aware that some battery packs contain fuses that can be blown by the zapping process.

Video In Dim Light

Q I have a Sony 8mm camcorder and would like to be able to shoot video in low-light and extremely-low-light situations. Of course a video light will work up

HOW TO GET INFORMATION ABOUT ELECTRONICS

Books: Several good introductory electronics books are available at RadioShack, including one on building power supplies.

An excellent general electronics textbook is *The Art of Electronics*, by Paul Horowitz and Winfield Hill, available from the publisher (Cambridge University Press, Tel: 800-872-7423) or on special order through any bookstore. Its 1125 pages are full of information on how to build working circuits, with a minimum of mathematics.

Also indispensable is *The ARRL Handbook for Radio Amateurs*, comprising 1000 pages of theory, radio circuits, and ready-to-build projects, available from the American Radio Relay League, Newington, CT 06111, and from ham radio equipment dealers.

Copies of past articles: Copies of past articles in *Electronics Now* and *Popular Electronics* (post 1991 only) are available from Claggk, Inc., Reprint Department, P.O. Box 4099, Farmingdale, NY 11735 (Tel. 516-293-3751).

Electronics Now and many other magazines are indexed in the *Reader's Guide to Periodical Literature*, available at your public library. Copies of articles in other magazines can be obtained through your public library's interlibrary loan service; expect to pay about 30 cents a page.

Service manuals: Manuals for radios, TVs, VCRs, audio equipment, and some computers are available from Howard W. Sams & Co., Indianapolis, IN 46214 (Tel: 800-428-7267). The free Sams catalog also lists addresses of manufacturers and parts dealers. Even if an item isn't listed in the catalog, it pays to call Sams; they may have a schematic on file which they can copy for you.

Manuals for older test equipment and ham radio gear are available from Hi Manuals, PO Box 802, Council Bluffs, IA

to a certain distance, but what about objects farther away? Is there some kind of adapter that can be mounted on the camcorder to provide daytime range at night? — M. M., Denver, CO.

A You're probably thinking about image-intensifier tubes, which are photoelectric devices that amplify a faint image. These are used in military night-vision binoculars and other instruments.

51502, and Manuals Plus, Box 637, Spanaway, WA 98387.

Replacement transistors, ICs, and other semiconductors: Replacement components for a wide variety of popular devices is marketed by Philips ECG, NTE, and Thomson (SK) and are available through most parts dealers (including RadioShack on special order). The ECG, NTE, and SK lines contain a few hundred parts that substitute for many thousands of others; a directory (supplied as a large book and on diskette) tells you which one to use. NTE numbers usually match ECG; SK numbers are different.

Remember that the "2S" in a Japanese type number is usually omitted; therefore, a transistor marked D945 is actually a 2SD945.

Hamfests (swap meets) and local organizations: These can be located by writing to the American Radio Relay League (Newington, CT 06111; <http://www.arrl.org>). A hamfest is an excellent place to pick up used test equipment, older parts, and other items at bargain prices, as well as to meet your fellow electronics enthusiasts both amateur and professional.

Internet: On the Internet, electronics is discussed in Usenet newsgroups such as *sci.electronics.repair*, *sci.electronics.components*, *sci.electronics.design*, and *rec.radio.amateur.homebrew*. "For sale" messages are permitted only in *rec.radio.swap* and *misc.industry.electronics.marketplace*.

Many electronic-component manufacturers now have web pages; see the directory at <http://www.hitex.com/chipdir/>, or try addresses such as <http://www.ti.com> and <http://www.motorola.com> (substituting any company's name or abbreviation as appropriate). Many IC data sheets can be viewed online.

Image tubes and instruments that use them are available from STANO Components, Inc., PO Box 2048, Carson City, NV 89702 (Tel: 702-246-5281, Internet: <http://www.stano.night-vision.com>). You'll need a complete night vision scope with optics to form a viewable image, not just the tube alone; then you can aim the camcorder into the instrument instead of your eye.

continued on page 28

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EQUIPMENT REPORTS

A PC-BASED BLOOD-PRESSURE MONITOR FROM PULSE METRIC.

Monitoring and recording blood pressure is easy with the DynaPulse.

CIRCLE 15 ON FREE INFORMATION CARD



It seems that people are becoming more and more aware of their own personal health. We're all more concerned today about what we eat, what we're exposed to, and so on. One aspect of that is an increased awareness of our cardiovascular health.

While the best way to monitor that is to make sure you visit your doctor regularly, in our hectic schedules, sometimes that gets put off longer than it should. To keep an eye on such things as pulse and blood pressure, some people have their own equipment. But even so, you have to be careful in taking measurements and then have to record the statistics.

The newest, easiest way to take and keep track of those measurements is to use Pulse Metric, Inc.'s (6190 Cornerstone Court East, Suite 103, San Diego, CA 92121; Tel: 619-546-9461, 800-927-8573) DynaPulse 200M, which is computer-controlled and keeps track of the records for you. The 200M monitor unit is housed in an attractive plastic enclosure that connects to a PC or Mac computer. You need DOS 3.3 or higher, Windows 3.0 or higher, or Macintosh System 6.0.7 or higher.

The kit comes with an inflatable, adult-sized cuff and inflation bulb that plugs into the side of the monitor. Different-sized arm cuffs—child-size and oversize—are optionally available. The monitor connects to the computer via a serial cable. Software then converts your computer screen into a cardiovascular laboratory. We tested DynaPulse on a

PC running Windows 95 and it couldn't have been easier to use. We were busy taking readings, printing charts, and storing records within minutes of installing the software.

About Blood Pressure

The pressure of the blood flowing through the arteries is known, obviously enough, as blood pressure, which varies as the heart beats. When the heart pushes blood out from the heart, the pressure increases, and the *systolic* or maximum blood pressure is achieved. When the heart relaxes, the pressure in the artery decreases, and the *diastolic* or minimum pressure is reached. The average pressure throughout the pulse cycle is called the Mean Arterial Pressure (MAP). The units of measurement for blood pressure are millimeters (mm) of mercury, or Hg. Systolic blood pressure is given first followed by the diastolic blood pressure, or systolic/diastolic in mmHg. Normal blood pressure typically has a high from about 130 to 139 and a low from 85 to 89.

In healthy human beings, blood pressure can increase temporarily during stressful activities, including drinking coffee and smoking, but will return to normal when the activity ceases. However, when it stays high over a long period of time, a person is said to have high blood pressure, or *hypertension*.

Unfortunately, you have to actually measure your blood pressure to know if it's normal or high. There's no other way to know if a problem exists—until it is too late.

Using the DynaPulse

The DynaPulse 200M is the perfect way to keep track of your blood pressure, your whole family's blood pressure, or even all of your customers' blood pressures if you happen to be a pharmacist or something similar. Note however, that we're only saying "keep track of" blood pressure, and nothing about interpreting it. Unless you are a doctor, you always have to consult one. A doctor is the only person qualified enough to interpret blood pressure and pulse-rate readings.

You can buy the DynaPulse 200M in one of three versions. The clinical version, \$499, is designed for hypertension screening in clinical environments with the ability to store a virtually unlimited patient database, trend and statistical analysis, histogram display, pulse-waveform analysis, and a physician's reference. The educational version, priced at \$295, is designed for teaching and comes complete with curriculum and lab material. A home version, which costs \$179, is simpler and can keep track of up to six people.

We found DynaPulse very easy to use. The software installed without a hitch, and we connected it to the COM1 port on a PC (software settings allow for operation on any available com port). There isn't even an on/off switch on the 200M, as software activates the unit when necessary. An inflatable cuff—just like your doctor's—wraps around your arm and secures with Velcro. A squeeze bulb with a relief valve inflates the cuff. But instead of having the output pressure tube connected to a mercury-filled instrument, it plugs into the DynaPulse monitor, which contains a semiconductor pressure sensor. The monitor, which is powered by four AAA batteries, converts the input pressure readings from the arm cuff into an RS-232 signal that your PC can understand.

When you use the DynaPulse, you can immediately begin measuring blood

continued on page 73

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Independent study is not for everyone. But, if you have the desire, the basic intellect and the motivation to succeed, CIE can make it happen. Our learning program is patented and each lesson is designed for independent study while our instructors are available to assist you whenever you feel you need help. In fact, CIE's curriculum is so well respected many Fortune 1000 companies utilize it for their own employees.



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uncanny... *Employers are looking for qualified applicants to hire and having a hard time finding them.*

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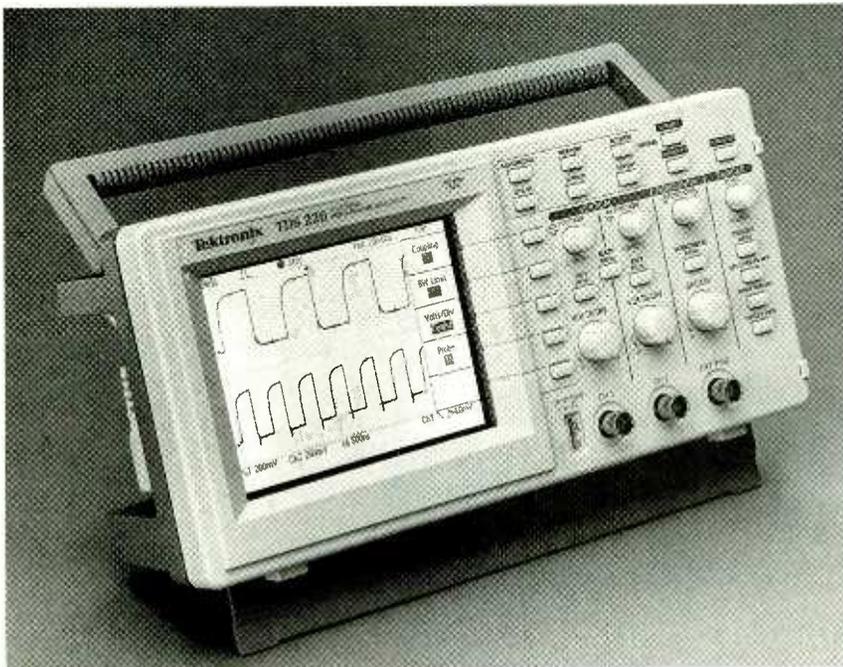
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Digital Real-Time Oscilloscopes

THE TDS 200 SERIES OF DIGITAL real-time (DRT) oscilloscopes from Tektronix cost about half the price of existing entry-level digital scopes and offer a combination of features that will

maintain full contrast at all sweep speeds and gain settings. Any signal that triggers the scope will be clearly visible on screen.

The TDS 200 series relies on Tektronix DRT oversampling technology to



CIRCLE 20 ON FREE INFORMATION CARD

overcome customers' objections to making the switch from analog to digital scopes. Designed for manufacturing, education, and service applications, the 60-MHz TDS 210 and the 100-MHz TDS 220 are priced competitively with similarly equipped analog scopes. They also offer superior measurement capability, analog-like controls and operating modes, and compact size—about one-fourth the size of other benchtop oscilloscopes.

One reason for that compact size is that both units in the TDS 200 series feature a bright, high-contrast, liquid-crystal display with a wide viewing angle. Unlike analog scope displays, the LCD main-

provide excellent waveform quality, update rate, and stability. Both models sample at 1 GS/s—at least ten times their bandwidth—which allows users to capture signal details invisible on analog scopes. Pre-programmed automatic measurements enable users to quickly quantify waveforms: period, frequency, cycle RMS, mean, and peak-to-peak. Other productivity features include automatic setups (similar to autoranging in a digital multimeter), stored reference waveforms, and stored front-panel setups that are not lost when the power is turned off.

The user interface looks and feels "analog," bringing back many of the

front-panel knobs that are familiar to analog-scope users. Routine functions such as gain, sweep speed, and vertical/horizontal positioning, are immediately accessible and respond like analog-scope controls. Automated digital functions are controlled by a simplified on-screen menu system, available in ten user-selectable languages.

The TDS 210 and TDS 220 carry suggested U.S. list prices of \$995 and \$1695, respectively.

TEKTRONIX, INC.

P.O. Box 500

Beaverton, OR 97077-0001

Tel: 1-800-479-4490, action code 317

DSP Filter

MFJ Enterprises' MFJ-781 DSP filter will add "brick wall" DSP filtering to any TNC or multimode data controller, allowing you to copy signals buried in noise and QRM—signals you can't even hear. The device will improve all modes on any model TNC, and it will give you an array of 100 sharp *No*Ring* linear-phase FIR filters. You can choose 20 filters to include on the front-panel switch for easy, one-knob selection.

The MFJ-781 plugs between your transceiver and multimode. It features input and output level controls and an accurate, easy-to-use input level indicator. Automatic gain control helps keep your audio level constant during signal fade. The on/off/bypass switch provides a true bypass.



CIRCLE 21 ON FREE INFORMATION CARD

Under severe QRM, the filter will greatly improve copy of packet, AMTOR, PACTOR, GTOR, Clover, RTTY, SSTV, WeFAX, Fax, CW, and just about any other digital mode. You can choose from 64 data filters with 16 mark/space pairs, four shifts, and four baud rates. Interference is 40-dB down, 60-Hz outsize passband. You also get 32 CW filters with eight CW tones (300-1000 Hz) and four bandwidths (50-500 Hz). Four customized filters are optimized for VHF packet, Clover, WeFAX, and SSTV.

The MFJ-781 DSP filter has a suggested retail price of \$129.95. For MFJ-1278B's, order the MFJ-780 plug-in DSP filter, priced at \$99.95.

MFJ ENTERPRISES, INC.

P. O. Box 494

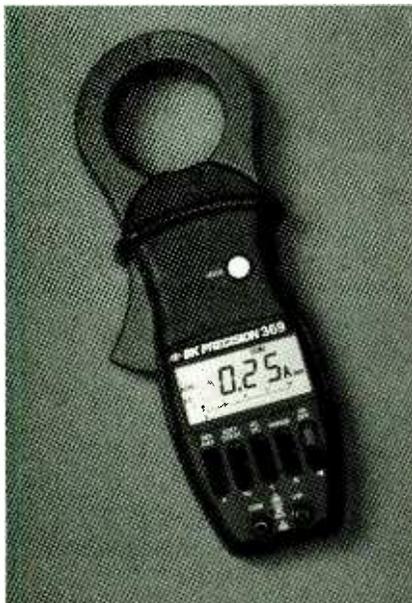
Mississippi State, MS 39762

Tel: 601-323-5869 or 1-800-6477-TECH

Fax: 601-323-6551 or 1-800-647-1800

True-RMS Clamp Meter

Electrical contractors, plant-maintenance engineers, electricians, and utility technicians will find B+K Precision's Model 369 multifunction clamp meter to be convenient and useful for measuring high electrical currents without direct electrical contact. The handheld instrument measures true-RMS AC current to 700 amps from 45 Hz to 1 kHz, and DC current to 700 amps with 2% accuracy. AC and



CIRCLE 22 ON FREE INFORMATION CARD

DC voltage can be measured to 750 volts with 1% accuracy, using test leads. The clamp can be used to measure resistance from 0.1 to 4000 ohms and frequency from 0.1 Hz to 10,000 Hz with 0.2% accuracy.

The Model 369 can also measure instantaneous AC amperes using its crest mode, which can log peak currents as high as 1000 amps. Data hold instantly freezes the displayed reading. Continuity check sounds a tone to verify an unbroken electrical path. Min-Max mode logs a running record of minimum, maximum, and average values.

The meter accepts conductors up to two inches in diameter. Its large, 4000-count LCD readout includes a 41-segment bar graph for peaking, nulling, and easy identification of varying signals.

The Model 369 clamp-on meter, complete with battery, clip-on carrying case, test leads, and manual, costs \$199.

B+K PRECISION

6470 West Cortland Street

Chicago, IL 60635

Tel: 1-800-462-9832

Fax: 312-794-9740

Four-Piece Inspection Light

Specifically designed for the field technician, Moody's Acu-Min Inspection Light allows light to shine on hard-to-



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reach areas. The set contains a flashlight, a straight conducting rod, a curved con-

ducting rod, and a mirror. The straight rod conducts the battery-powered xenon light down straight passages. The curved rod conducts light around corners to reach areas not normally visible. The small mirror fits snugly on both conducting rods to expand the user's field of view. The set comes packaged in a vinyl pouch.

The Acu-Min Inspection Light (stock #58-0235) costs \$42.95.

MOODY TOOLS, INC.

42-60 Crompton Avenue

East Greenwich, RI 02818-0230

Tel: 1-800-TOOL-INC

Fax: 401-885-4565

Memory Tester

Aristo Computers' SIMCHECK II is a third-generation, state-of-the-art memory tester. With a fast 486 processor and sophisticated time-delay circuitry, the tester allows users to accurately test today's—and tomorrow's—large memory devices. The stand-alone, portable unit tests both 72-pin and 30-pin SIMM modules in sizes up to 4Gx40 with a 96-pin expansion slot for future add-on companion testers. The SIMCHECK II measures RAS and CAS access time at 1-ns resolution. It includes a generic interface for the Automatic Handler, parallel printer, and other devices. The fully automatic test program allows non-technical personnel to operate the tester with the push of a single button, yet



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still allows engineers to set up complex custom tests.

The SIMCHECK II has a retail price of \$2495.

ARISTO COMPUTERS INC.

6700 SW 105th Avenue, Suite 300

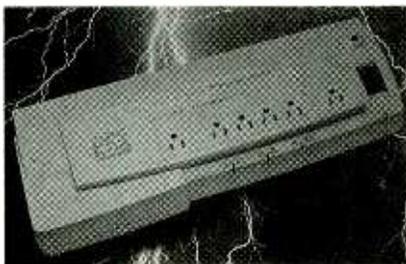
Beaverton, WA 97008

Tel: 1-800-3ARISTO or 503-626-6333

Fax: 503-626-6492

Workstation Surge Protection

The Back-UPS Office from American Power Conversion is a multipath power device intended to combat hardware damage caused by surges and prevent data loss from brownouts and blackouts. The device offers multi-outlet surge protection, phone line protection for on-line users, network data-line protection for corporate workstations, and battery backup for CPUs. Aimed at the small-office/home-office (SOHO) market, and backed by a \$25,000 equipment-protection guarantee, the device protects against all power problems on all power paths to a computer and peripherals including printers, scanners, external tape drives, and fax machines.



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The Back-UPS Office offers six outlets, all with surge-suppression and EMI/RFI filtering, and three of them also provide battery power for data protection. The device provides 7 to 13 minutes of battery backup during a power disruption, allowing the user plenty of time to shut down the system in an orderly manner. Modem protection safeguards users' Internet access and prevents PC damage from surges and spikes entering through the "back door." An indicator lets the user know when a new battery is needed. A site-wiring fault indicator detects wiring problems in the building that could cause potential fire hazards. Unique "BlockSafe" outlet spacing allows transformer blocks to be used without sacrificing other outlets.

The Back-UPS Office surge protector costs \$179.

AMERICAN POWER CONVERSION

P. O. Box 278
132 Fairgrounds Road
West Kingston, RI 02892
Tel: 1-800-877-4080
Fax: 401-789-3710

Web site: <http://www.apcc.com>

900-MHz Cordless Phone

Sanyo's Model CLT-986 900-MHz, digital spread-spectrum cordless telephone features a call-management caller-ID system, AC power-failure protection, and—for those who need still more freedom than that afforded by mere cordless phones—a "Speak Station" handset speakerphone for hands-free communication. The 900-MHz direct-sequence, spread-spectrum technology extends the transmission range and virtually eliminates interference. The digital technology also makes it difficult for eavesdroppers to tap into the signal.



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AC power-failure protection allows the CLT-986 to be used even during interruptions in the supplied line power. The back-up battery pack, built into the base of the unit, uses four "AA" alkaline batteries. The speakerphone handset also provides two-way paging. Sanyo's call management system is intended for use with the Caller ID service provided by local phone companies. With a recorded log of up to 20 calls, the system maintains a list of caller names with bi-lingual prompts, call times, dates, and last call received, with area-code editing capability. A 16-digit, two-line LCD readout on the handset allows the user to scroll through recorded data. Other features include one-hour quick charge, dual keypad operation, and 20-number memory.

The CLT-986 cordless telephone has a suggested retail price of \$349.99.

SANYO

21350 Lassen Street
Chatsworth, CA 91311-2329

Tel: 818-998-7322

Fax: 818-701-4149

Interface Converter

New safety standards such as IEC 8081-2 place limits on the shock hazards to which people are subjected when using electronic devices in a medical environment. Telebyte's Model 287 RS-232 to RS-422 opto-isolated interface converter satisfies those stringent requirements for computer systems.

The Model 287 does not require a separate AC or DC input because the power required is extracted from the PC's RS-232 interface. That power is further conditioned to develop an isolated power supply to operate the link side of the interface converter.



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A DB9 female connector allows the converter to be directly attached to any PC communications port, and an RJ-12 modular connector creates the link interface. A DTE/DCE switch allows the user to reverse the transmit data and receive data signals to interface to a different type of port. Data is accommodated at rates up to 19.2 kilobytes per second. The transmit- and receive-data signals use the four inner pins of the RJ-12 connector, and the two outside pins are reserved for grounding a shield on the link cable, if one is used. The ground path includes a ground stud to which a 12-inch ground connection is attached. The Model 287 will withstand a 4-kilovolt discharge with the ground connection.

The Model 287 RS-232 to RS-422 converter costs \$155.

TELEBYTE TECHNOLOGY, INC.

270 Pulaski Road
Greenlawn, NY 11740
Tel: 516-423-3232 or 1-800-TELEBYT
Fax: 516-385-8184
E-mail: sales@telebyteusa.com
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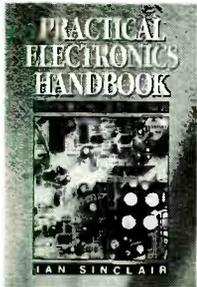


NEW LITERATURE

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Practical Electronics Handbook Fourth Edition

by Ian Sinclair
Butterworth-Heinemann
225 Wildwood Avenue, Unit B
P. O. Box 4500
Woburn, MA 01801
Tel: 617-928-2500
\$32.95



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This comprehensive book provides a practical collection of circuits, rules of thumb, and design data for professional engineers, students, and electronics hobbyists. Enough back-

ground is included to make the book accessible to beginners and to facilitate the understanding and development of a range of basic circuits. For those with more electronics experience, the book can serve as a compact compendium of everyday information and a convenient reminder of electronic principles and circuits.

Topics covered include passive components, active discrete components, discrete-component circuits, linear ICs, digital ICs, microprocessors and microprocessor systems, transferring digital data, digital-to-analog conversions, computer aids in electronics, and hardware components. The fourth edition has been updated with new chapters and sections covering topics such as sensing components, connectors, and soldering.

Switch Catalog #103

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An all-metal, sealed, vandal-proof keypad leads off the new line of keypad devices included in this catalog. The brochure also features a wide variety of heavy-duty and signal-level pushbuttons, pilots, and selectors; emergency stop switches; snap-acting switches; joystick controls; pulse counters; and power supplies. All products feature UL and international approvals as well as ISO 9001 certification. The 56-page catalog contains ordering information, descriptions, illustrations, technical specifications, and prices.

Fuzzy Logic for Real World Design

by Ted Heske and Jill Neporent Heske
Annabooks
11838 Bernardo Plaza Court
Suite 102A
San Diego, CA 92128
Tel: 619-673-0870 or 1-800-462-1042
Fax: 619-673-1432
\$49.95, including disk



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language fuzzy kernel, complete with

directions for cross-compiling it for a variety of Motorola and Intel microcontrollers. The diskette also contains all of the source code that is presented in the book.

The first three chapters present an overview of fuzzy-logic history, terminology, and theory of operation. Subsequent chapters discuss engineering fundamentals, embedded-systems considerations, and hardware/software partitioning. The book also discusses object-oriented fuzzy-logic design and C++ implementation. A fuzzy-logic primer ties it all together. Appendices include a list of fuzzy-logic development tools and suppliers, and instructions for cross-compiling the fuzzy kernel for a variety of Motorola microcontrollers.

Multimedia DSO Teaching Aid

Metrix
P.O. Box 332
Brea, CA 92622-0332
Tel: 714-992-1239
\$10



CIRCLE 340 ON FREE INFORMATION CARD

The Metrix OX-8020 CD-ROM is an interactive, multimedia demonstration of how to use a digital storage oscilloscope (DSO). Instruction is presented in French, English, German, and Spanish. Aimed at both teachers and students, the CD-ROM can be used for on-the-job or classroom instruction. Besides an introduction to the use of oscilloscopes to capture and store waveforms, the CD-ROM demonstrates how, after acquisition, data can be manipulated and displayed different ways, and how measurements can be output to plotters, computer files, and monitors.

Although it uses the Metrix OX8020

digital storage scope as a model, the disk can be used with a PC alone. Minimum system requirements are a 486 multimedia PC (with audio board), 8 megabytes of RAM, a video card, a CD-ROM drive, Windows 3.1, and at least 10 megabytes of free hard-drive space.

The Corporate Intranet: Create and Manage an Internal Web for Your Organization

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New York, NY 10158-0012
Tel: 1-800-225-5945
Web site: <http://www.wiley.com/compbooks/>
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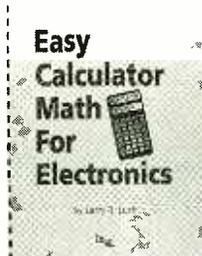
While many companies use the Internet to provide their outside customers with in-depth on-line information, relatively few take advantage of internal, or Intranet, Web sites. A corporate Intranet site is an inexpensive yet powerful alternative to other forms of internal communications. It is a secure, interactive network that allows employees to instantly access, view, and contribute to live product-management documents, regardless of what kind of computer is being used.

This book shows Internet-savvy managers, marketers, and other communications specialists how they can dynamically distribute and share vital information across their organizations—even reaching foreign subsidiaries and home-offices. It presents a practical overview of everything needed to allow a computer network to support an Intranet system. After introducing basic Web tools and technology, the book helps various departments within a corporation budget to plan and promote the Intranet. It explains how to provide outside employees with secure access, and how to create “public” and “private” channels to interface the Intranet with the Internet. Case studies from Sun Microsystems, Chevron Petroleum,

Digital Equipment, and Nortel enhance the text.

Easy Calculator Math for Electronics

by Larry R. Luchi
Limelight Books
Division of Tiare Publications
P. O. Box 493
Lake Geneva, WI 53147
Tel: 414-248-4845
\$17.95 plus \$3 shipping and handling



CIRCLE 342 ON FREE INFORMATION CARD

This study guide helps readers make quick work of math problems involving electronics. It takes the reader through each required step in more than 30 formulas used in electronics; topics include Ohm's Law, phase angles, component values for resonance, transistor characteristics, and much more.

Each formula is carefully explained, with one or more step-by-step examples presented in an easy-view, easy-to-follow format. Explanations of terminology and theory are also included, along with diagrams to help readers understand the material.

Coaxial Products Catalog #1995

Pasternack Electronics
P. O. Box 16759
Irvine, CA 92713
Tel: 714-261-1920
Fax: 714-261-7451
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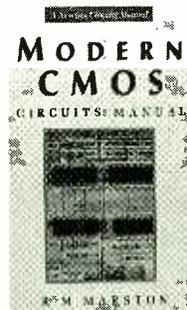
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such as multiplexers and decoders. The final chapter presents a miscellaneous collection of CMOS circuits.

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Error Coding Cookbook: Practical C/C++ Routines and Recipes for Error Detection and Correction

by C. Britton Rorabaugh

McGraw-Hill, Inc.

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New York, NY 10011

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Unless you happen to be an abstract mathematician, you're likely to get lost in the maze of error-correction coding that is a crucial element of any signal-processing or communications system. This book strives to simplify the complexities of error coding.

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EN

Q & A

continued from page 16

PIC Information

Q I've designed an electronic product that I think could be greatly improved by using PIC microcontrollers. To redesign, I need information about microcontrollers. If you have any information that you can share with me, I would greatly appreciate it. — T. Z., Easton, PA.

A Go straight to the horse's mouth and get a set of PIC manuals (including the *Embedded Control Handbook*) from Microchip, Inc., 2355 West Chandler Boulevard, Chandler, AZ 85224 (Tel: 602-786-7200). Also take a look at their Web page, <http://www.microchip.com>, and Don Lancaster's web page, <http://www.tinaja.com>. Don Lancaster is our "Tech Musings" columnist, and he has written a lot about PICs.

Other than the manuals, there's no general book about PICs as far as we know. If you're entirely new to microcontrollers, you may want to start with the 8051 family simply because good textbooks are available. One of the best

is *The 8051 Microcontroller*, by Kenneth J. Ayala, published by West; any bookstore should be able to order that for you. If you go with an 8051-family controller, consider the Philips 87C750; it's cheap (under \$5) and a development kit that attaches to your PC is available from Philips for less than \$100.

We've Been Surpassed

In the July installment of "Q&A" (see page 14), a reader asked how to light either a red or a green LED at the flip of a single SPST switch. We published a circuit with 3 resistors and a transistor. Several readers wrote in with simpler

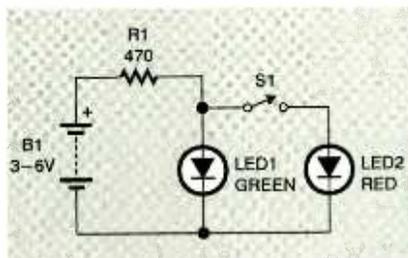


FIG. 3—THIS SIMPLER SOLUTION to the switch-operated LED problem takes advantage of the fact that red LEDs have a lower voltage drop than green ones.

solutions. Figure 3 shows the simplest, submitted by D. L. Bare of Kirby, Wyoming. Red LEDs have a lower voltage drop than green ones, so if you connect red and green LEDs in parallel, only the red one lights.

Mr. Bare points out that the voltage of an LED is directly related to the amount of energy in each photon—higher at shorter wavelengths of light. Thus infrared LEDs take the lowest voltage, and blue LEDs, the highest. The moral? Never connect LEDs in parallel—if there's even a slight difference in wavelength, the lower-wavelength LED will take all the current.

Thanks to everyone who wrote in!

Writing to Q&A

As always, we welcome your questions. The most interesting ones are answered in print, usually within 9 months. Please be sure to include plenty of background information (we'll shorten your letter for publication). *If you are asking about a circuit, please include a complete diagram.* We regret that due to the volume of mail, we cannot give personal replies. **EN**

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BUILD THIS AUTOMATIC PARTS TRAY

Learn how to use stepper motors, and build a great system that simplifies PC-board assembly in the process.

JAMES J. BARBARELLO

Stepper motors are simultaneously exciting and intimidating for the hobbyist. There's something fascinating about a precision device with so many uses. That fascination dampens, however, when you consider the logistics of obtaining steppers, not to mention the hardware and software required to drive them. Wouldn't it be nice to see a complete project using parts obtainable in small quantities at low cost?

Well, this project does just that. Using a readily available 5-volt stepper motor and a handful of common parts, we'll create a computer-controlled device called the Automated Parts Tray (APT). Using a short and simple QBasic program, APT demonstrates the principles of optimizing PC-board assembly. APT uses a stepper-controlled rotating parts bin along with a graphical display of PC-board component locations to help ensure that the right parts are inserted in the right spots on the board in optimal order of assembly.

APT can handle boards up to 6 x 8 inches. In addition, the project can be expanded easily to include closed-loop control. Further, it can even be used as the basis for a mini PC-board drilling system. (Those enhancements will be presented in future articles.) Best of all, you don't need a lot of money or special mechanical skills. All key parts are readily available from a single, well-established mail-order source, and parts cost about \$30.

All about APT. APT is a simplified adaptation of a semi-automatic electronics manufacturing system that has been in commercial use for years. The system is *semi*-automatic in that an operator must manually pick up and insert each part, but the actual part and its location are automatically determined and displayed.

In the commercial version, a series of trays are stacked vertically, like pies in a dessert display in a diner. Each tray contains several bins. The mechanism is such that all bins but one are covered. The cover can be visualized as a pie from which one slice has been removed. The area of the removed slice corresponds to the exposed bin. Each bin contains a specific part (a 10K resistor, a 2N2222 transistor, and so on).

The PC board being assembled mounts in a holder in front of the operator. To prepare for a part to be inserted, an X-Y table under the PC board moves a solid-state light source (a high-intensity LED or low-intensity laser) directly under a hole in the PC board, where one lead of the part to be inserted will go. Then a parts tray rotates so the bin containing the correct part is exposed. The operator takes a part from the tray and inserts it into the position indicated by the lighted holes.

Our version contains one tray with twelve bins. However, the software can accommodate tray changes during parts insertion, thereby affording an unlimited number of bins. And instead of using a mechanically complicated X-Y table and solid-state light

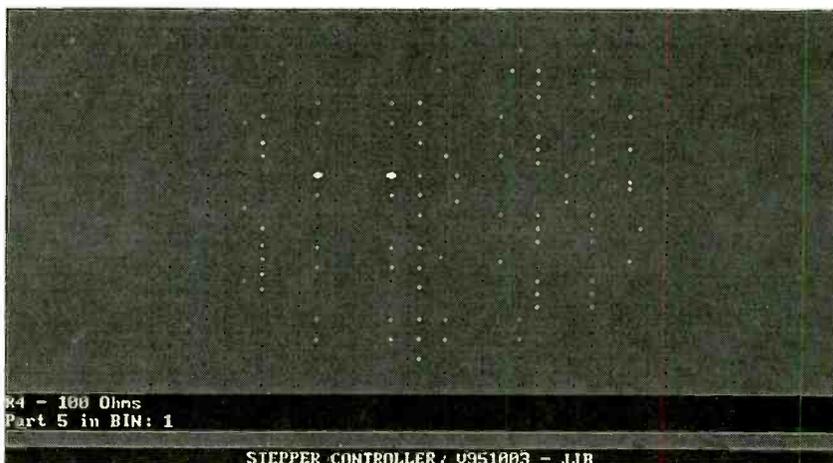


Fig. 1. The automated-parts-tray screen displays a grid overlaid with mounting holes for each component. The current component is highlighted.

source, our version displays a graphical replica of the PC board, all component holes, and a special representation of where the current part should be inserted. Figure 1 shows an example.

The mechanics of this project are quite simple, for two reasons. One is our use of an easily obtainable rotating "Lazy Susan" tray available anywhere kitchen products are sold. (We had good luck with a Rubbermaid brand tray.) Second is that we control tray movement using a direct-drive system, thereby eliminating the need for lead screws or gears. So let's get started.

The Stepper and Drive Circuit. The stepper motor is a two-phase, four-wire type. It consists of a permanent-magnet rotor and two field coils, as shown in Fig. 2. Table 1 lists the specifications for the selected motor. When the field coils are switched in the proper sequence, they attract the rotor, pull it to a precise position, and hold it there. By energizing coils A and B in the sequence shown in Table 2, the rotor will move precisely 7.5°, which amounts to 48 discrete steps through its rotation.

In Table 2, note that the four inner columns represent two things: The motor winding leads (A, A*, B, B*), and the PC parallel-port pin numbers that control those leads. Those numbers correspond to the pin numbers shown in the schematic (Fig. 3). Pin 2 represents the least-significant bit, and Pin 5 represents the most-significant bit. Column six of Table 2 shows the decimal value that should be written to the port to achieve the desired bit pattern for each step in the sequence.

As shown in Fig. 3, it doesn't take much in the way of electronics to drive a stepper. The circuit contains four identical functional blocks. The

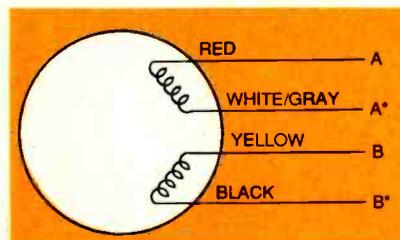


Fig. 2. A two-phase, four-wire stepper motor consists of a permanent-magnet rotor and two field coils.

TABLE 1—STEPPER MOTOR SPECIFICATIONS

Item	Description
Motor	Bipolar (2 phase) AIRPAX stepper motor (LB2773-M1)
Size	2.25 (D) × 0.99 (H) inches
Weight	0.61 lb
Electrical	5-volts DC, 800 mA, 6.25 ohms
Resolution	7.5 degrees/step
Shaft	0.25 (D) × 0.75 (L) inches
Mounting Holes	Two 0.2-inch mounting holes, spaced 2.6-inches apart
Torque	100 g-cm (detent), 1080 g-cm (holding)

TABLE 2—MOTION CONTROL SEQUENCE

STEP	A(5)	B*(4)	B(3)	A*(2)	Decimal
1	1	0	1	0	10
2	0	0	1	1	3
3	0	1	0	1	5
4	1	1	0	0	12

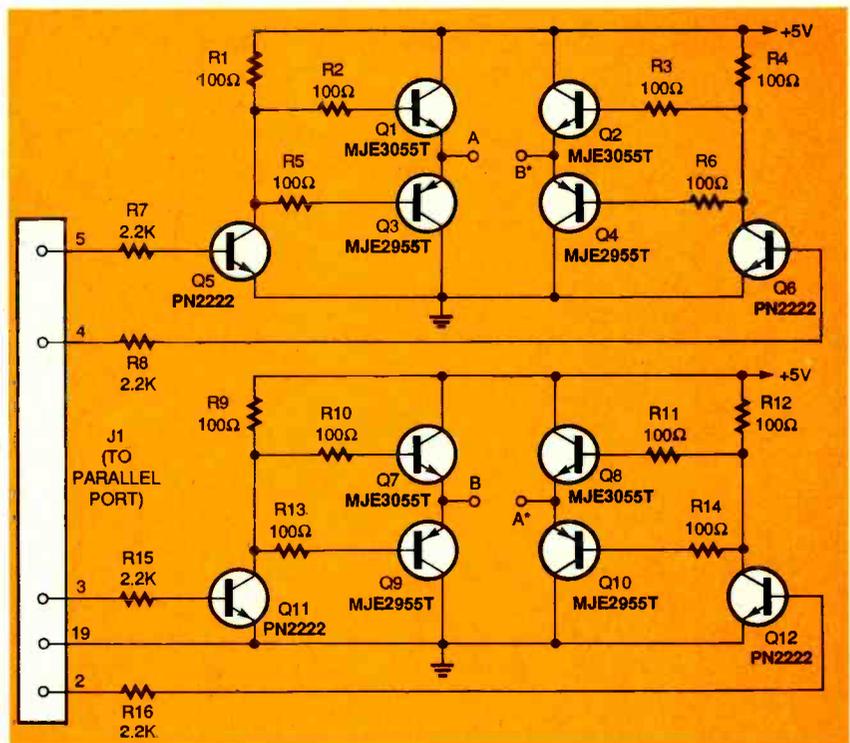


Fig. 3. The driver circuit allows a standard PC parallel port to alter the direction of current flow in both windings of the stepper motor according to the states of the four inputs.

purpose of each block is simply to provide a path from one end of a motor winding to either +5 volts or ground. By alternately switching the polarity of the voltage applied across the windings, we can cause motion to occur.

To see how that works, let's concentrate first on the block that controls the A lead. That block contains Q1, Q3, and Q5, along with the associated resistors. If pin 5 of J1 goes high, Q5 conducts, bringing its collector near ground. That in turn forward-biases

Q3, which brings its emitter near ground. Of course, V_{CE} of both Q5 and Q3 depends on the current being drawn by the load.

Now let's examine the block that controls the A* lead, including Q8, Q10, and Q12, and the associated resistors. If pin 2 of J1 goes low, the collector of Q12 goes high. That in turn causes Q8 to conduct, and Q10 to remain off. So, with A low and A* high, a current path has been established through Q8, coil A of the stepper motor, and Q3.

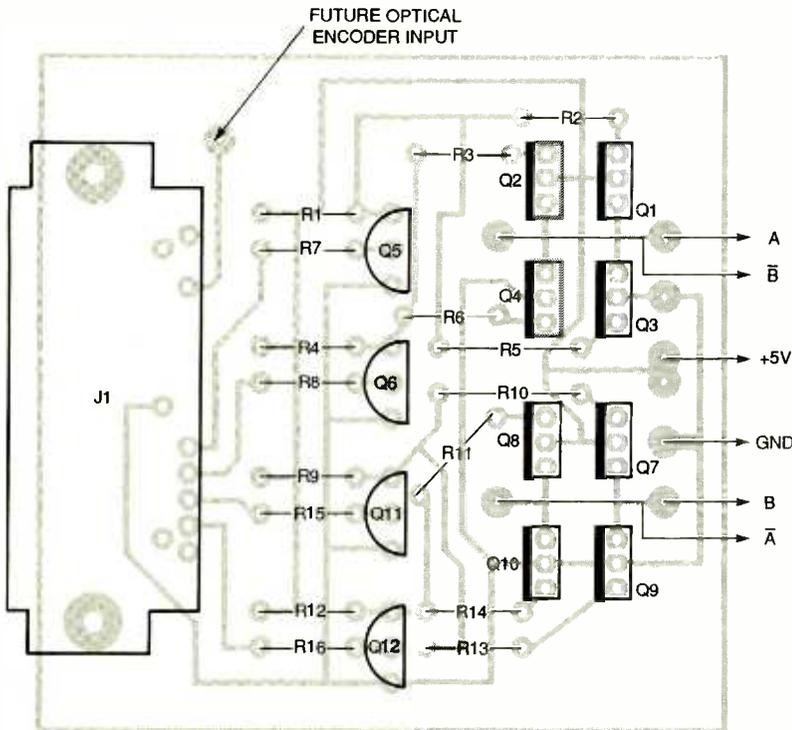
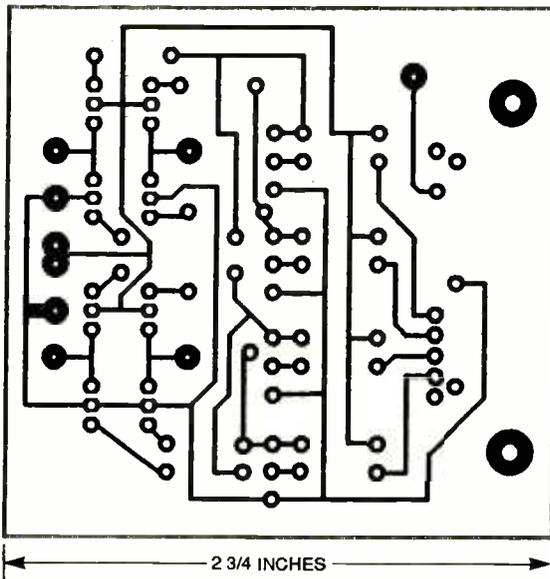


Fig. 4. Mount all components as shown here. A future installment will show how to use the optical encoder inputs.



Use this foil-pattern when etching the PC board.

Moving the Stepper. By driving input pins 2–5 in the proper sequence, we can cause motion to occur. We've already seen the motion-control sequence in Table 2. The question now is how to deliver that sequence in a format acceptable to the motor. The code fragment in Listing 1 shows how. Note that we sequentially output the decimal values from column six of Table 2, with a delay of about 150 ms

after each. The delay is required to accommodate the mechanical inertia of the stepper motor. Without the delay, the control sequences would arrive from the PC so fast that the motor would simply sit there and chatter!

Power Considerations. Many stepper-motor control circuits use a current-limiting resistor to prevent exces-

**LISTING 1—
MOVING THE STEPPER**

```

OUT 888, 10 : GOSUB DELAY
OUT 888, 3 : GOSUB DELAY
OUT 888, 5 : GOSUB DELAY
OUT 888, 12 : GOSUB DELAY
...
END

DELAY:
START! = TIMER
WHILE (TIMER-START!) < 0.15 : WEND
RETURN
  
```

sive current from causing the motor to overheat. In our circuit, the relatively large current demand of the motor causes a measurable voltage drop across the power-providing transistors (in the preceding example, Q3 and Q8). Each will have a V_{BE} drop approaching 1 volt. Therefore, the stepper motor coil sees a net of only about 3 volts. With a coil resistance of 6.25-ohms, the current provided is then $3/6.25$, or about 480 mA. That is well within the motor's dissipation capability, so no current-limiting resistor is required.

The tradeoff, of course, is that the motor provides less than maximum torque. That's acceptable in our application, but it might not be in others. You could increase torque by increasing the supply to six volts without modifying the circuit. You might be tempted to increase the supply to seven volts to offset the V_{BE} drops in the transistors and provide full power to the coils. That increase is not recommended, however, as you will exceed the motor's ability to dissipate heat, leading, naturally enough, to overheating.

We calculated current demand of each coil in this circuit configuration as about 400 mA. That implies that a 1-amp power supply should be sufficient. However, depending on the actual V_{BE} drops across the transistors, as well as variations in the motor coils, that value could increase to 1 amp or even more. To provide a margin of safety, we recommend use of a 1.5- or 2-amp power source.

There are many sources for new 5-volt, 1.5–2 amp power supplies. However, you can save a bundle by buying surplus. For example, some suppliers sell suitable power supplies for less than \$10. A potential draw-

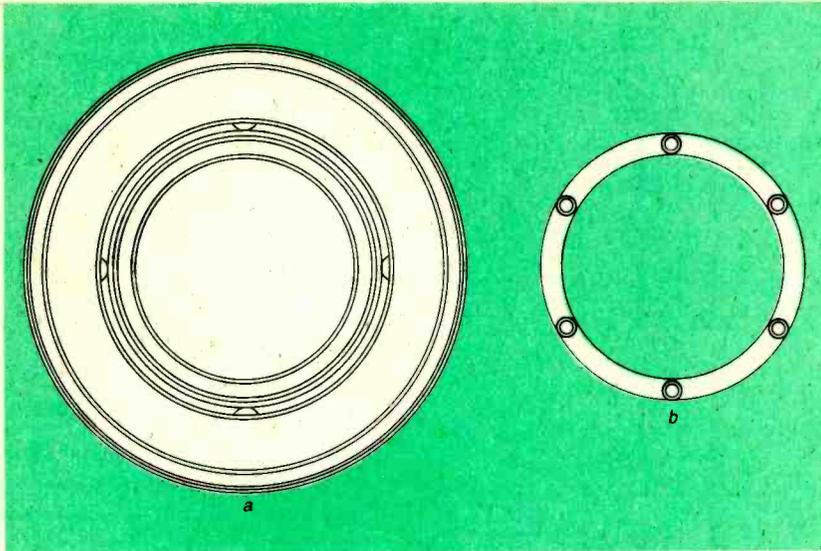


Fig. 5. The rotating tray—the complete assembly is shown in a, and the ball-bearing ring in b.

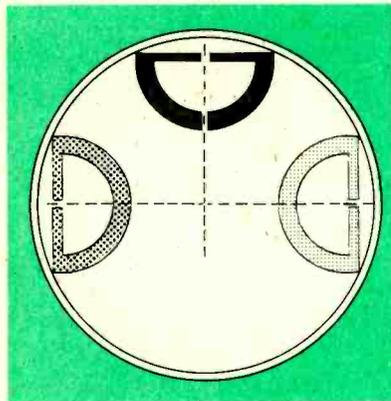


Fig. 6. Finding the center of the tray using a protractor and a straight edge; the point where the lines cross is the center of the circle.

back of that type of supply is that it may require a minimum load at all times. If that minimum isn't met, voltage may rise, for example, to about 5.3 volts. That presents no problem in our application.

Construction. Begin construction with the motor-control circuitry. A PC board layout accompanies this article; the parts-placement diagram appears in Fig. 4. Install the sixteen resistors first. Then install the eight TO-220 package transistors, ensuring both that you install the MJE3055s and MJE2955s in the right positions, and that they have the correct orientation. Next install the four TO-92 transistors (Q5, Q6, Q11, and Q12), again with the proper orientation. Now remove the connectors (if any) on the ends of the

various diameters; to be consistent with our prototype, try to obtain one that has about a 10-inch diameter. Figure 5-a shows a bottom view of a typical tray. It has a concentric ring that is press-fit under four equally spaced tabs. Under the ring is a ball-bearing assembly, as shown in Fig. 5-b. Holding the tray firmly, distort the concentric ring so it can slip past one of the tabs. Then slide the ring free of the tray and discard the ring. Remove the ball-bearing assembly and save it.

Now we have to find the exact center of the tray. That is most easily accomplished with a center finder. If you don't have one, you can use a clear plastic protractor and a straight edge. As shown in Fig. 6, place the two corners of the protractor against the inside lip of the tray and draw a line

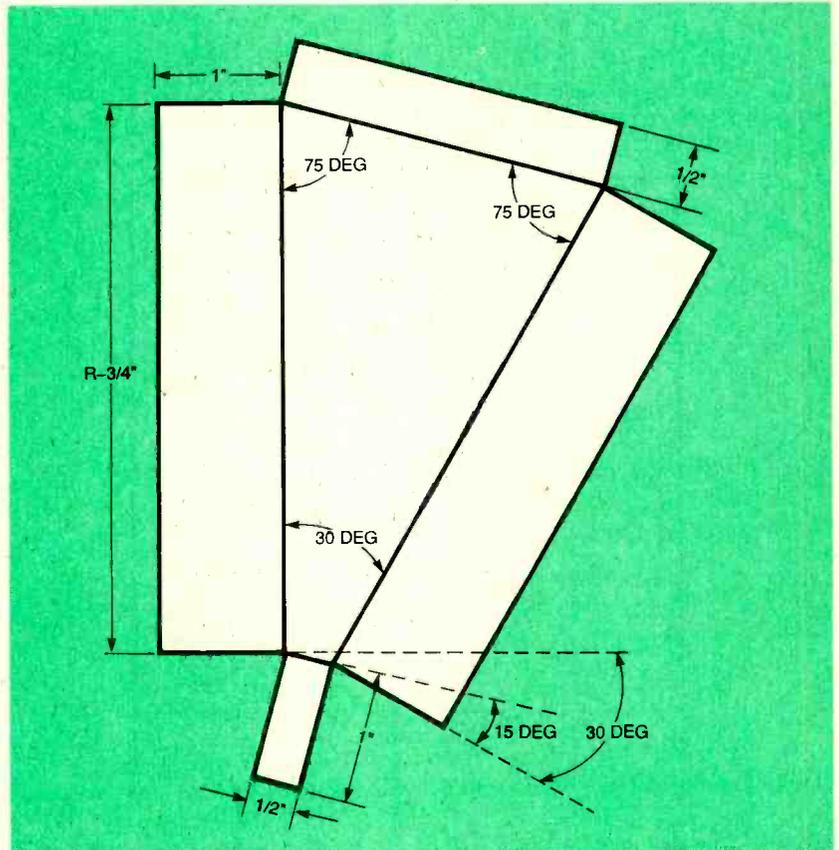


Fig. 7. Use this pattern to create the bins. The length of a side is given by the radius of the tray minus three-quarters of an inch. You'll need twelve of these.

stepper motor leads, and connect them to the appropriate points on the PC board. Attach the positive and negative power supply leads to the PC board.

Now let's look at the mechanics, starting with the tray. Trays come in

from the center marker on the straight portion of the protractor through the 90° indicator on the protractor's arc. Do the same thing at three or more locations on the tray. Where the lines cross is the exact center of the tray. (In geometric terms, each protractor

PARTS LIST FOR THE AUTOMATIC PARTS TRAY

R1-R6, R9-R14—100-ohm, ¼-watt resistor
 R7, R8, R15, R16—2200-ohm, ¼-watt resistor
 Q1, Q2, Q7, Q8—MJE3055T NPN transistor, TO-220 case
 Q3, Q4, Q9, Q10—MJE2955T PNP transistor, TO-220 case
 Q5, Q6, Q11, Q12—PN2222 NPN transistor, TO-92 case
 J1—DB-25 connector, female, PC-mount
 5-volt DC, 6.25-ohm coil, bipolar stepper motor (Airtax LB82773-M1; JAMECO I17954 or equivalent); PC board; 5-volt/2-amp power supply (JAMECO 107326, 109276, or equivalent); 2.5-mm female power jack; 2.5-mm male power plug; Universal shaft coupler (JAMECO 106606 or equivalent) (2); Rubber coupler (JAMECO 106622 or equivalent); "Lazy Susan" tray (Rubbermaid or equivalent, 10-inch diameter); ¼-20 × 1½-inch machine bolt; ¼-20 nut (2); 1¼ × 4-inch aluminum or plastic panel; #4 sheet metal screws (4); #6 or #8 sheet-metal screws (2); 24 × 36-inch piece of "Oaktag" or poster paper; ½-inch plywood; ¼-inch Luan mahogany plywood; glue, nails, DB-25 extension cable, solder, wire, etc.

Note: The following are available from James J. Barbarello, 817 Tennent Road, Manalapan, NJ 07726; PC Board; APT-PC (\$12.00). Software including source and executable code for all software in the series, sample data files, and an enhanced version of the APT software (including the optical encoder application); APT-S (\$12.00). All prices include shipping. International orders add \$5.00 (U.S. funds only). NJ residents must add appropriate sales tax. The author will accept phone calls 6-8:00 PM EST., Monday through Friday **ONLY** (908-536-5499). The author will gladly answer written questions if accompanied by a self-addressed stamped envelope.

edge is a chord, and the line you draw is a perpendicular bisector of that cord. Perpendicular chord bisectors are, by definition, along a radius, and therefore cross the circle's center).

Drill a ¼-inch diameter hole in the

LISTING 2—STEPPER CONTROL PROGRAM

```

REM** STEPPERS.BAS (c) 1995, JJ Barbarello
REM** V951007
CLS : DEF SEG = 64: DEFINT A: add = 888
DIM a(4): a(1) = 5: a(2) = 3: a(3) = 10: a(4) = 12
abinold = 1: ainit = 12: OUT add, ainit
COLOR 15, 1: LOCATE 2, 1: PRINT SPACES(79)
LOCATE 2, 26: PRINT "APT STEPPER CONTROLLER TESTER"
COLOR 7, 0: LOCATE 10, 20: PRINT "Position Tray At Bin 1, then press Enter"
waitforenter:
a$ = INPUT$(1)
IF a$ <> CHR$(13) THEN SOUND 800, 1: SOUND 500, 1: GOTO waitforenter
LOCATE 10, 20: PRINT SPACES(40)
loop01:
LOCATE 10, 27: PRINT "TRAY CURRENTLY AT BIN: "; abinold
LOCATE 20, 10: PRINT SPACES(60)
LOCATE 20, 23: LINE INPUT "Which Bin (1-12, Enter to end)... "; abin$
IF LEN(abin$) = 0 THEN END
abin = VAL(abin$): IF abin < 1 OR abin > 12 THEN BEEP: GOTO loop01
abin2 = abin: IF abin2 < abinold THEN abin2 = abin2 + 12
asteps = abin2 - abinold
SELECT CASE asteps
CASE 1 TO 6
lo = 1: hi = 4: steps = 1
CASE IS > 6
lo = 4: hi = 1: steps = -1: asteps = 12 - asteps
CASE IS < 0
lo = 4: hi = 1: steps = -1: asteps = -asteps
END SELECT
OUT add, ainit
bin = abinold
FOR i = 1 TO asteps
FOR j = lo TO hi STEP steps
OUT add, a(j)
IF i > 1 AND i < asteps THEN delay = .075 ELSE delay = .125
start! = TIMER
WHILE (TIMER - start!) < delay: WEND
NEXT j
bin = bin + steps
SELECT CASE bin
CASE IS = 0
bin = 12
CASE IS = 13
bin = 1
CASE ELSE
END SELECT
LOCATE 10, 27: PRINT "TRAY CURRENTLY AT BIN: "; bin; SPACES(2)
SOUND 625, 1
NEXT i
IF steps = -1 THEN
OUT add, a(lo)
ainit = a(lo)
ELSE
ainit = a(hi)
END IF
start! = TIMER
WHILE (TIMER - start!) < 1: WEND
OUT add, 0
abinold = abin
GOTO loop01
END
  
```

center of the tray. Obtain a ¼-20 machine screw at least 1½-inch long, and two ¼-20 machine nuts. Thread

one nut on the screw and insert the screw into the drilled hole from the top of the tray. Now thread the other

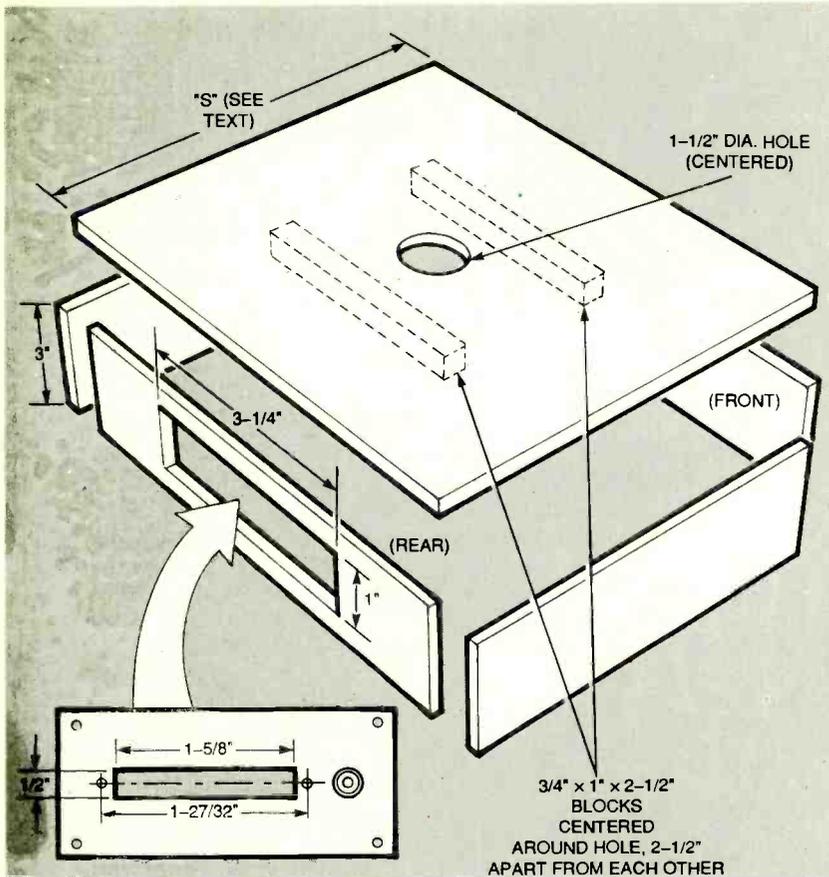


Fig. 8. One-half inch plywood serves well in building the case. The blocks on the underside hold the stepper motor, and the slot in the rear panel is for a mounting plate that connects power and the parallel port.

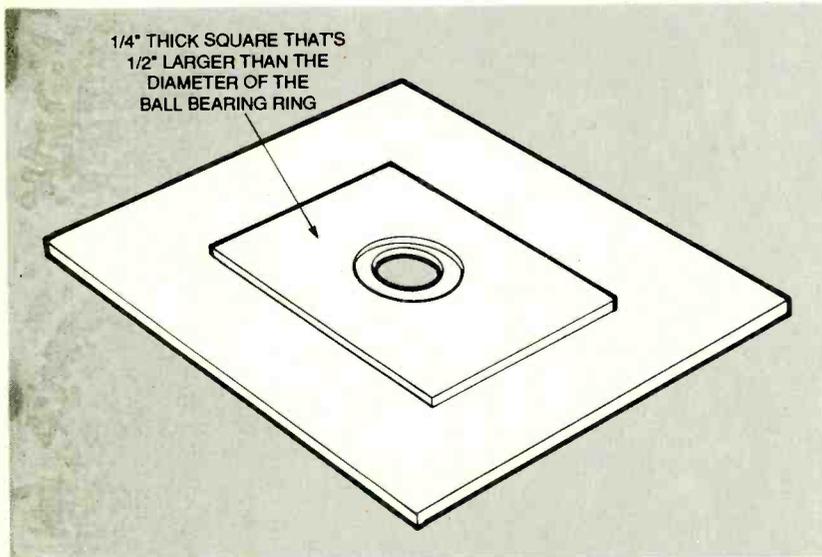


Fig. 9. The spacer provides clearance for the shaft-coupling mechanism.

nut onto the screw, locking it in place. Do not tighten the nuts at this point, as the protruding length of the screw will be adjusted later.

The next task is to make the twelve bins. Figure 7 shows a pattern for one

bin. Note that all dimensions are constants, except the length, which is defined as $R - \frac{3}{4}$ -inch. Measure the inside diameter of the tray and divide by two to obtain the radius. For example, the author's prototype used a

10½-inch diameter tray, and $10\frac{1}{2} / 2 - \frac{3}{4} = 4.5$ -inches. You can make the bins from thin aluminum, wood, plastic, or other materials. An effective alternative is poster paper (commonly called "Oaktag" paper). It's easy to work with, has the thickness of about five normal sheets of paper, and is stiff enough to hold the required bends.

Using the length calculated for your tray, cut twelve blanks. Fold the four flaps upward, being careful to fold them straight and along the lines indicated on the pattern. Secure the tabs with transparent tape. When all twelve bins are complete, arrange them in a circle and secure them to one another where they meet with additional transparent tape. With careful assembly, the bins should fit snugly into the tray. However, an exact fit isn't necessary. The requirement is for twelve approximately equal bins in an assembly that won't rotate inside the inner lip of the tray.

Building the Case. Now we're ready to build the case. We used ½-inch plywood for our prototype. Form a square box with a closed top and an open bottom, as shown in Fig. 8. Side dimension S should be ½-inch larger than the outside diameter of the tray, plus twice the thickness of the material you're using for the case top cover. For example, with our 10½-inch tray and ½-inch plywood for the cover, $S = 10.5 + 0.5 + 2 \times 0.5 = 12$ inches.

A good material for the box top is ¼-inch luan mahogany plywood. Draw a line through diagonal corners and mark the point where the lines cross. Draw a line through the center perpendicular to the sides. Draw two parallel lines on either side of that one, each ¼-inch from the first line. You should end up with two lines straddling the centerline of the top, and 2½-inches from each other.

Drill or otherwise form a 1½-inch hole at the center of the top. The actual diameter or shape is not critical, as long as the opening is at least 1 inch in diameter. Now prepare two ¾ × 1 × 2½-inch blocks. Attach the two blocks to the underside of the top and along the two parallel lines drawn previously. Screw or glue the blocks in place.

Measure the diameter of the ball-bearing assembly (BBA) shown in Fig. 5-b. Add ½-inch to that amount, and

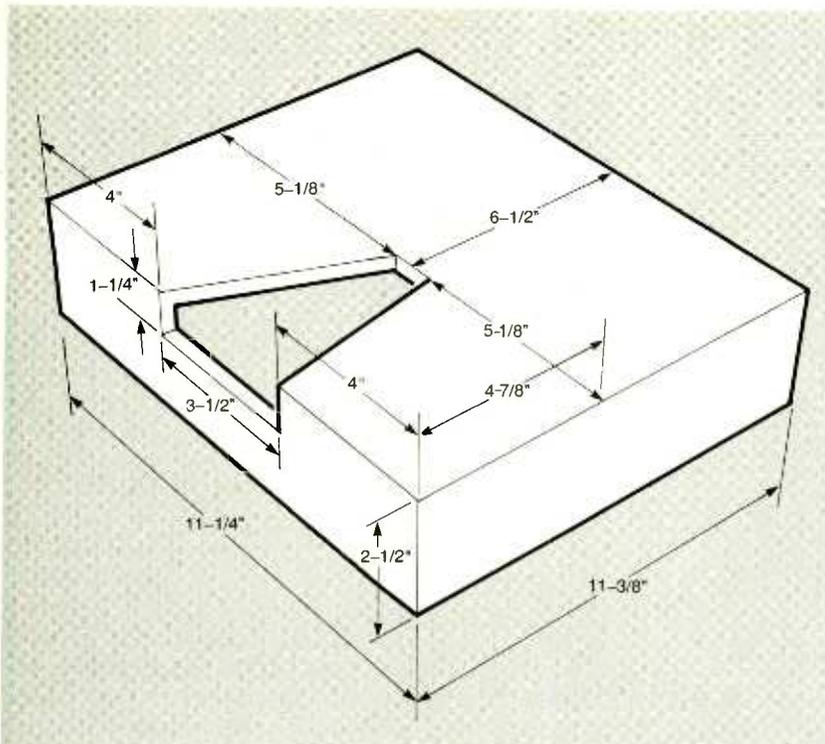


Fig. 10. The top cover is the same size as the base, and has a wedge-shaped cutout to allow access to the current bin.

call it L. Cut a piece of 1/4-inch material into a square, with sides of length L, to form a spacer. Form a 1 1/2-inch opening similar to that formed in the top and secure the spacer to the top of the case. Align the BBA to the spacer so it is concentric with the center hole, as shown in Fig. 9. After that's done, staple or otherwise attach the BBA to the spacer.

Create a centered rectangular opening 1 x 3 1/2 inches in the rear side as shown. Then make a cover of plastic or metal and mount J1 to the cover. Also mount a power connector, and attach the cover to the rear panel with #4 sheet metal screws.

Using the value of S calculated earlier, build a cover, as shown in Fig. 10. The height should be 2 1/2 inches. Do not drill a center hole; instead, form a wedge-shaped cutout as shown in Fig. 10. Using a 30-60 triangle, draw two lines from the center to one end, forming a pie shaped wedge. Fatten the wedge by drawing lines parallel to the first two lines, but 1/4-inch farther out. Extend the two lines down the front side and then connect them, forming a rectangle. Then, to trim the sharp edge of the wedge, draw a line 3/4-inch from the center. Cut out the wedge.

Final Assembly and Checkout. To finish up we need to mount the stepper motor and connect its shaft to the 1/4-20 bolt with a flexible coupling. Start by centering the tray on the case bottom. Hold it in place temporarily with masking tape. Position the motor against the blocks with the shaft of the motor facing the bolt. If the motor has a gear attached, remove and discard it. Adjust the bolt's depth as necessary so it and the shaft almost touch. Position the motor so the bolt and shaft are concentric, and mark the position of the two mounting holes. Attach the motor to the blocks with #6 or larger sheet-metal screws. Remove the masking tape.

Attach one shaft coupler to the motor shaft, and another to the bolt. Place a rubber coupler in one of the shaft couplers, and loosen the nuts holding the bolt. Mate the two couplers. Adjust the bolt depth so the tray floats 1/16 to 1/8-inch above the BBA. The object is to minimize drag, but allow the bearings to come into use if the tray tips slightly from uneven weight distribution. Tighten the nuts to secure the bolt.

Attach the power connector and the DB-25 connector to the parallel port of your PC using an appropriate

cable. Mark the front flap of one of the bins as "1," and place numbered slips of paper in each bin, beginning with bin 1 and going counter-clockwise. Place the bin assembly in the tray so bin 1 is accessible through the wedge cutout in the top.

Type the test program shown in Listing 2 into QBasic. Center bin 1 in the opening and run the program. As you select different bins, the tray should rotate to show the appropriate bin through the opening.

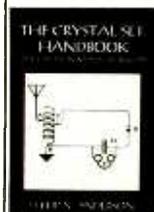
That's it for this installment. Next time, we'll present the general-purpose APT program, show how to create the ASCII data file for a PC board, and use the program to populate the stepper controller's own PC board. We'll also show how to add an optical encoder that can provide position feedback for the stepper motor. Ω

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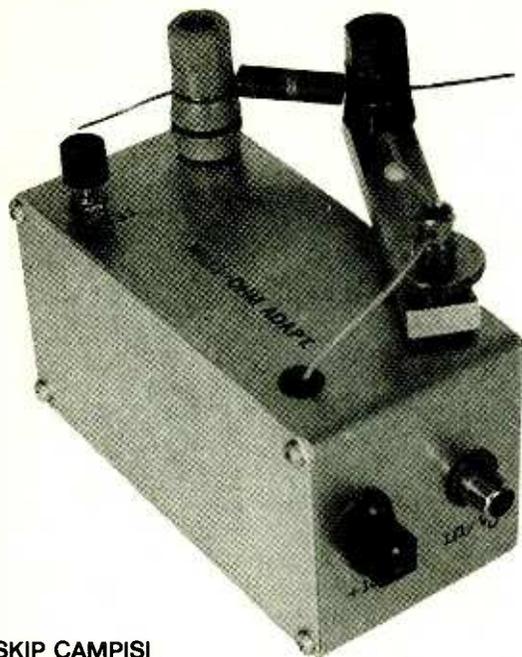
THE COLLECTED WORKS OF MOHAMMED ULLYES FIPS

#166—By Hugo Gernsback. Here is a collection of 21 April Fools Articles, reprinted from the pages of the magazines they appeared in, as a 74-page, 8 1/2 x 11-inch book. The stories were written between 1933 and 1964. Some of the devices actually exist today. Others are just around the corner. All are fun and almost possible. Stories include the Cordless Radio Iron, The Visi-Talkie, Electronic Razor, 30-Day LP Record, Teleyglasses and even Electronic Brain Servicing. Get your copy today. Ask for book #166 and include \$16.00 (includes shipping and handling) in the US and Canada, and order from CLAGGK Inc., P.O. Box 4099, Farmingdale, NY 11735-0793. Payment in US funds by US bank check or International Money Order. Allow 6-8 weeks for delivery. MA05



Build This MILLI-OHM ADAPTER

Extend the range of your DMM down to the milliohm level with this inexpensive, easy-to-build adapter.



SKIP CAMPISI

Have you ever tried to measure accurately a low-value resistance, only to find that your test leads had a higher resistance than the device you were measuring? Even with a meter capable of *nulling out* the lead resistance, the null is never stable due to the hooks or clips used for the connections.

The Milliohm Adapter was specially designed to get around that problem and to do it with an accuracy of $\pm 1\%$ for readings over a range of 10 milliohms (0.01 ohms) to 5.0 ohms. Used with a $4\frac{1}{2}$ -digit DVM, the adapter can resolve resistances as low as 10 micro-ohms, and be able to measure the resistance of a short length of hookup wire! Checking switch-contact resistance is a breeze with the adapter plugged into your DVM.

When measuring a resistance below 1.0 ohm, the leads of a resistor contribute significant error to the reading. Thus, a novel circuit approach was taken in designing the adapter. To generate an output-signal voltage high enough to be measured easily, a current of about 1.0 ampere is desirable. That current could easily fry some circuit components and damage the unit under test. However, by applying a low duty-cycle, 1.0-ampere pulse, no damage will occur. By using Kelvin voltage sensing probes right at the connections to the resistance, all of the other voltage

drops due to the 1.0-ampere pulsed current in the other leads are essentially eliminated.

About the Circuit. The schematic diagram (Fig. 1) for the adapter can be partitioned into four sections: power supply, oscillator, current source, and peak detector. The R_x (resistance to be measured) is connected between BP1 and BP2, and with the 1.0-ampere pulse applied to R_x , the resulting output transfer function appearing at J1 is 1.0 ohms-per-volt output to the DVM.

The power supply consists of IC2, a 78L12 voltage-regulator chip that provides regulated +12 volts to the circuit, and a 2N2222 transistor, Q2, which provides -0.7 volts to IC3 and a virtual power ground to the rest of the circuit. Transistor Q2 is used as a diode-connected transistor; that type produces only half of the ripple voltage that would appear if a standard rectifier were used. Battery B1 is user selectable and, although 18 volts is specified in the schematic diagram, it also can be any voltage source from 15-volts DC to 25-volts DC. For example, two series-connected 9-volt batteries will power the adapter quite nicely. Further, note that the prototype shown in the photos does away with B1 entirely; it uses a 117-volt AC power-pack adapter rated at 17.4-volts DC at 50 mA plugged into a jack on the instrument. Power switch S2 was not used on the prototype.

A TLC555 CMOS timer, IC1, is configured as an astable multivibrator operating at a frequency of about 100 Hz. The components used provide a duty-cycle of 99%; thus, a negative-going pulse of about 100 μ s results at the output, which in turn gates (switches) the current source on for 100 μ s at a duty-cycle of 1%. The resulting average current is 10 mA—safe for almost all circuits and circuit elements.

Light-emitting diodes LED1 and LED2 are standard red LEDs that have a forward voltage of about 1.75 volts each, and they are used as the voltage-reference diodes. As Q1 (a TIP125) has a forward voltage of about 1.5 volts, about 2.0 volts appears across R2 and R3, whose net resistance is 2.0 ohms; thus, a current pulse of 1.0 ampere is generated at Q1's collector. The current pulse is supplied via a capacitive-discharge type setup, from C1 (100 μ F), which is recharged via R1 (33 ohms) during the 99% off state.

Adequate compensation for any temperature drift by Q1's two base-emitter junctions are provided by LED1 and LED2, and calibration is provided via CAL potentiometer R4, which adjusts the LEDs' forward voltage by varying the bias current. The prototype adapter uses a one-turn potentiometer for R4; you might wish to use a multi-turn trimmer instead. Also, you can trim fixed resistors R2 and R3 to adjust into R4's calibration range.

The TLC272 CMOS dual op-amp, IC3, is configured as a positive voltage-peak detector, which converts

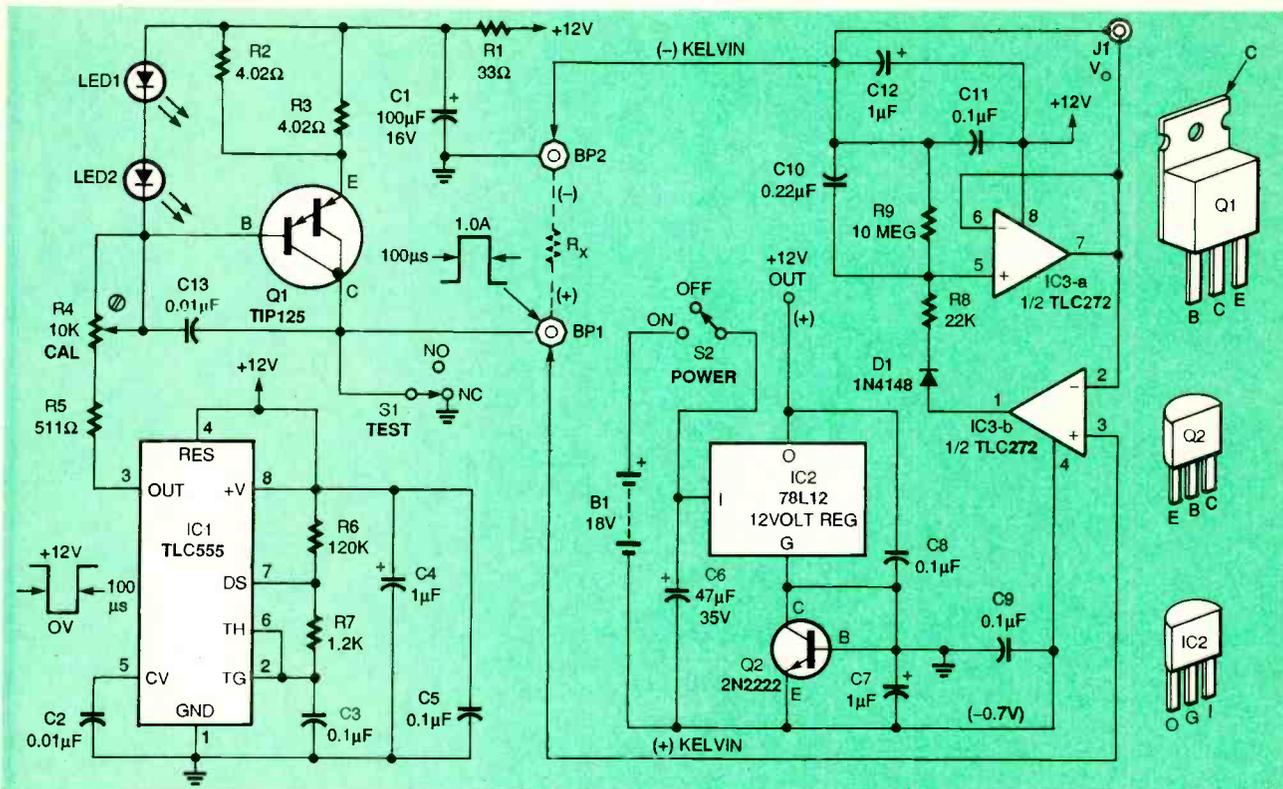
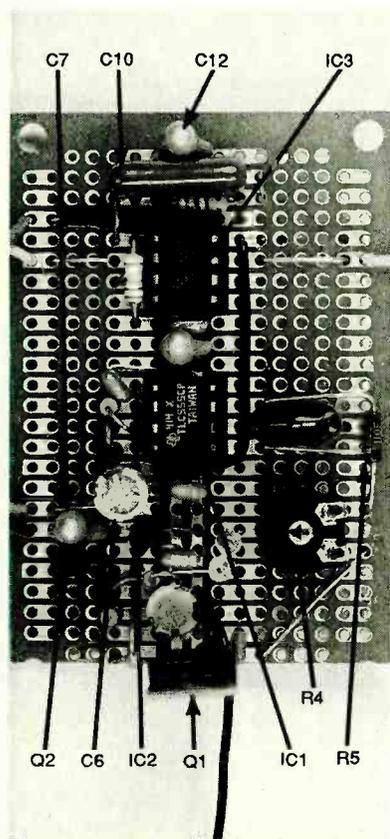
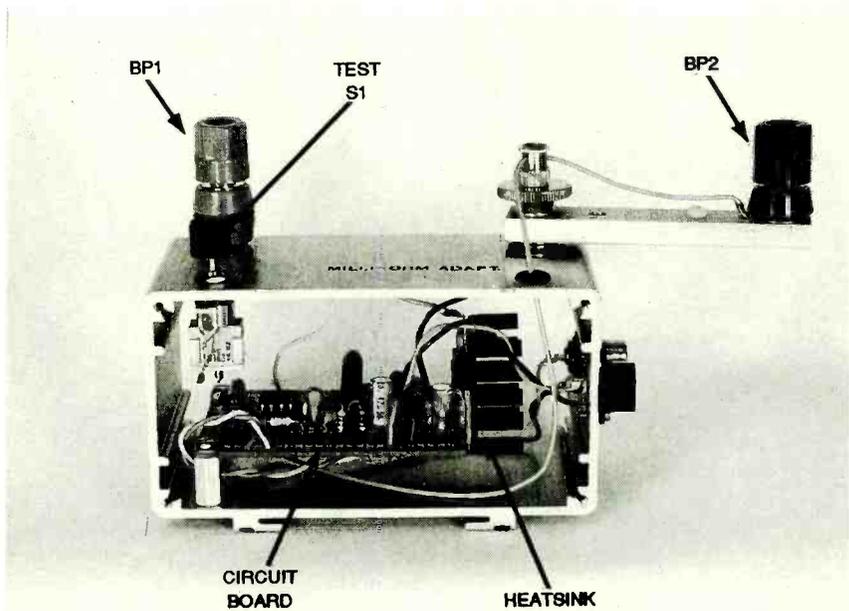


Fig. 1. Here's the schematic diagram for the Milliohm Adapter. The circuit can be separated into four sections: power supply, oscillator, current source, and peak detector.



A piece of a PC board that matches a solderless board supports most of the circuit's parts. Layout is not critical; however neatness is important.



A view of the Milliohm Adapter before the side covers are installed. Note that the heat sink has been attached to the Darlington transistor Q1 and stands free of any metallic contact.

the 1% duty-cycle voltage pulse generated across "Rx" to a steady DC voltage having the exact magnitude of the pulse's peak voltage value. Thus, the output at J1 is a DC voltage with the transfer function of 1.0-ohm-per-volt across Rx.

Construction. The only critical sections of the adapter are the binding-post connections to the resistance to be measured. Use a pair of jumbo (5-way) binding posts rated for 15 amps or more; the posts specified in the Parts List have large-area gold-plated

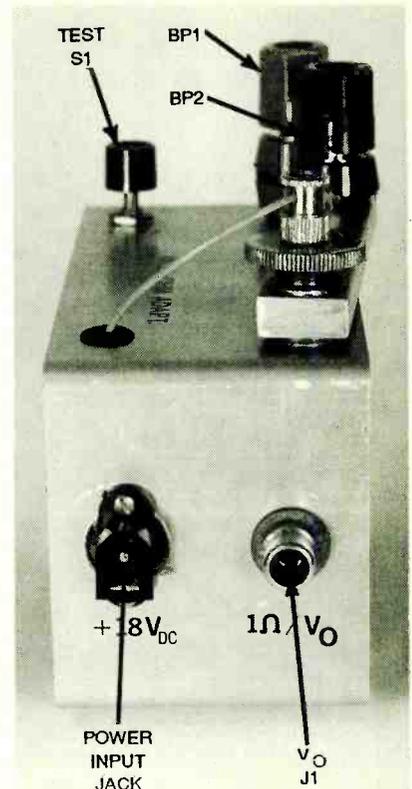
contacts that make the physical and electrical securing of "R_x" very good. Once you have selected the binding posts, the next thing you must decide is how to mount them. The spacing between BP1 and BP2 must be mechanically variable to allow easy adjustment for various resistor sizes, wire lengths, etc.

The best method for mounting the binding posts is to leave the positive terminal (BP1) fixed, and have the negative ground terminal (BP2) movable. There are three different options to accomplish this: leave BP2 dangling from its leads without any mechanical mount; cut a slot in your cabinet so that BP2 can slide back and forth in the slot; or mount BP2 on an arm that pivots on a stud, thus rotating away from BP1 for adjustment. The last method was used for the prototype. Pick any of the methods and mount the binding posts so that they are level with each other, using shims or washers where needed. Be sure to insulate BP1 from the cabinet (which has to be aluminum), while BP2 should

be electrically connected to the cabinet.

The prototype uses a cabinet made from extruded aluminum having a 3/32-inch thick wall for drilling and tapping for machine-screw attachments. For chassis boxes made from aluminum sheet metal, you can use ordinary machine screws, lock washers, and nuts.

The prototype cabinet measures 2-inches wide by 4 3/8-inches long by 2 3/8-inches high. Binding post BP1 is mounted at one end of the cabinet top, with a 10-32 x 1-inch screw protruding out of the other end. On this stud rides the swing arm, which is made from a piece of 1/4-inch thick by 5/8-inch wide by 3-inch long aluminum bar. One end of the arm has a clearance hole for the 10-32 stud, and BP2 is mounted at the other end, along with a lug for the Kelvin connection. The arm rides on washers and is locked in place with a 3/4-inch diameter, 10-32-thread knurled nut (a wing nut works fine, also). At its closest position, the binding post terminal spacing is



The power input jack (optional, see text) and insulated RCA phono jack (J1) that supplies the output signal to the DVM mounts on one side of the case

about 3/4 inch apart, which can be opened to a maximum of about 5 1/2 inches. Output jack J1 and an optional power-input jack are mounted on one end of the cabinet with normally-closed push-button switch S1 (TEST) mounted on the top, near BP1. Jack J1 has to be isolated from ground. Use fiber shoulder washers or an insulated phono jack made for the purpose. If you use POWER switch S2, mount it near S1 for the most convenience.

Assemble the circuit board, following the parts location shown in the photos, on a 1 7/8-inch by 2 7/8-inch circuit board (see Parts List) starting with Q1 on one end of the board. Attach a small heat sink to Q1. Install two 8-pin DIP sockets and potentiometer R4 as shown; then add the rest of the components and interconnects leaving long leads for connecting the jacks and switches. The positive Kelvin lead is a separate wire connected directly from pin 3 of IC3 to binding-post BP1, and the collector tab of Q1 is also connected directly to BP1 via a separate wire.

(Continued on page 79)

PARTS LIST FOR THE MILLIOHM ADAPTER

SEMICONDUCTORS

- IC1—TLC555 or TLC555CN CMOS timer integrated circuit.
- IC2—78L12 12-volt, 100-mA, positive-regulator integrated circuit
- IC3—TLC272/TS272CN CMOS dual op-amp, integrated circuit
- Q1—TIP125 PNP Darlington transistor
- Q2—2N2222 PNP general-purpose transistor
- D1—1N4148 switching diode
- LED1, LED2—Light-emitting diode, red, T1 case

RESISTORS

- (All fixed resistors are 1/4-watt, 5% units, unless otherwise noted.)
- R1—33-ohm
 - R2, R3, R_c—4.02-ohm, 1%, metal film
 - R4—10,000-ohm, one-turn potentiometer, PC mount, cermet (see text)
 - R5—511-ohm, 1/4-watt, 1%, metal-film
 - R6—120,000-ohm
 - R7—1200-ohm
 - R8—22,000-ohm
 - R9—10,000,000-ohm

CAPACITORS

- C1—100-μF, 16-WVDC, electrolytic
- C2, C13—0.01-μF, monolithic ceramic

- C3—0.1-μF, polyester (Mylar)
- C4, C7, C12—1-μF, 35-WVDC, solid tantalum
- C5, C8, C9, C11—0.1-μF, monolithic ceramic
- C6—47-μF, 35-WVDC, electrolytic
- C10—0.22-μF, polyester (Mylar)

ADDITIONAL PARTS AND MATERIALS

- B1—See text
- BP1, BP2—Binding post, insulated, 30 ampere (H.H. Smith #257)
- J1—RCA phono jack, isolated (Mouser#16PJ050, or equiv.)
- S1—Mini-push-button, spdt, momentary, 3 A
- S2—Mini-toggle switch, spdt, 1-amp (optional)
- Prototyping board (RadioShack 276-150, or equiv.), 8-pin IC socket (2), TO-220 heat sink, post spacers (2, threaded holes at ends with matching screws), threaded ends with screws to match, aluminum cabinet (see text), aluminum bar (see text), wire, phono plug, DVM plug, etc.

Note: The semiconductors and precision resistors are available from Mouser Electronics and other sources. All other parts are available at most local electronics stores and electronics mail-order houses.

Get picture-perfect results every time with this easy-to-build, easy-to-use darkroom aid.

BUILD A ZONAL ENLARGING METER

MICHAEL A. COVINGTON

Most enlarging exposure meters tell you how many seconds to expose print paper. The Zonal Enlarging Meter described here does not. Instead, it tells you how light or dark each area of the picture will turn out, based on a selected standard exposure time for your enlarger.

When in the photo darkroom, you position the Zonal Enlarging Meter with one hand and adjust the lens

opening of the enlarger with the other hand. The exposure setting technique using the Zonal Enlarging Meter is much faster than twisting the dials on a conventional enlarging meter and it assists in obtaining a correctly exposed enlargement that fits all the brightness zones of the negative into the response range of print paper, from stark white to jet black. Ordinary enlarging meters measure only one zone which is usually a high-

light or skin tone, and just guess where the other zones will fall. The Zonal Enlarging Meter lets you measure any area of the enlarger's project image on the paper surface and adjust the lens opening until that area is as light or as dark as you want it to be.

How it Works. The heart of the Zonal Enlarging Meter circuit (Fig. 1) is a National Semiconductor LM3915 LED bargraph driver IC, which lights any-

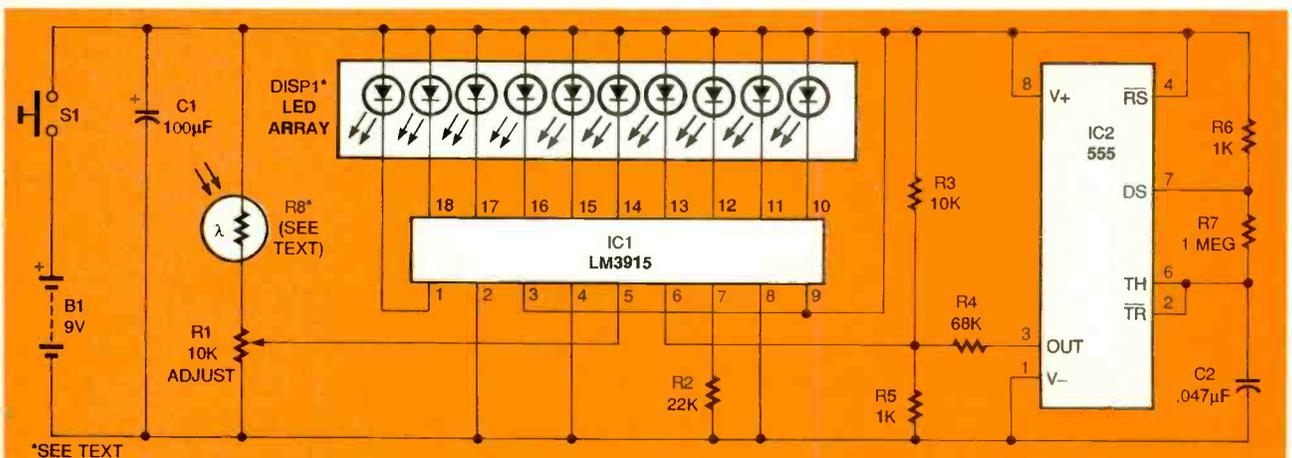


Fig. 1. Here's the schematic diagram for the Zonal Enlarging Meter. Light falling on photoresistor R8 causes LEDs in the bar-graph display DISP1 to illuminate. The number of LEDs that come on is logarithmically proportional to the light intensity.

where from 0 to 10 LEDs depending on the ratio of the input voltage on pin 5 to the reference voltage on pin 6.

The trigger voltages for the LEDs in bar-graph display (DISP1) are arranged along a logarithmic scale, just like photographic exposures, and the total voltage range is 10 to 1. Because of some nonlinearity in the photo resistor's response to light-intensity change, the range of light levels that the meter actually covers is more like 30 to 1, which is ideal because it slightly exceeds the density range of a properly exposed negative.

Each LED in DISP1's bargraph display has three states, off, flashing, and fully on; that feature lets you read a total of 20 steps rather than just 10. The flashing effect is produced by the 555 oscillator (IC2), which makes the reference voltage at pin 6 of IC1 fluctuate

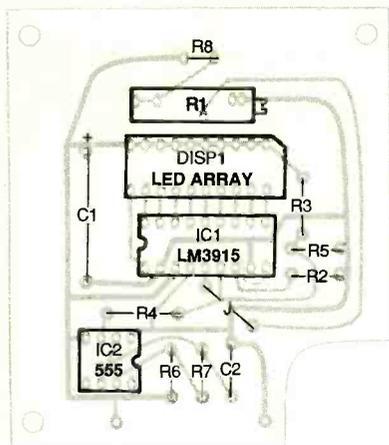


Fig. 2. Parts location diagram shows that the PC board is uncluttered and easy to assemble. Mounting holes align with the screws used to close the plastic case.

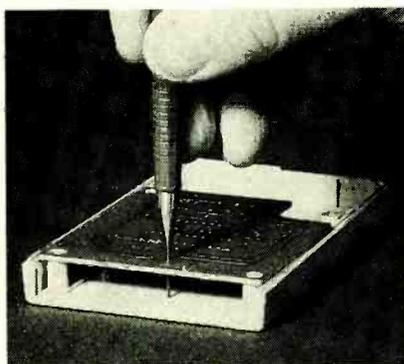
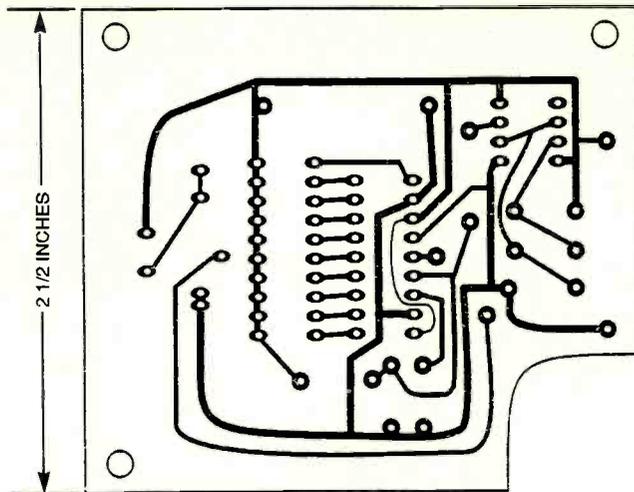


Fig. 3. Prior to inserting parts onto the PC board, extend the lead of an automatic pencil through the holes in the case cover for the LED bar-graph display DISP1 and photoresistor R8.



Same-size foil-pattern diagram for the meter's PC board. Carefully drill holes so that integrated-circuit chips and display chip mount quickly.

PARTS LIST FOR THE ZONAL ENLARGING METER

SEMICONDUCTORS

DISP1—10-LED bar-graph display, red (Mouser 351-2402 or equiv.)

IC1—LM3915 LED logarithmic-bargraph driver integrated circuit (National Semiconductor)

IC2—555 timer-oscillator integrated circuit

RESISTORS

(All fixed resistors are 1/8-watt, 5% units.)

R1—10,000-ohm, 10-turn, 3/4- to 1-inch long, trimmer potentiometer

R2—22,000-ohm

R3—10,000-ohm

R4—68,000-ohm

R5, R6—1,000-ohm

R7—1-megohm

R8—Cadmium sulfide photoresistor (see text and note below).

ADDITIONAL PARTS AND MATERIALS

B1—9-volt transistor-radio battery

C1—100- μ F, 16-WVDC, electrolytic capacitor

C2—0.047- μ F, ceramic capacitor

S1—Normally-open, momentary-contact, push-button switch

Plastic-case enclosure (includes battery connector; Pac-Tec HML-9VB.

RadioShack 270-211, or equiv.). PC circuit-board material as needed (see text), wire, solder, etc.

NOTE: A suitable photoresistor, type 76C59, is available from Mouser Electronics, 2401 Highway 287 North, Mansfield, TX 76063, phone 800-346-6873.

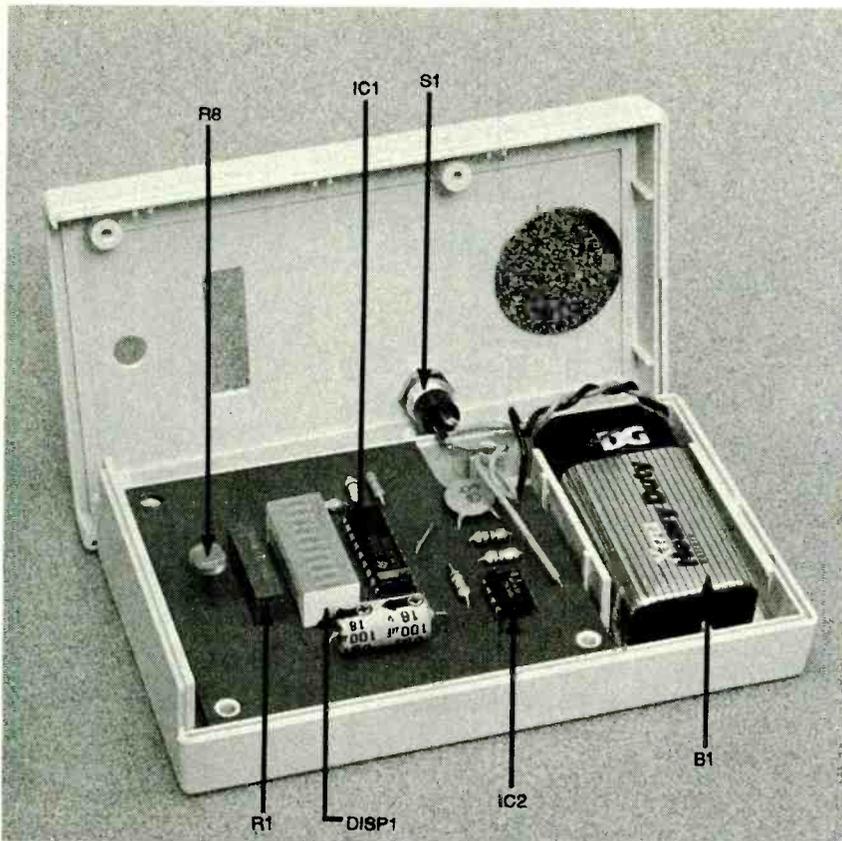
feature by omitting IC2, R4, R6, R7, and C2.

Choosing a Photoresistor. The choice of cadmium sulfide photoresistor (R8) used in the meter depends on what is available and what kind of paper and exposure time you like to use. You'll need one whose resistance is somewhere between 50K and 500K at the light level corresponding to a mid-gray tone in a picture printed on your paper with your exposure time.

One commercially available photoresistor that works well is the type 76C59 available from Mouser Electronics (see the Parts List). It's rated for a resistance of 20K to 50K ohms at a light intensity of 10 lux (1 foot-candle), and 20 megohms in total darkness. The light level for a mid-gray tone in a 5-second exposure on most fast enlarging papers is about 1 lux; at that light level, this photoresistor has a resistance of about 300K.

Another way to get a suitable photoresistor is to buy a surplus assortment and test the photoresistors until you find a suitable one. The testing procedure is simple. First, reject any photoresistors whose resistance in total darkness is less than 2 megohms, or which take more than a few seconds to stabilize when placed in darkness after exposure to room light. One way to put a photoresistor into total darkness is to wrap it in several layers of black cloth, plastic, or electrical tape. Avoid aluminum foil; it reflects light and tends to develop cracks that will throw your readings awry.

so that an LED that is just on the verge of turning on will flash. To simplify the circuit, you can leave out this flashing



The Zonal Enlarging Meter with PC circuit board and battery B1 in position just prior to closing the plastic case. Note the holes cut for the photoresistor R8 and LED bar-graph display DISP1. The photoresistor is mounted above the PC board to be flush with the inside surface of the case's cover.

Next, set up your enlarger to make a properly exposed print on your usual paper with your usual exposure time. Then put the photoresistor on a mid-gray area of the projected image, turn off the safelight, and measure the resistance. If it's between 50K and 500K, and the resistance in total darkness is at least 10 times higher, you have a workable photoresistor. If the photoresistor's test measurements are outside that range specified above, you can still use the photoresistor by substituting a different value for R1. The resistance of R1 should be about 1/50 to 1/2 that of the photoresistor.

Putting it Together. The Zonal Enlarging Meter is housed in a Pac-Tec HML-9VB plastic enclosure (see Parts List). The illustration of the foil-side pattern of the printed-circuit board provided is same-size and can be used to produce a PC board using any of the photographic techniques available. You can assemble the project equally well on perfboard or a universal, pre-drilled circuit board. The parts loca-



Here's the Zonal Enlarging Meter all closed up and ready for use.

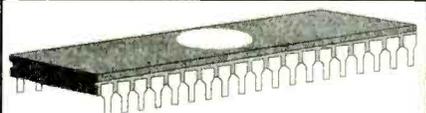
tion diagram in Fig. 2 should be followed closely no matter what circuit board you use.

The photograph in Fig. 3 shows how to locate the holes for the photoresistor and the LED display in the plastic case cover once you've made the circuit board. To cut the rectangular opening for the LED bar-graph display (DISP1) in the case, drill

holes in the corners directly over the display, then join them with a jeweler's saw if you have one. If you don't have a jeweler's saw, simply drill more holes until you have an approximately rectangular opening. Either way, finish the hole carefully with a file. Even though it is not attached to the hole in the cover, the photoresistor should stand up high enough on its leads so that it doesn't pick up stray light from the LEDs.

Calibration. Set up your enlarger to make a properly exposed print with your usual paper and exposure time. Place the meter on a mid-gray area of the image, turn off the safelight, and press S1. Adjust R1 so that five of the ten LEDs are on.

Now explore the rest of the picture. You will probably find that two or three LEDs come on in the densest areas of the negative that will show detail on the print, and eight LEDs are illuminated in the thinnest areas that will show detail. You may find it useful to make a set of strips of paper exposed at a light level of one LED, two LEDs, up to ten, so that you can see the exact shade of gray that corresponds to each meter reading. Once you have the desired adjustment for your darkroom operation, close up the meter's case. You are now ready to produce quality, full-tonality photographs at a rapid pace on the first try with each negative. Ω



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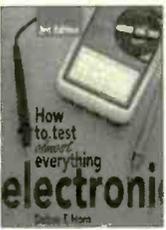
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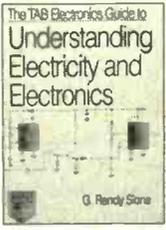
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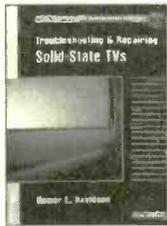
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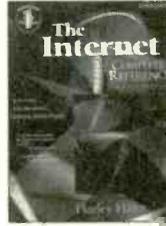
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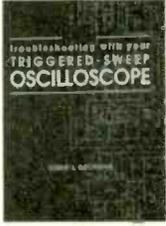
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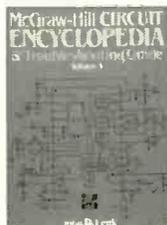
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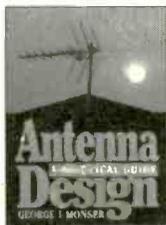
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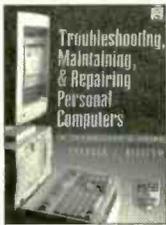
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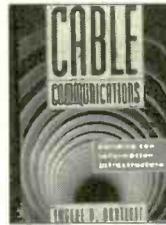
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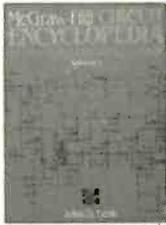
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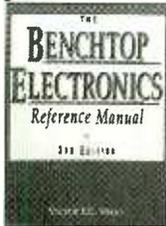
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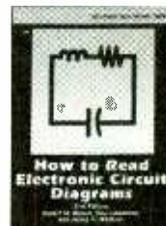
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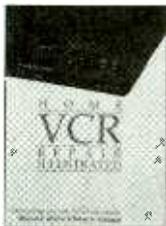
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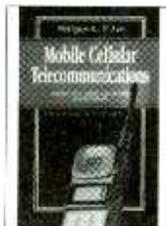
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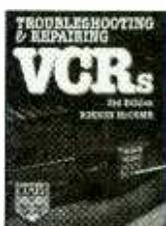
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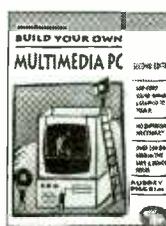
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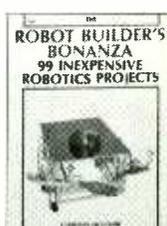
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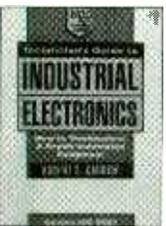
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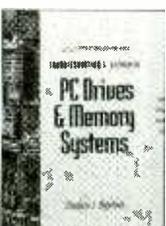
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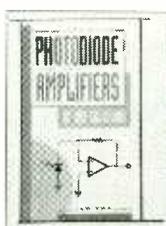
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BUILD THIS Hobby Spectrum Analyzer

*At less than \$100 to build,
this spectrum analyzer is
a must for every hobbyist!*

BOB KOPSKI

Over the last two months we have discussed the theory behind the \$100 *Hobby Spectrum Analyzer* and built and tested its various boards and subassemblies. Now it's time to put everything together and finish up the project.

Functional Interconnection and Test. Connect all four functional modules together on the bench top for a final check. This is not the *cleanest* RF arrangement, but it is workable for initial inter-module checkout.

Hook up the bench supply and current meter to the DC/DC converter and regulators battery lead. Turn on the HSA power switch but not the comb generator switch, and slowly run up the variable supply from zero, watching the current drain behavior as you advance to 12-volts DC. Look for a current draw of 26-31 mA. Turn on the comb generator; the current draw should increase 5-8 mA. Turn the comb generator-off.

Connect the log amplifier output temporarily to the oscilloscope input, and the trigger output to the oscilloscope's trigger input. Set the vertical coupling to AC, and the range to 0.1 volts/division. Set the sweep to 1-mS per division. Set the IF ATTN to normal, and the INPUT SWITCH to mid-position (50

ohms). You should see a noisy baseline trace having about 0.1 volt peak-to-peak of noise. Be sure the oscilloscope is triggered for a stable display. Turn on the comb generator. You can expect a mess of vertical lines to appear on the oscilloscope. If so, you're now ready to do final assembly and alignment.

Cabinet Assembly. All modules and related parts easily fit in the specified cabinet; nevertheless, care is required in marking, drilling, and installing everything.

Start by flattening the dimples in the cabinet bottom where the feet screws were intended to go. The rubber feet can be glued on later. Hold a Universal prototyping board on the cabinet floor and mark four hole locations for the stack bolts. The rear board edge should be located 0.5-inch inside the rear panel, and as far to the right side of the cabinet as possible. Drill the holes. The stack screws are #6 machine screws. It is easier to slip the Universal prototyping boards over the #6 screws if the holes in the boards are drilled out to 5/32-inch diameter.

Next, drill the holes for the four phono jacks on the rear panel located on a line 1 3/8-inch up from the cabinet floor to clear the stacked boards inside. Jack-to-jack spacing and elec-

trical assignment are not critical. Glue or double stick tape a 1/4-inch thick, 3/4-inch wide, 2 1/2-inch wood or foam spacer block on the rear cabinet wall right behind the battery box location. Attach a strip of self-adhesive-backed Velcro tape to the battery box bottom and the cabinet inside floor, and trial mount the battery box.

The front panel is the most difficult mechanical task. With the RF circuit

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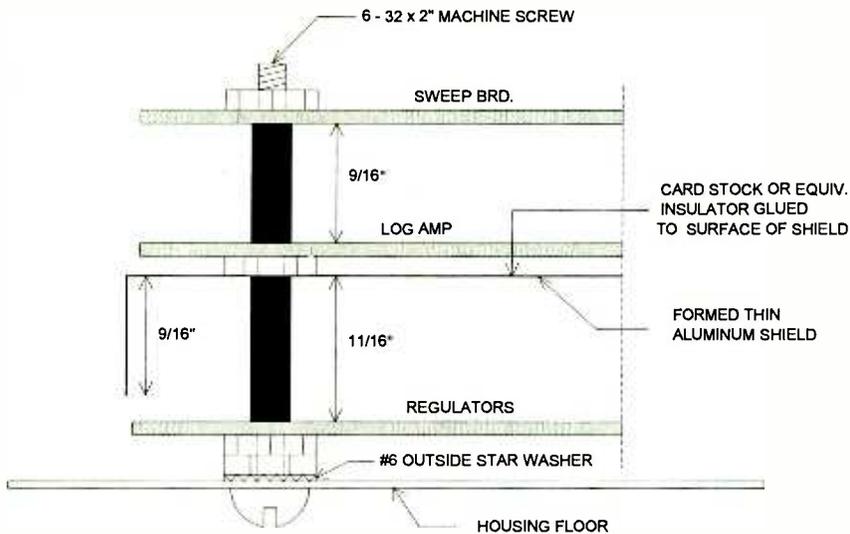
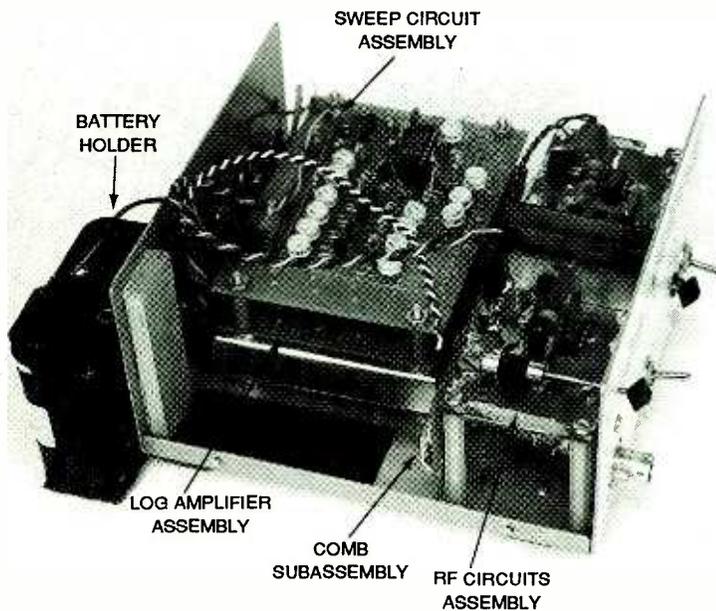


FIG. 12—MODULE STACK ASSEMBLY details are illustrated here (not to scale). Aluminum shields between the log amplifier module and DC/DC converter and regulators module provides RF shielding from stray radiation generated in the DC/DC converter circuitry.



FRONT PANEL OF THE HSA mounts four switches and a BNC connector for the input signal. The rear panel (not shown) has four RCA phono jacks that provide three output signals and a battery test point.

module in hand, mark off the various hole centers in the front panel. There are two critical hole locations: the $\frac{5}{64}$ -inch holes for the switch push rods (discussed in a moment). Make sure the alignment is correct before you drill. Use a $\frac{5}{8}$ -inch chassis punch to make the clearance opening for the BNC connector. Finally, the panel screw just above the BNC connector is a 4-40- $\frac{1}{4}$ -inch screw. It screws into a tapped hole in the BNC mounting plate to draw the latter snug against

the rear surface of the cabinet front panel.

Locate and drill the four mounting holes in the cabinet floor for the RF circuit module spacers ("legs"). The mounting holes for the toggle switches and POWER LED2 are not critical. Make push rods for the switches using $\frac{1}{16}$ -inch brass rod, a decorative bead glued on for a knob, and model-plane wheel collars to capture the sliding switch knobs themselves. Install all the electronics/interconnections in

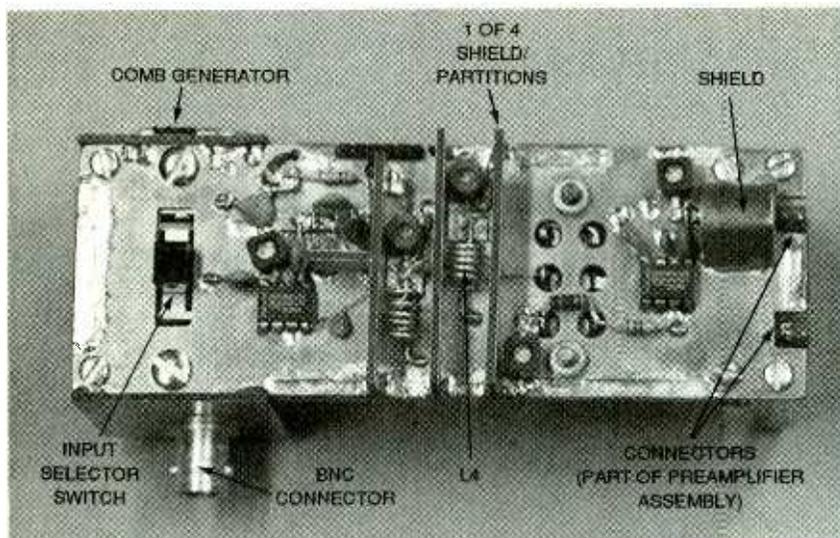
the cabinet as in the drawings and photos. Temporarily omit the topmost stack nuts (Fig. 12), so that the sweep board can be lifted to access the log amplifier.

Final Alignment. Temporarily connect the unused preamplifier output test point to the oscilloscope vertical, and connect the trigger output to the oscilloscope trigger input. Power up. Connect a lead to a source of 145-MHz signal and allow the lead to radiate near the double-tuned 145-MHz filter. Tune the second local oscillator trimmer capacitor C27 and the filter capacitor trimmers C13 and C17 iteratively (again and again) for both a visible audio frequency heterodyne and maximum signal as well. Remove the 145-MHz signal.

Position the start of the baseline sweep precisely at the left most graticule line on the oscilloscope. Turn on the comb generator. Readjust the sweep circuit board adjustments (in the same sequence as before) to progressively locate the spectral lines on subsequent graticule divisions. The sweep offset (R7) and sweep gain (R10) board-mounted controls are used to set the lines from zero to mid-screen (50-MHz) beginning with the 10-MHz component on the first graticule line. The remaining adjustments cover the last 50 MHz. Unlike the earlier rough tuneup, you can now use the segment gain adjustments (R17, R19, R21, and R23) for fine-fitting the entire sweep shape. Work with all the screw adjustments; you can't hurt anything, and you'll observe that sweep alignment goes easily.

If you find that you can't quite hit the highest and/or one or two of the lowest frequencies, note that the HSA will likely not tune below 1-2 MHz. As for the high-end difficulties, try adjusting RF circuit module capacitor C6 in conjunction with re-spacing the loops in inductor L2. The trick is to have a suitable ratio of L and C and enough motion in C (via varactor D1) to cover the band.

Fine tune the HSA using one of the comb generator's spectral lines. The 30-MHz line is good, or an external source can be used. Connect the unused preamplifier output to the oscilloscope vertical input and the trigger output to the oscilloscope trigger input. Power up. Center up the



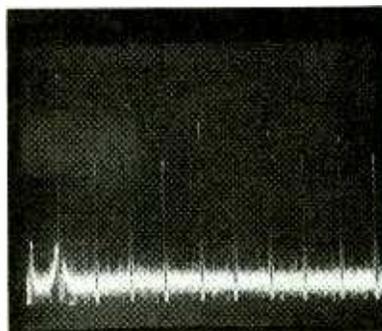
THE RF CIRCUITS MODULE has two subassemblies—preamplifier and comb generator. Note the partition/shield area in the center that isolates the two sections of 145-MHz bandpass filter. Inductor L4 has a tap on the first turn (bottom in photo) that is difficult to see in this view.

desired spectral line on the oscilloscope display, and then use the scope magnifier if it has one. You should see a symmetrical heterodyne bubble including a “suck out” at zero beat. Fine tune the IF trimmer capacitors C13 and C17 iteratively for a smooth sharp passband peak with the heterodyne dead center.

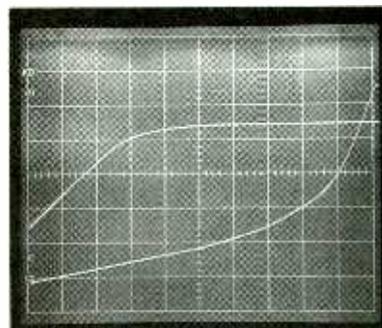
Switch in the IF attenuator and increase signal or oscilloscope gain as necessary to re-display the bubble. It will likely be detuned. Adjust attenuator-compensation capacitor C18 to reshape the display. Note that the bubble should have $\frac{1}{10}$ the amplitude of the original signal (it is 20 dB down).

The adjustment of the V+ level is somewhat subjective and somewhat quantitative. Lower voltages reduce the overall HSA gain; the highest values increase it significantly. However, along with higher gains comes more noise, jitter and trash near the baseline. The baseline may also take on an undulating or curvy appearance. Another indication is an unaccounted baseline spike located at about 72 MHz. Setting V+ to a compromise level eliminates all the above unpleasantness and provides for very good operation as well. The prototype's V+ setting is about 5.7 volts.

The spectral line at the 10-MHz position can be used to help adjust HSA amplitude performance. Locate the top of that line on an upper oscilloscope's graticule line at three



A VIEW OF THE HSA comb generator oscilloscope display after the alignment procedure is completed.



THE SWEEP-CIRCUIT OUTPUTS as viewed on an oscilloscope. The lower-most curve is the varactor (sweep) drive waveform—the bottom grid line is 0.0 volts, 5-volts per division. The upper-most waveform is the local-oscillator boost waveform—1-volt/division, top of trace is 4.5 volts. Both curves are displayed on a 1- μ s/division time base.

main graticule divisions up from center face. This is the -30 -dBm level. The

base-line noise should be down around the third main division below center line (almost six divisions below the signal). Set the IF attenuator to -20 dB. The signal should fall two vertical divisions. If it travels less, increase log amplifier output gain (R28); if it travels more, decrease the gain. Continue the adjustment until the attenuator change and the change in display agree. This calibrates the 10-mV/dB log constant.

Adjust log amplifier input gain (R2) so that logging begins above the base-line noise (positive noise peaks should not appear compressed). In all the steps above, be sure the base-line clipper trimmer (R26) is set to *just* trim off negative going spectral lines and *not* infringe on the magnitude of the base-line noise. Trimmer R26 will require resetting during the above procedures.

With that done, the 30-MHz line should be 10 dB lower than the 10 MHz line. The 50-MHz line should be down 5 more dB. The 70-MHz line should be about 3 dB down from that. Finally, the 90-MHz line should be 21 dB below the 10-MHz line. The latter is the line most likely to be off due to the comb-generator-waveform quality limitations. Finally, pay no attention to the even-order spectral lines; if the comb generator waveform were ideal they would not be present at all.

Frequency flatness is best confirmed with a quality signal source/power meter combination. The rough tuneup of the local oscillator boost given earlier should be fairly good, but if you have access to a flat source you can fine tune the boost function. The adjustments R33 and R30 control boost waveform “zero” and ramp rate respectively. The setting of R35 controls the waveform effect on local oscillator power.

Hints. The Hobby Spectrum Analyzer just begins to overload for signals exceeding -30 dBm. This is about 20 mV peak-to-peak on 50-ohm lines. Distortion manifests itself in several ways including baseline “buckling” at the base of such a spectral line, and “splatter” across the display. This situation can often be controlled with the input and/or IF attenuators.

It is sometimes convenient to transformer couple RF energy into the HSA. (Continued on page 118)



PHONE LINE SENTINEL

Put an end to phone-call interruptions with the Phone-Line Sentinel—it will let others know when you're on the line.

MORDECHAI SAAD

WE ALL KNOW HOW ANNOYING IT CAN be when you're in the middle of an important phone call and somebody else picks up the line and says "Oh, I didn't know you were on the phone." And it's all the more annoying when they start dialing without first checking for a dial tone. Of course, such an interruption can be devastating to a fax or modem transmission. If you are regularly plagued with such interruptions, then you need one of our Phone-Line Sentinels placed next to every phone in your house. The PC board measures only 1×1.8 inches.

How it works

The nominal voltage of a telephone line, when not in use, is about 50 volts DC. As soon as the line is in use, meaning that a telephone on the line has been picked up, the line drops to about 5 volts DC. Therefore, all we need is a voltage-level sensor to detect whether or not the line is in use. The Phone-Line Sentinel is just that; it monitors the phone-line voltage and lights an LED to let you know when the telephone line is in use.

At the heart of the circuit, shown in Fig. 1, is IC1, an ultra-low-current voltage-level sensor.

Using that IC, the circuit draws "no" current (about $5 \mu\text{A}$) when the phone line is not in use, and negligible current (about 3 mA) when the line is in use. Power for IC1 is supplied from the phone line via R2, D1, and C1. Transistor Q1, which powers LED1, is driven directly from IC1 whenever the proper voltage level has been detected. Resistor R1 limits the current flow through LED1, and R3, R4, and D2 divide the phone-line voltage down to a proper level for IC1. Protection from phone-line transients is provided by resistor R5 and varistor R6.

PARTS LIST

All resistors are ¼-watt, 5%.

R1—1500 ohms
R2, R3—2.2 megohms
R4—3.3 megohms
R5—5.1 ohms
R6—MOV022 varistor

Capacitors

C1—0.1 µF, 50 volts, ceramic

Semiconductors

IC1—OP8602 ultra-low-current voltage-level sensor

D1—1N5245B 15-volt Zener diode

D2—1N5253B 25-volt Zener diode

BR1—DB103 bridge rectifier

LED1—light-emitting diode

Q1—ST91A NPN transistor

Miscellaneous: PC board, modular phone cord or hookup wire, solder, etc.

Note: The following items are available from TelMore, 11 Market Dr., Syosset, NY 11791: A complete kit, including PC board and all parts in Parts List (above), \$14.99. An assembled and tested unit, \$19.99. With the assembled units, you must specify which way you want the LED positioned. With the LED pointing straight up, order LIUD-UP; with it pointing to the long side of the board, order LIUD-LS; with it pointing to the short side, order LIUD-SS; and with it mounted off the board on wire leads, order LIUD-W. Add \$1.75 for the -W model. Please add \$7.50 for shipping and handling to all orders. NY State residents must add appropriate sales tax.

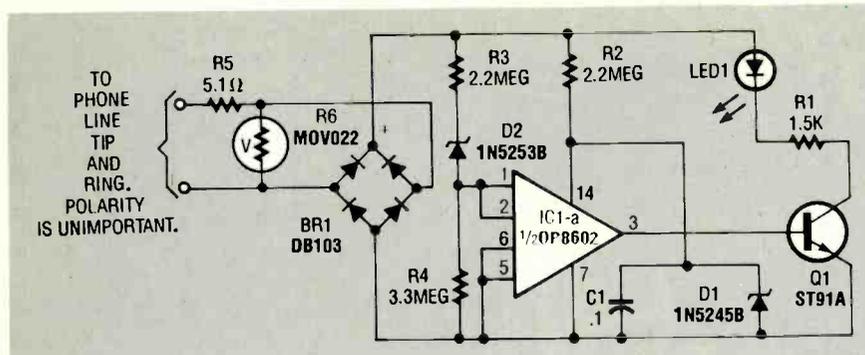


FIG. 1—AT THE HEART of the circuit is an ultra-low-current voltage-level sensor that draws only about 5 µA when the phone line is not in use.

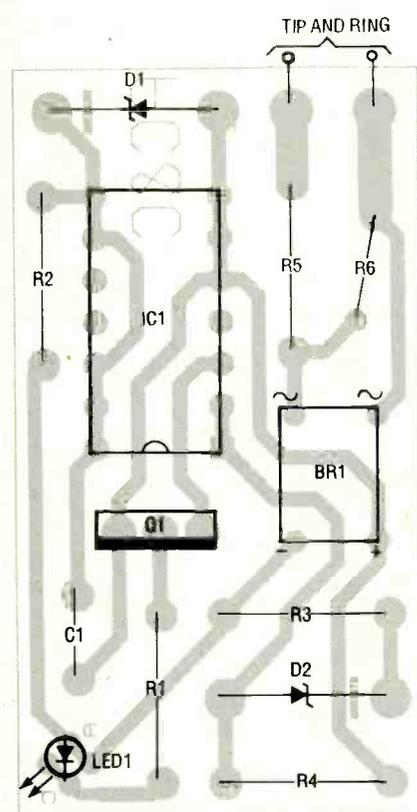


FIG. 2—IF YOU'RE USING A PC board, follow this parts-placement diagram. The LED can be mounted so that it can be bent in any direction, or remain straight up.

Construction

The Phone-Line Sentinel is available as a kit (or completed unit) from the source mentioned in the parts list. However, if you can dig up all of the parts on your own, you can point-to-point wire the circuit, or make your own board from the foil pattern we've provided.

If you're building the circuit using a PC board, simply follow the parts-placement diagram in Fig. 2. If you'll notice, the LED can be mounted on the board in

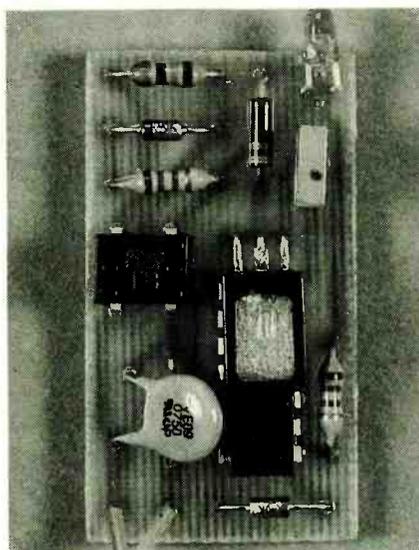
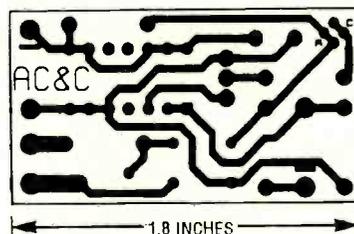


FIG. 3—THE COMPLETED BOARD should look something like this.



USE THIS FOIL PATTERN to make your own PC board.

two positions, so that it can be bent in any direction, or remain straight up. You can also mount the LED on leads as long as you like, allowing the board to be hidden from view, or perhaps inside a telephone if there's enough room, leaving only the LED indicator in view. We'll leave the details up to you. Just be sure to observe the LED's polarity on the board regardless of how you install it.

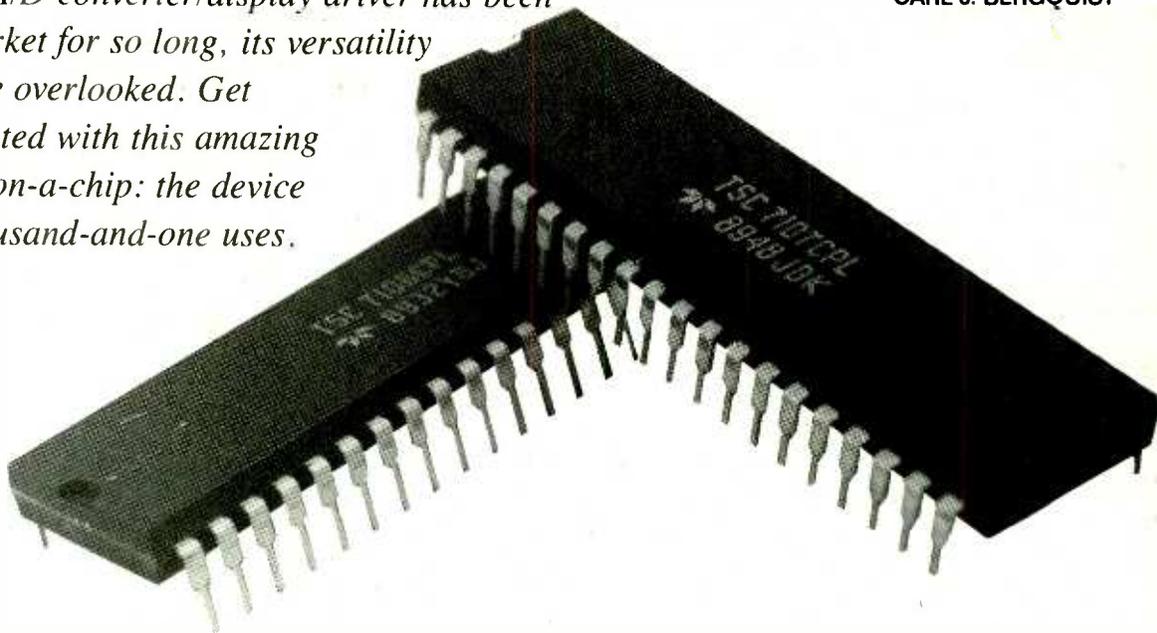
Connecting the unit to a phone line is easy. If you have a spare

jack in a desirable location, all you have to do is solder the tip and ring (green and red) wires of a modular phone cord to the board as shown in Fig. 2. Otherwise you can use whatever wire you like and connect it to the line however you see fit. Figure 3 shows the completed board.

Testing the circuit is as simple as using it. Just connect it to the phone line; the LED should be off if the line is on-hook. Then, if you pick up any phone on the line, the LED should light. After the operation of the circuit checks out, it's time to decide what you're going to do with it. Because of the extremely compact size of the board, the neatest thing you can do is mount one inside every phone you own, with only the LED left exposed. If you do a neat job, it will look like it was factory installed. □

The 7107 A/D converter/display driver has been on the market for so long, its versatility tends to be overlooked. Get re-acquainted with this amazing voltmeter-on-a-chip: the device with a thousand-and-one uses.

CARL J. BERGQUIST



USING THE 7107

With the invention and introduction of the seven-segment light-emitting diode (LED) display, adding an information display to the front panel of almost any project has become commonplace. Digits are easier to read than analog meters, and tend to "dress up" the appearance of the completed unit.

Those displays, of course, do not light themselves, but rely on logic and driver circuitry to display the desired information. The combination of a binary or decade counter with a decoder/driver is one way to display information on the LEDs, especially in clock applications, but a more versatile method is an analog-to-digital converter.

A number of options are available along that line. Combining a Motorola 14433 3½-digit A/D converter or an RCA CA3162 A/D converter with an RCA CA3161 BCD-to-7-segment decoder/driver chip is one way to go, but for ease of use, low cost, and low component count, it's hard to beat the Intersil/Harris ICL7107/7106 3½-digit A/D converter/display driver.

Originally designed primarily as a voltmeter, the 7107 is a combination analog-to-digital converter, reference voltage, timing clock, and decoder/driver circuit all on a single CMOS IC. It features high accuracy, low power consumption, and directly

drives instrument-sized, common-anode, 7-segment LED displays. The 7106 is the liquid-crystal display (LCD) version of that device and incorporates a backplane driver.

The number of support components needed for operation of the 7107 are minimal: five capacitors, four resistors, a potentiometer, and the display. Add a split five-volt power supply, and the 7107 becomes a complete 3½-digit voltmeter with a full-scale reading of either 200 mV (199.9) or 2 volts (1.999), depending on the values selected for the support components. Another attractive feature is that since both chips have been on the market for several years, their price through catalog distributors has dropped to below four dollars each.

With the basic voltmeter circuit, any measurement, value, or quantity that either exists as a voltage or can be converted to a voltage will provide the input. The 7107 is then easily calibrated to display that measurement or value digitally.

So, the possibilities are limitless. Volt-

age, current, resistance, inductance, light, temperature, speed, capacitance, frequency, etc., can all be directly displayed through simple transducer circuits. We'll show you how to do that, and armed with that knowledge, it is very convenient to either equip projects and new designs with digital displays, or modernize older gear.

7107 Circuit Operation. Figure 1 is the schematic for a basic 2-volt configuration. Power for the chip is applied to pin 21 for ground, pin 26 for -5 volts, and pin 1 for +5 volts. Pins 2-20; and 22-25 connect the device to the LED display, with pin 19 driving the ½ digit, or the leading "1", on the display. Pin 20 indicates when the input voltage drops below 0 volts, so it can be used to drive a minus sign on the display.

Pins 30 and 31 accept the negative and positive inputs, respectively, while pins 35 and 36 handle the reference voltage generated by a resistor-potentiometer divider network. The lo

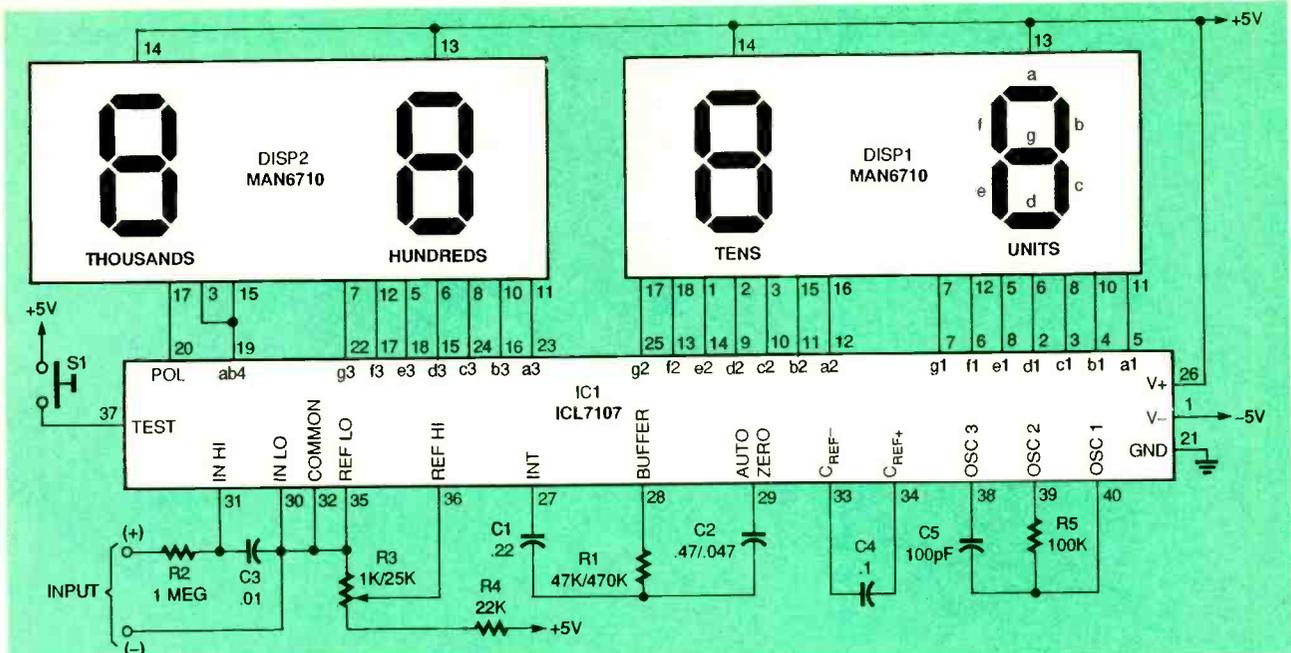


Fig. 1 The 7107 was originally designed to be a self-contained, highly accurate voltmeter. By changing the values of C2, R1, and R3, the 7107 can have a range of 200-mV or 2 volts.

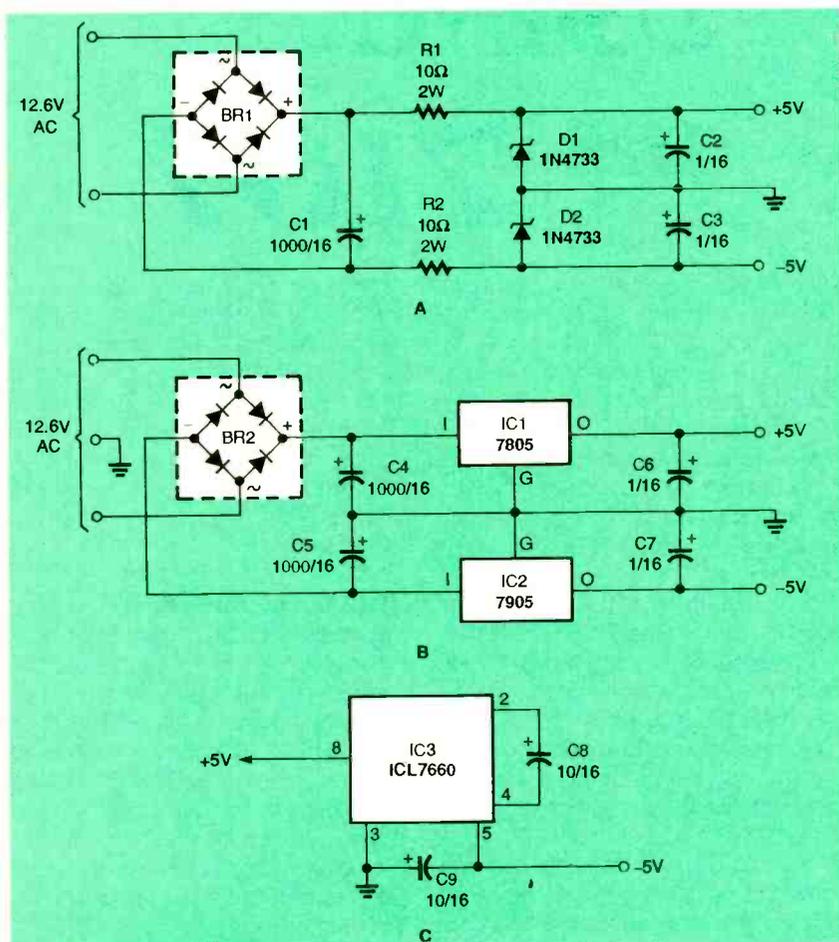


Fig. 2. Here are a few different methods of generating the + and -5-volt power required by the 7107. A pair of Zener diodes (A) are handy if the transformer you want to use does not have a center tap. A pair of three-terminal regulators (B) and a center-tapped transformer also work well. An interesting alternative is the ICL7660 chip (C), which generates a negative-voltage output from a positive-voltage input.

reference (pin 35), analog common (pin 32), and negative input (pin 30) are tied together in any application where the input signal is "floating" with respect to the power supply. The analog common also provides the reference voltage for the auto zero feature, which maintains a zero reading for a 0-volt input.

Pins 38, 39, and 40 provide access for the clocking circuit. The recommended values result in a frequency of 48-kHz (3 readings per second), which generally gives excellent performance. If a different frequency is desired, the equation $f = 45/RC$ can be used to find the component values needed. If you keep R at 100,000 ohms, the formula will select the correct value for C. In addition to the RC arrangement, a crystal can be connected between pins 39 and 40, or an external oscillator signal can be fed into pin 40.

With the exception of R1, C2, and R3, component values are common to both the 200-mV and 2-volt configurations. Resistor R1 provides linearity over the input range. Recommended values are 47,000 ohms for a 200-mV range, and 470,000 ohms for the 2-volt range.

Auto-zeroing capacitor C2 has an effect on noise in the circuit. For the 200-mV scale, a value of 0.47- μ F improves noise immunity, while 0.047- μ F is adequate for the 2-volt version. That

smaller value also improves recovery speed of the circuit. A value of 1,000 ohms for potentiometer R3 in the lower-voltage meter is increased to 25,000 ohms to provide a wider reference range for the higher-voltage meter.

For maximum accuracy and stability, it is best that all capacitors, with the exception of C5, be of the Mylar variety. With its lower dielectric absorption, that type of capacitor will provide superior performance. Capacitor C5 can be a standard ceramic disc or silver-mica type, and all resistors are 5% carbon film.

One disadvantage of the 7107 is the need for a split 5-volt power supply, but there are several simple ways to meet that requirement. If a bench supply is at hand, it usually has ± 5 volts available, either as a separate output or through the use of the adjustable supplies. If that source is not convenient, or a separate self-contained supply is preferred, Fig. 2 shows three different approaches.

In Fig. 2-a, input power from a small step-down transformer is first rectified by bridge rectifier BR1 and smoothed by capacitor C1. A pair of 1N4733 Zener diodes (D1 and D2) regulate the input power to the needed 5 volts.

PARTS LIST FOR THE 7107 VOLTMETER

SEMICONDUCTORS

IC1—ICL7107CPL A/D converter/LED display driver, integrated circuit

DISP1, DISP2—dual 7-segment common-anode LED display (MAN6710 or similar)

RESISTORS

(All fixed resistors are 1/4-watt, 5% units.)

R1—47,000-ohm/470,000-ohm

R2—1-megohm

R3—1000-ohm/25,000-ohm, potentiometer, (see text)

R4—22,000-ohm

R5—100,000-ohm

CAPACITORS

C1—0.22- μ F, Mylar

C2—0.47- μ F/0.047- μ F, Mylar (see text)

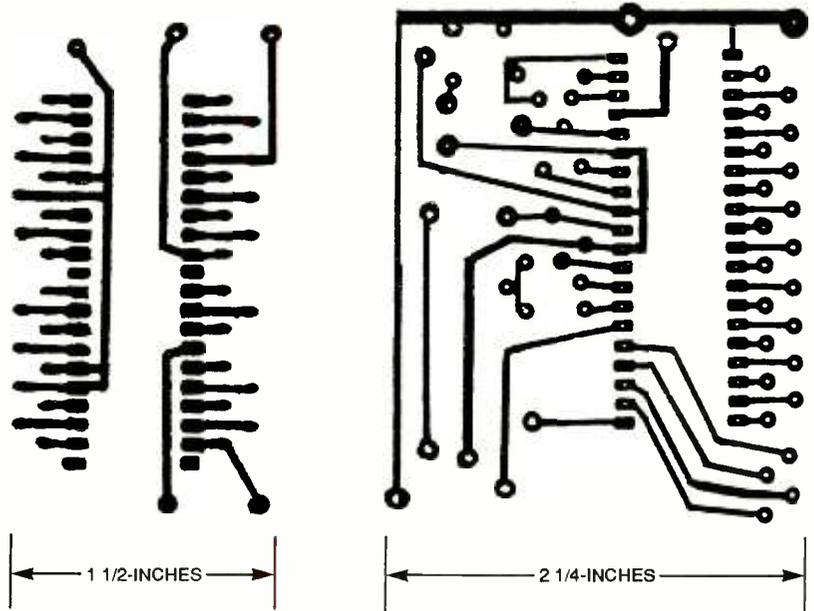
C3—0.01- μ F, Mylar

C4—0.1- μ F, Mylar

C5—100-pF, ceramic-disc

ADDITIONAL PARTS AND MATERIALS

IC sockets, hookup wire, etc.



Here are the foil patterns for the basic 7107 voltmeter and the LED display. A split power supply and a handful of passive components turn the 7107 into an accurate, easy-to-use instrument. Putting the display on a separate board makes the project more versatile in terms of mounting arrangements. You can also combine both boards into one if you need to.

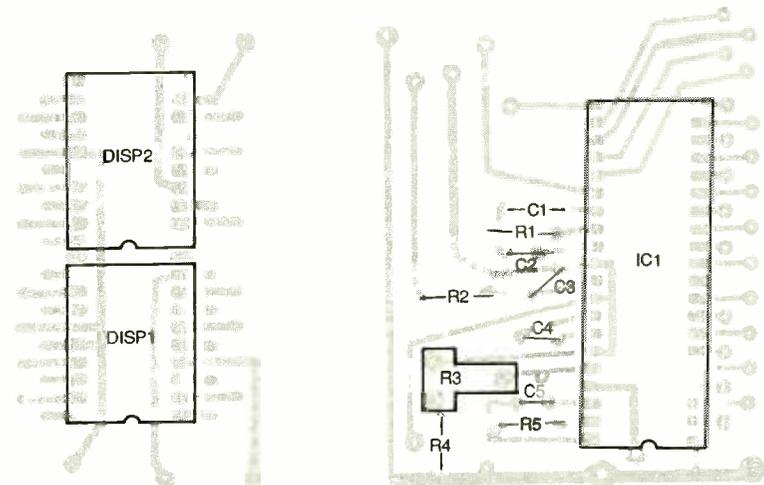


Fig. 3. If you want to build your own 7107 voltmeter, you can follow the parts placement diagrams here. Using sockets for the 7107 and the displays make troubleshooting easy.

Actually, the diodes are rated at 5.1 volts, which is well within the 7107's tolerance. Resistors R1 and R2 limit the current that flows through the Zener diodes themselves. The remaining circuitry is a standard "rail" power supply.

Figure 2-b illustrates a similar configuration utilizing positive- and negative-output linear voltage regulator ICs. However, we are using a center-tapped transformer to form a true split power supply. A disadvantage of a center-tapped transformer is the added expense. However, never try to

get around that by using a non-center-tapped transformer and connecting one side of the AC input to ground. Although that would work, it would create a "hot" ground: a potentially dangerous situation. Any extra money spent on the proper transformer will be far cheaper than spending several days in a hospital should some component in the circuit fail. Be sure both the 7805 and 7905 voltage regulators have adequate heat sinks.

Figure 2-c uses a voltage-con-

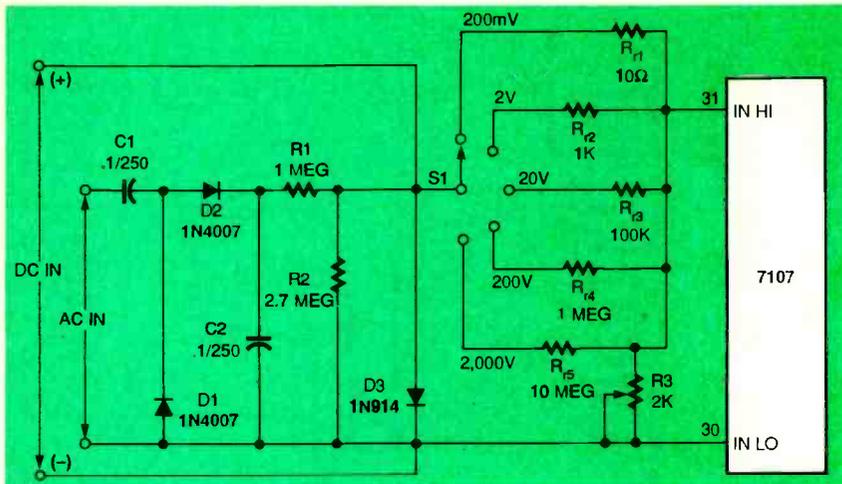


Fig. 4. Adding this circuit to the 7107 produces a versatile digital voltmeter (DVM). Both AC and DC voltages in five ranges up to 2,000 volts are accurately measured.

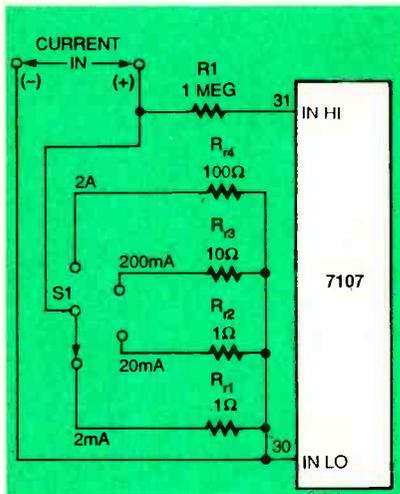


Fig. 5. With this circuit, the 7107 can measure DC current. The rotary switch lets you select from four ranges, with a capacity up to 2 amps.

version technique. In that circuit, either the Teledyne TSC7660 or the Intersil/Harris ICL7660 will work. Both are 8-pin DIP packages with identical pinouts. If a 7660 is used, the power supply need only deliver +5 volts. The 7660 converts that input voltage to -5 volts, giving us a split supply.

Construction of the Basic 7107 Meter. While breadboard or point-to-point wiring can be used, printed-circuit techniques work best. Foil patterns are included for a printed-circuit board based on the sample circuit in Fig. 1. Separate boards are used for the main circuit and the display. Multicolor ribbon cable works well as hook-up wire between the two boards. Keeping the sections separate affords a little more versatility. If you wish, the

LED readouts and main circuit can be combined onto one board. It's a simple matter to merge the two patterns together.

Regardless of how you handle your PC boards, use a 40 pin IC sockets for both the 7107 and the LED displays. That makes changing the 7107 or the displays easy if you need to. The parts-placement diagram in Fig. 3 will aid in component insertion at the proper locations. When installing the discrete components, the only orientation to observe is the IC itself, as the capacitors are non-polarized.

Like the display circuit, the power-supply circuit can either be put on the main PC board or kept separate. Convenience or personal preference will, of course, influence which way you decide to go. With all three sections completed and connected together, we can move on to the next step.

Testing and Operation of the 7107 Meter. Before installing the 7107 chip itself, confirm that the correct voltages are present at the power supply, and at pins 1, 21, and 26 of the 7107 socket. If a problem is encountered, double-check the wiring and component placement for errors. Once the proper voltages are verified, disconnect the power and plug the 7107 into its socket. Turn the power back on, and the display should read "000".

Apply +5-volts to pin 37, and "-1888" should be displayed. Pin 37 is the test input and activates all segments. A permanent switch can be added if the test function is to be used often. However, do not leave the test on for more than a few minutes if you're using the 7106. The test function on that chip applies straight DC instead of squarewaves to the LCD segments. That might cause the image to "burn" into the LCD.

Apply a known, stable voltage to the + and - inputs. Adjust potentiometer R3 until the display reads that voltage. The meter is now calibrated and ready to go.

Another method of calibration is to read the actual reference voltage at pins 35 (REF LO) and 36 (REF HI). For the 200-mV meter, that reading should be as close to 100 mV as possible. For the 2-volt meter, 1 volt is the needed measurement.

That procedure will also be useful if

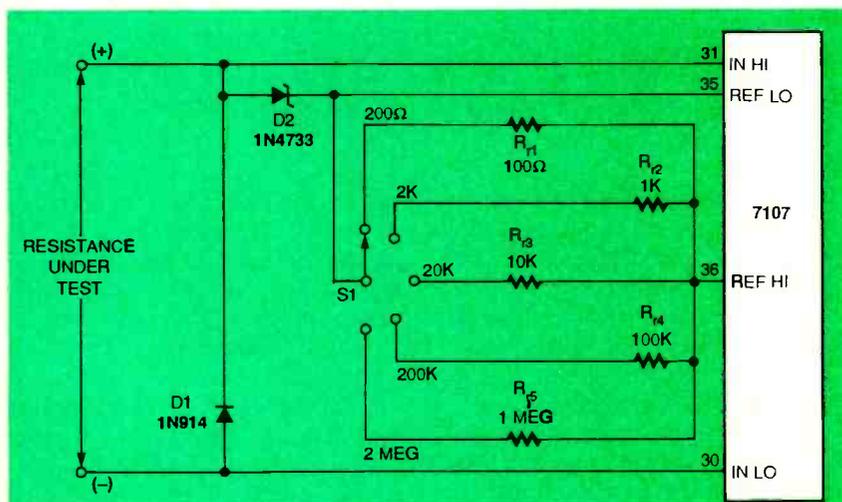


Fig. 6. Although you could measure resistance with a simple voltage-divider circuit, the use of a Zener diode and a switch-selectable resistor to change the 7107's reference voltage makes it easier to measure resistances up to 2 megohms.

ormal voltage reference is needed. In some applications where the transducer output is above or below the standard meter parameters, it is easier to adjust the reference voltage to accommodate the transducer, rather than attempt to correct the transducer's output voltage. In any event, always adjust the reference to one half the input voltage.

Additionally, a decimal point can be displayed by hard wiring a 470-ohm resistor from ground to the pole of a four-position rotary switch. With the four contacts connected to the four decimal points on the display, the decimal point can easily be placed wherever it is needed.

Applications and Input Transducers.

With the basic digital meter built and tested, it's time to put the unit to work. As we mentioned earlier, any value or measurement that is a voltage or can be converted to a voltage can be displayed, but only if we connect what we need to measure to the meter properly. That is where the input circuits and transducers come into play.

Voltage Measurements. Since the 7107 is a voltage-measuring device, let's look at that application first. Figure 4 is a circuit for a digital voltmeter (DVM) that will measure voltages from 0 to 2,000 volts in five ranges. The circuit can measure both alternating and direct current, with C1, C2, D1, D2, R1, and R2 acting as a rectifier/filter for AC measurement. Resistors R_x and R3 form a selectable input-voltage divider. Rotary switch S1 connects any one of the five resistors, R_{r1} – R_{r5} , for the selected voltage range.

Once that input circuit has been connected to the 7107, choose a known voltage source, either AC or DC. Select the appropriate range with S1, and adjust R3 to obtain a display that matches the known source. That will fine-tune the circuit for future voltage measurements.

Current Measurements. The next basic measurement to consider is current. We do that by passing the current through a shunt resistor. The shunt develops a voltage across itself in proportion to the amount of current flowing through it. That voltage can be measured by the 7107 meter.

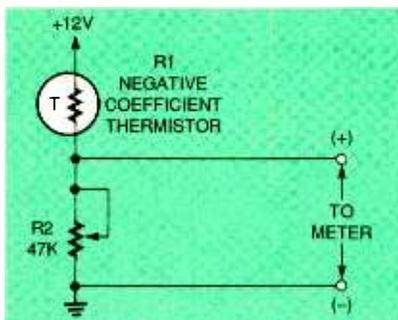


Fig. 7 A simple voltage-divider circuit using a negative-temperature-coefficient (NTC) thermistor is a low-cost and accurate method of measuring temperature with the 7107. An NTC thermistor's resistance drops as its temperature rises. If you switch the locations of R1 and R2, the reading on the 7107 will drop with rising temperature.

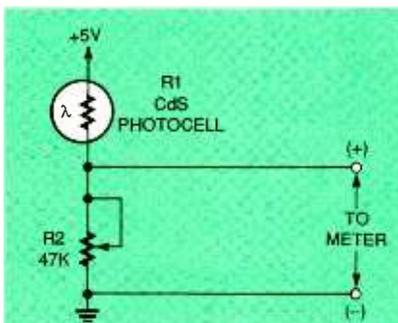


Fig. 8. We can measure light intensity the same way we measure temperature by substituting a cadmium-sulfide (CdS) photocell for the thermistor in Fig. 7. In most CdS photocells, resistance will drop with an increase in brightness. Should you need to have the 7107's display reading drop as the photocell gets brighter, or if you have a photocell that increases in resistance with exposure to light, simply switch the positions of R1 and R2.

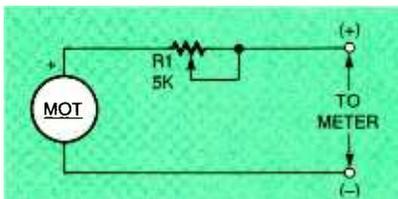


Fig. 9. You can use a small permanent-magnet motor as a tachometer. Attach the motor's armature to whatever spinning shaft you want to measure, and the voltage generated by the motor can be read directly by the 7107.

Figure 5 is the schematic of a four-range system, where R_{r1} – R_{r4} controls the range and acts as the shunt. Resistors R1 and R_{r1} – R_{r4} form a voltage divider that provides the input for the

meter. A rotary switch arrangement similar to the range selector in Fig. 4 works nicely for the ammeter as well. The values for the shunt resistor are selected by S1. Using 1% precision metal-film resistors gives the greatest accuracy.

Resistance Measurements. The last type of value commonly measured by most digital multimeters (DMMs) is resistance, and Fig. 6 illustrates a method for that. Zener diode D2 develops an external reference voltage, allowing S1 to select one of R_{r1} – R_{r5} to control the on-chip reference voltage. A DC voltage is generated across the unknown resistance, and that value is then processed by the 7107 and displayed.

That measurement could also be done with a standard voltage-divider circuit, but the problem with that method is that R_{r5} would have to be in the 500-megohm range for the 200,000- to 2-megohm setting. That is a difficult value to obtain, especially at precision levels. Adjusting the reference voltage results in a workable value for R_{r1} – R_{r5} .

Temperature Transducer. There are a number of ways to measure temperature. Figure 7 is a simple and surprisingly accurate method. In that configuration, a 47,000-ohm potentiometer provides as calibration, and a negative-temperature-coefficient (NTC) thermistor acts as the temperature probe. By applying 12 volts and setting the decimal point on the display between the units and tens digit, readings to an accuracy of $\frac{1}{10}^\circ$ can be achieved. Again, the circuit is a voltage divider.

Light Measurement Transducer.

The light transducer in Fig. 8 is almost identical to the temperature sensor. The only differences are a 5-volt supply voltage and the use of a cadmium-sulfide (CdS) photocell in place of the thermistor. Changes in ambient light shining on the photocell changes the resistance of the cell. That in turn changes the voltage produced by the divider. Any change in light intensity will be shown in the display. The display can be calibrated to indicate "f-stops" for photography work, or can be an arbitrary numerical value for which a chart or graph

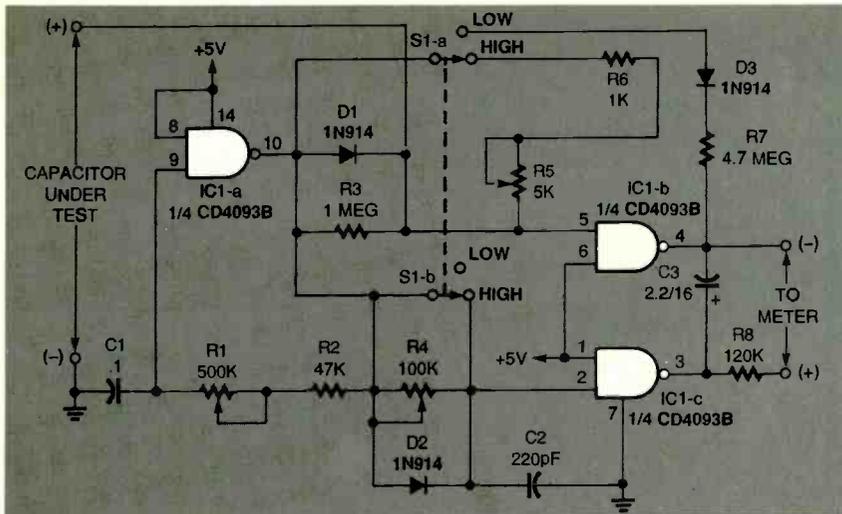


Fig. 10. With this circuit, the 7107 gains the ability to measure the value of capacitors from 2 pF to 2 μ F. Potentiometer R4 adjusts the circuit for a zero reading, while R1 and R5 calibrate the low and high ranges.

can be developed as appropriate. By using a photocell with a range of 500-ohms illuminated to 2- to 3-megohms dark, very sensitive results can be achieved with the circuit.

Those two circuits illustrate how any device that changes resistance due to any circumstance can be plugged into the divider network. You can try replacing the CdS photocell with a 1,000-ohm potentiometer. After calibrating with the 47,000-ohm variable resistor, the exact value of the potentiometer between 0 and 1,000 ohms will be displayed.

Speed Measurements. Figure 9 shows a method of measuring rotary speed. Since the 7107 is a voltmeter, and electromagnetic motors produce a voltage when their armatures are rotated, the measurement circuit is extremely simple. A 5,000-ohm potentiometer is used for calibration, with one end connected to the positive motor pole, and the other tied to the HI input (pin 31). The negative side of the motor goes to the LO input (pin 30). When the motor shaft is coupled to a rotating object, the voltage developed is proportional to the speed of rotation. That system can be used for tachometers, wind-speed indicators, generator-voltage monitors, and the like.

Capacitance Meter. One of the most useful bench tools around is the digital capacitance meter. Those meters will save not only time, but money as well. Surplus capacitors are

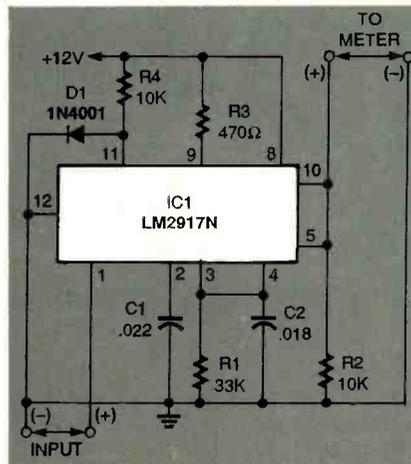


Fig. 11 Adding an LM2917 to the 7107's inputs lets you measure lower frequencies up to about 10 kHz.

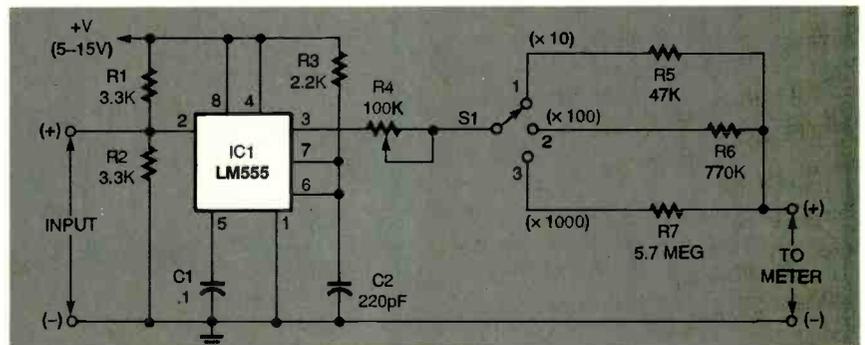


Fig. 12 To measure higher frequencies than the LM2917 can handle, this circuit does the job quite well. Frequencies in 3 ranges up to 2 MHz (1.999 x 1000) can be measured.

often sold by the pound at a greatly reduced price, but due to factory marking, or no marking at all, it can be hard to determine the values of those. A capacitance meter solves the problem, but most commercial meters are

relatively expensive.

Figure 10 is the schematic for a unit that makes use of a 4093 quad 2-input NAND Schmitt trigger, and will measure capacitors from 2 pF to 2 μ F in two ranges. The low setting handles 2 to 1,000 pF while the high setting is for capacitor values from 0.001 to 2 μ F. The circuit hooks up directly to the 7107.

Once connected to the 7107, calibration is simple. Turn the unit on and adjust R4 for a zero reading. With S1 in the low setting, connect a 100-pF capacitor to the test leads, and adjust R1 for a reading of "0100". Then switch S1 to the high setting, and with a 1- μ F capacitor connected to the test leads, adjust R5 for a "1000" display. With that done, the meter is now ready to test and measure capacitors within the meter's range.

It is a good idea to conduct those last two steps with several known capacitors to fine-tune the calibration. While not shown in the schematic, it is common practice when using CMOS-technology ICs to connect the inputs of any unused logic gates (e.g., pins 11 and 12 of IC1) to either ground or the positive voltage. That will reduce power consumption and interference. On a final note, be sure the +5-volt supply is well regulated to maintain accuracy.

Frequency Measurements. Figure 11 uses the LM2917N frequency-to-voltage converter in a standard configuration. That device is a simple and

inexpensive way of displaying frequency with the 7107. The 2907/2917 series was originally designed for tachometer systems, and is limited to frequencies from DC to about 10,000
(Continued on page 79)

Understanding Digital Filters, Using Your Time Profitably, and More

RECENTLY GOT A HELPLINE CALL FROM SOMEONE WHO STRONGLY FEELS THAT THEY HAVE ONCE AND FOR ALL SOLVED THE CELLULAR-PHONE FRAUD PROBLEM. THAT SOLUTION WAS BASED ON THE USE OF HIS ELEGANT SYSTEM-

software modification. The question was how to profitably market the concept. Well, maybe, or maybe not.

Without a closer look, and even if it did not have any obvious or hidden flaws, the chances are that this caller's simple solution would only further escalate the cell wars a notch. But that's not the problem.

The problem is that certain things can be sold by small-scale start-ups or independent individuals, while some can not. Whenever you come up with what you think is a solution to an industry problem, it seems to me that there are

three key questions you should ask:

- **Are you an industry insider?** Do you aggressively subscribe to all the field's trade journals, read its books, attend its shows, and network with its experts? Do you thoroughly *grok* the fundamental technical and marketing principles of the industry?

If not, the odds are overwhelming that you're developing a non-solution to a non-problem. You probably do not possess the skills or the tools to even understand the real problem, let alone correct it. And that the "gotchas" here are certain to "git ya."

- **Does the field welcome innovation?** If the industry 1) has areas that are highly regulated; 2) has a complex infrastructure; 3) is controlled from a solidly entrenched oligopoly; or 4) requires major changes for your concept to fly, it is not a reasonable place for you to be spending your time and effort. Also, avoid investing time in fields populated by lawyers eager to eat innovators for lunch, or one that is subject to lawsuits, etc.

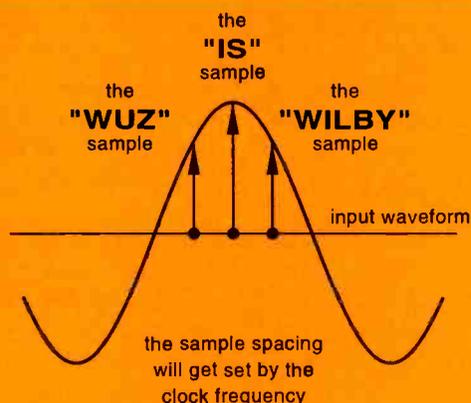
- **Can you sell six of them?** Your best concepts are those you can sell to real people who have real wallets in their back pockets, with real credit cards in them. If you cannot sell a few of your designs to your friends, there is no way you will ever sell lots of them to your enemies.

Let's look at some "for instances:" If reasonably priced, your improved laptop battery would be instantly gobbled up as a sure-fire winner. But that very same battery technology for an electric car is pretty near certain to get ruthlessly stomped upon.

A new personal-airplane design is guaranteed to bankrupt you—every time. But a variant sold as a quarter-sized R/C model kit could be a very popular product, especially when it doubles as a video platform.

More to the point: A snap-on accessory that an end-user can attach to a phone to eliminate cellular fraud is workable. But fundamental changes in the cellular standards and distribution are not. At least not for most small scale startups or outside individuals.

Sure, it's real difficult not to get excited about a new concept. Long ago, I allowed low-pressure pneumatic



Select carefully chosen coefficients X and Y. Then...

$$\text{filter output} = Y(\text{WUZ}) + X(\text{IS}) + Y(\text{WILBY})$$

FIG. 1—THE "TRISAMP" is a useful building block that can let you understand, design, test, debug, and apply digital filters.

**new from
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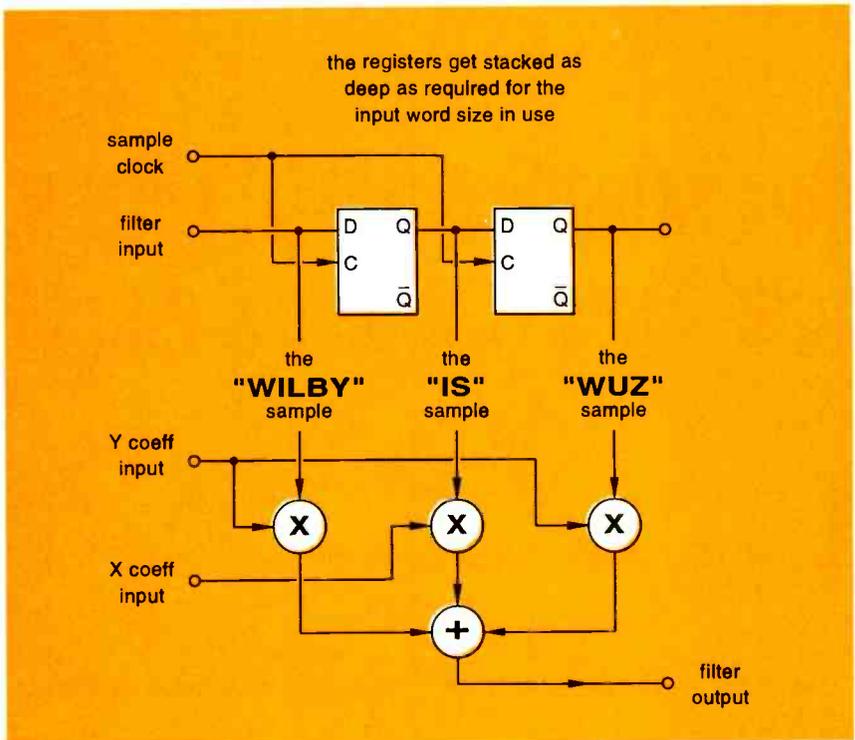


FIG. 2—DIGITAL FILTERS can be much more powerful than analog ones because they can look both forward and backward in time. The need for a "time machine" is avoided by using the shift-register scheme shown here.

robotics to gobble up all sorts of time and resources. And my magic sinewave development is currently using as much as twenty hours a day of my time. But, as hard as it is to do, you must focus on stuff that is technically challenging and still marketable by a small scale start-up if you are to be successful. Asking the fundamental questions outlined above ahead of time can save you lots of hours and grief and lets you focus your time and energy in better directions.

For much more on all this, see my *Case Against Patents* package, **WHEN2PAT.PDF** on www.tinaja.com, and, of course, my *Incredible Secret Money Machine*.

Digital Filters

Most books on digital filters seem excessively and unnecessarily arcane to me. This month, let's instead try a totally different and off-the-wall approach.

A filter is just some frequency-selective network that is designed to favor certain frequencies over others. It is usually used to isolate a desired signal or to improve the signal-to-noise ratio of a system. For example, the treble control on your hi-fi is a low-pass filter, the bass control is a high-pass filter, and AM radio tuning uses a bandpass filter.

Traditional filters were originally built with capacitors and inductors. Many of those were replaced long ago by active filters—combinations of resistors, capacitors, and op-amps that exactly fake inductors. You can find more details on that in my *Active Filter Cookbook*.

In contrast, a digital filter takes an existing pile of numbers and runs multiply-and-add calculations upon them to create a new pile of numbers whose behavior will, we hope, be "better" in some way or another than the original. For instance, a stream of digital video can become digitally high-pass filtered to improve its sharpness, or low-pass filtered for softening or to eliminate slanted "jaggies".

Plus and Minus

There are bunches of advantages to digital filters. First and foremost, a well designed digital filter is always "correct" and never needs "tuning". A digital filter could easily be adjusted over an incredibly wide range using software. Digital filters can often be swept without any nasty transients.

Special circuitry could be totally eliminated if the digital filtering gets done inside a stock microprocessor or a DSP digital signal processor.

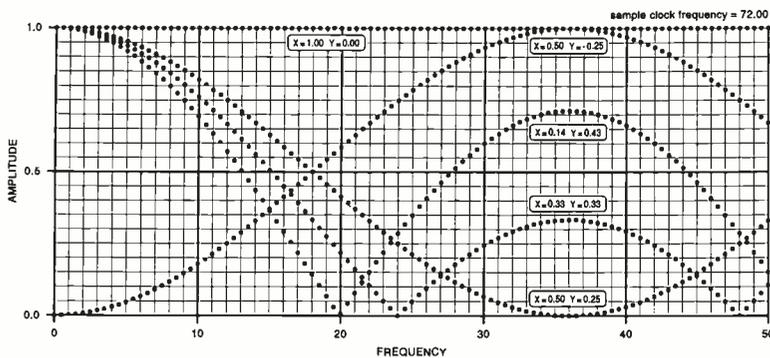


FIG. 3—HOW A TRISAMP'S FREQUENCY RESPONSE varies when its X and Y coefficients are changed.

Best of all, a digital filter can do certain tasks that end up being difficult or impossible when using classic analog designs. For one thing, in a sense, they can look forward and backward in time. That is, unlike capacitors and inductors, they can react to currents and voltages that are yet to happen; classic analog components can only react to things that have already occurred.

Examples here include "brick-wall" filters with extremely sharp cutoffs and linear-phase filters that attenuate a waveform's harmonics without any time-shifting distortion.

There are also disadvantages and limitations to digital filters. While they are a lot simpler than some may have you believe, they still are rather hard to understand.

You do already have to have your pile of numbers before you can filter them. Thus, A/D and D/A conversion might be needed in your system.

There is a really ugly property of digital filters called aliasing. If you sample any waveform less than twice per cycle, you might "fold over" and generate lower-frequency noise and artifacts. Very rarely, aliasing can be a valuable tool, one that lets you do digital mixing, downsampling, or a downconversion. But far more often, aliasing is a major nuisance that must be dealt with by pre-filtering.

Here's a rule to follow when working with digital filters: Input signals to a digital filter must get prefiltered so that zero energy exists above one-half of your sample frequency. That is, unless you have some really good reason to be doing otherwise!

The dynamic range of any digital filter is limited by several factors. Those

include your input and output word sizes, truncation errors, and any round-off errors.

Because you are often adding up very small differences between large values, the internal word size usually has to be much larger than that of the input or output. Thus, digital filters are much more suited to larger input signals than to very small ones.

Simpler digital filters apply integer math or fixed-point arithmetic. Such filters are faster and easier to implement, but have reduced dynamic range.

Exotic digital filters can use a full floating-point processing for all their math. While more accurate, floating-point filters often run much slower, either restricting the maximum input frequency or forcing you to move to non-real-time applications.

Finally, if your filter only works with a small number of samples, you might get into some ugly windowing problems. Softening the edges of a window or making sure that the edges happen where they don't cause problems are two

possible cures. Watch out for that windowing detail, or it will nail you every time.

Trisamp Building Blocks

My approach in the *Active Filter Cookbook* was to use a basic analog building block called a second-order section. No matter how exotic your filter response, all you really ended up with was a pile of those cascaded sections. And each section only had two possible adjustments—the cutoff frequency and its damping.

Let's try something similar here. I'll call our basic building block a "trisamp," and it is shown in Fig. 1. Just as you can use and cascade second order analog sections, you can use and cascade trisamps.

A trisamp gathers in three samples of a waveform. Which I will call "wuz," "is," and "wilby." It then scales them and adds them all together by using this fairly simple rule:

$$\text{output} = Y(\text{was}) + X(\text{is}) + Y(\text{wilby})$$

Since a digital filter is a linear type of "thingy," it should not matter what frequency or what phase we use for our analysis. Thus, we can apply just one frequency at a time to determine our overall response and arbitrarily pick an "is" phase of 90 degrees.

For a single-frequency sinewave input, your output should be a scaled amplitude clone of your input. The output will be larger or smaller than the input, depending on the values and signs of X and Y, and upon the ratio of your input frequency to the sample-rate clock.

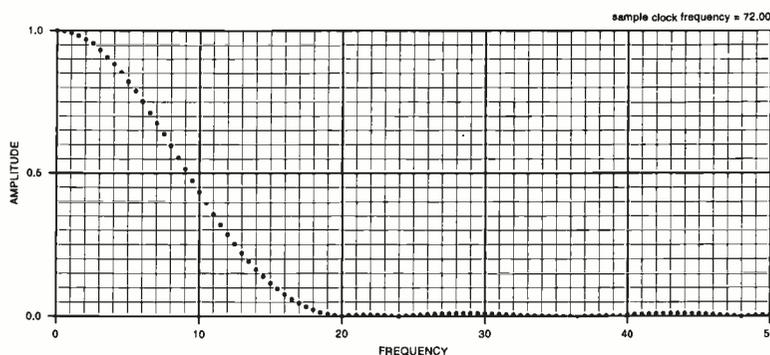


FIG. 4—A LOW-PASS FILTER built by cascading three trisamps. This is a "distortionless" or linear-phase filter that is extremely difficult to build using older analog techniques. To simplify your final design, using ordinary algebra easily reduces three cascaded trisamps into a single, seven-sample "septsamp." Additional samples improve response shape.

```

% PostScript triple cascaded trisamp digital filter designer v 2.04

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% For best results, improve with Guru Gonzo PostScript utilities. Enhanced and
% fully annotated version available as TRISAMP.PS on www.tinaja.com

% draw a graph:
110 350 translate 8 dup scale 0.03 setlinewidth 1 setlinecap gsave 0 0 moveto 51
{0 0 moveto 0 20 rlineto 1 0 translate} repeat stroke grestore gsave 0 0 moveto 21
{0 0 moveto 50 0 rlineto 0 1 translate} repeat stroke grestore 0.12 setlinewidth
gsave 3 { -0.5 0 moveto 50.5 0 rlineto 0 10 translate} repeat stroke grestore gsave
6 { 0 -0.5 moveto 0 20.5 rlineto 10 0 translate} repeat stroke grestore

/dot { newpath 0.150 0 360 arc fill } def % dot utility

/tripletrisamp {0 0.5 50 {/freq exch store 180 freq mul sampfreq 2 div div cos
coeffB mul 2 mul coeffA add /firsthold exch store firsthold abs 20 mul freq exch
dot 180 freq mul sampfreq 2 div div cos coeffD mul 2 mul coeffC add /secondhold
exch store secondhold abs 20 mul freq exch dot 180 freq mul sampfreq 2 div div
cos coeffF mul 2 mul coeffE add coeffC coeffD 2 mul add div /thirdhold exch store
thirdhold abs 20 mul freq exch dot firsthold secondhold mul thirdhold mul abs 20
mul freq exch dot} for} def

% //// demo - remove or alter before reuse. ////

/sampfreq 72 def % set sample clock frequency

/coeffA 2.0 4 div def % center of first trisamp
/coeffB 1.0 4 div def % pair
/coeffC 1.0 3 div def % center of second trisamp
/coeffD 1.0 3 div def % pair
/coeffE 1.0 7 div def % center of third trisamp
/coeffF 3.0 7 div def % pair

tripletrisamp showpage quit % do it and flaunt it

```

FIG. 5—THIS POSTSCRIPT TRIPLE TRISAMP exploration utility could make you an instant digital-filter-design expert. The code shown here can be easily expanded.

The X and Y values are known as coefficients. And while you could select different coefficients for “was” and “wilby,” that change would add or remove time delay to your response.

Forcing the coefficients for “was” and “wilby” to always be identical can give you the class of “distortionless” filters known as linear-phase filters. Those are especially significant for data communications applications, and can be extremely difficult to do when using the older and more traditional analog design methods.

Which leaves dealing with . . .

Negative Time?

So how *do* you find out who “wilby” is without a time-travel machine?

Simply look one stage previous in the shift register scheme of Fig. 2, or access one sample address earlier in a memory data bank. This is sort of the same way

any vertically delayed scope lets you look at the waveform edge you have just triggered on.

Let’s look at the responses we can expect from a trisamp as we vary its coefficients and the input frequency. Naturally, I prefer to use the superb PostScript general purpose computer language for this. I will use 72 clock samples per fundamental cycle.

Figure 3 shows you several trisamp responses. Positive Y values result in low-pass shapes and negative Y values result in band-pass shapes. Also, in general, the overall peak gain is set by the absolute value of the sum of X and Y. Gains near unity are often used to keep the results from getting too large or disappearing entirely.

For instance, a Y value of zero and an X value of one simply copies the peak value to the output for a flat or an all pass response. Next, consider Y = 0.25

and X = 0.50. At low frequencies, “wuz,” “is,” and “wilby” are nearly on top of each other, so they pretty much sum to 1.0 and give us nearly unity gain.

But at the frequency whose time period equals exactly 36 clock cycles, an interesting result happens. “Wuz” and “wilby” end up on negative cycle peaks, and “is” sits on a positive cycle peak. In other words, they sum to zero!

Other X and Y coefficients create the shapes shown. By themselves, those shapes may be interesting. But they aren’t all that useful. So, to get useful response shapes, you must cascade your trisamps.

Figure 4 shows a highly desirable linear-phase, low-pass filter made by cascading the three trisamps shown. Note the excellent stopband response. And the modest droop in the passband is fairly typical of linear-phase filters. Most important, there is zero excess phase shift to higher frequency harmonics. That property is very important in telecomm filters and for wave analysis.

Yes, you can easily re-graph this result in semi-log frequency-vs.-decibels for a more traditional-appearing, classic response plot. Among other features, that re-plot would make the stopband zeros more obvious.

Actually, nobody really cascades trisamps. Go through some simple algebra and you can quickly prove that any two cascaded trisamps are the same as a five-coefficient filter. And three cascaded trisamps are the same as a seven-coefficient filter. So you apply a pentsamp or a septisamp instead. All digital filtering amounts to is finding the right coefficients to use for the result you are after.

PostScript code to do a seven-coefficient filter made from three cascaded trisamps is shown in Fig. 5. You could easily use that routine to explore fancier digital-filter response shapes on your own. Just modify the coefficients with your favorite word processor or editor. Then send it to GhostScript or route it to almost any PostScript printer.

Lots more PostScript-as-language details are found on www.tinaja.com For an amazing range of applications, PostScript can completely blow away the more traditional general purpose computer languages.

Incidentally, more coefficients are normally chosen for fancier shapes.



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899 Presidential, Ste. 110
Richardson, TX 75081
(800) 864-1155

Dukane Ultrasonics
2900 Dukane Drive
St Charles, IL 60174
(708) 584-2300

Genesis Microchip
2111 Landings Drive
Mountain View, CA 94043
(415) 428-4277

Harris Semiconductor
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Melbourne, FL 32902
(407) 724-7000

ICT
2123 Ringwood Avenue
San Jose, CA 95131
(408) 434-0678

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San Diego, CA 92110
(619) 276-3421

Qualcomm Inc
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San Diego, CA 92121
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40G Commerce Way
Totowa, NJ 07511
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(800) 334-WALE

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21651 Tungsten Road
Euclid, OH 44117
(800) 531-1230

Typical hardware building-block chips offer four coefficients each. Those can get cascaded “wide” to handle twelve to sixteen or more coefficients. Or, they can be cascaded “deep” to handle the number of bits in a fixed-point word. Harris and Qualcomm are two big sources for these dedicated chips, but you can easily do the same thing with a PIC microprocessor.

I’ve been using digital filters as an important part of my magic-sinewave research. Magic sinewaves are my brand new way for simplifying and dramatically improving the efficiency of such products as variable-speed induction-motor drives, solar panels, and electric cars. You can find a lot more about them and all the new research opportunities they present on my Magic Sinewave shelf, which is in the www.tinaja.com reference library.

5SiMX Hard Drives

As we saw a couple of months or so ago, the Hewlett-Packard 5SiMX is an ideal mid-range PostScript laser printer,

one well suited to book-on-demand publishing. Its many features include genuine Adobe PostScript Level II, 24 pages-per-minute print speed, a page-flipping duplexer, 11 × 17 capability, refillable toner cartridges (offering excellent economics), 600 DPI resolution, and photo halftone enhancements; and all the service manuals and parts are readily available.

It also has, at least in theory, a hard disk.

Scant few printer users appreciate how absolutely crucial a local hard disk is for a PostScript printer (though Apple and QMS have had them for years). First, your hard disk lets you store lots of fonts. Second, it lets you stash all of your book-on-demand files so you’ll never have to tie up a network resending them. That same storage lets you do a run unattended for overnight BOD publishing.

The same goes in spades for often-used forms or patterns. When a diskless PostScript printer is first turned on, all of those needed font bitmaps have to be laboriously built up into a font cache.

Your first few printouts (and anything “new” after that) will always be very slow.

A local hard disk instead saves a font cache for you. There is normally not any speed-difference slowdown on your first few files.

Hard disks are also real useful for PostScript-as-language apps where they can serve as your primary I/O. They are also quite handy to log what is coming into your printer, to solve interface hassles, to convert formats, or to grab otherwise inaccessible data or commands. Once you have used a PostScript printer that offers a hard disk, it is unthinkable to ever again so much as walk through a room housing a printer that lacks one.

The only tiny 5SiMX problem is that the HP disk drive has been undeliverable—and it appears permanently so now as HP has gone completely out of the hard-drive business. Well, it turns out you can easily substitute your own hard drive—for as little as \$35—after you know and understand a few simple things.

Let’s excerpt some key info from the HP’s *LaserJet 5SiMX Developer’s Quick Reference Guide*:

“The standard 2½-inch ATA IDE disk drive interface is supported. (ATA stands for ‘AT Attachment, as in the IBM PC-AT bus. And IDE stands for Intelligent Drive Electronics.) This printer is designed to allow these drives to be mounted directly to the formatter board.

“The disk drive attaches to four standoffs. It is electrically connected via a ribbon cable.

“The Seagate ST9420AG is the disk that has been qualified to work in the LaserJet 5SiMX printer.”

The developer’s guide is available through HP Developers. My favorite source for custom cables is Redmond Cable. The oddball 2-millimeter bulk ribbon cable and connectors are sold by Digi-Key or Mouser (this is sometimes called a mini-IDE or “European” cable).

Bargain drives often show up in *Compu-Mart*, *Computer Hot Line*, and similar publications. Note that non-Seagate drives may be larger and have different mounting holes. Older and larger 3½-inch drives are most likely not worth the hassle. Besides needing excess supply current, their larger pinouts take a special adaptor.

Navigation Resources

Advanstar Communications

7500 Old Oak Blvd.
Cleveland, OH 44130
(800) 598-6008

GPS World

859 Willamette St.
Eugene, OR 97401
(503) 343-1200

Institute of Navigation

1800 Diagonal Rd., #480
Alexandria, VA 22314
(703) 683-7101

ITS World

859 Willamette Street
Eugene, OR 97401
(503) 343-1200

NASA Tech Briefs

41 E 42nd St., #921
New York, NY 10017
(212) 490-3999

Navtech Books & Software

2775 S Quincy St., #610
Arlington, VA 22206
(800) NAV-0885

SAE

400 Commonwealth Drive
Warrendale, PA 15096
(412) 776-4841

Trimble

585 N Mary Avenue
Sunnyvale, CA 94086
(408) 481-8000

The last three digits of the Seagate part number are apparently its size. In the case of the unit referenced above, it is 420 megabytes.

Be extremely careful when you experiment here on your own! Any crossed cable can destroy both your drive and the printer electronics. Do not attempt to interface a SCSI drive. Unless you know all about fancy and expensive IDE to SCSI conversions. And, of course, never hot swap an IDE drive! Always turn power off.

On your PostScript software side, the drive is called "%disk%." Fonts usually go in a fonts subdirectory. Although half a gig is vastly more storage than you are likely to need for this, there's one curious limitation: You are only allowed 1000 different files on your drive. Filenames can be one to 100-characters long. Nulls, backslashes, percents, end-of-file, and spaces are disallowed characters.

Again, much more on BOD in general can be found in my *Book-on-Demand Publishing Kit*.

Navigation Resources

I just got a flyer from Advanstar Communications on their brand new bookstore. This one focuses on GPS Global Positioning System and GIS Geographical Info System texts.

Because of that flyer, and since it's been a while, I thought we might summarize several of the better navigation info sources as this month's resource sidebar.

A good place to start is with the Navtech Bookstore. Then go on to those shows and publications from the

Institute of Navigation. Two important trade journals in this area are *GPS World* and *ITS World*; the latter focuses on "Intelligent Transportation Systems."

Finally, here's a reminder that Trimble has a great nav tutorial it calls *GPS—A Guide to the Next Utility*. Hot links to several useful GPS and nav sources are also found on www.tinaja.com.

New Tech Lit

New from Thomson-CSF, a new data book on their CCD Image Sensing Products. From Mitel comes an analog and digital Telecomm data book.

The PC1802 Stereo Enhancement Processor chip from ICT uses 3-D psychoacoustics to "spread out" the apparent source of stereo sounds. The new GMVLD10, from Genesis Microchip, is a real-time video-line doubler integrated circuit that is useful for de-interlacing. Uses for it include TV-to-monitor conversions and video walls.

The MIM Module from Clement Engineering can be useful for balloon telemetry and other remote sensing apps. Original jukebox manuals are sold by Western Reserve Games.

Some info on power ultrasonics appears in the *Waves* newsletter from

NEED HELP?

Phone or write all your US Tech Musings questions to:

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Web page: <http://www.tinaja.com>

Dukane. Bunches of traditional pipe-organ building info gets sold by the American Institute of Organbuilders, who offer various newsletters and conferences.

Two unusual glass topics: Glass paints are newly available through Wale Apparatus, while Foturan is a new photo-etchable glass product line from the Schott folks.

That long unclaimed \$10,000 prize for anybody able to convincingly demonstrate dowsing techniques to locate a buried water pipe has just been upsized to \$640,000. Contact www.randi.com for details. There's more on pseudoscience bashing in general on www.tinaja.com

For more on the fundamentals of digital integrated circuits, read my *CMOS Cookbook* and *TTL Cookbook*, either by themselves or as part of my bargain *Lancaster Classics Library*, per my nearby Synergetics ad.

As usual, many of the mentioned resources appear in our Names & Numbers and Navigation-Resources sidebars. A reminder that a no charge technical helpline is available per the Need Help box. Funding and time constraints strictly limit that service to U.S. callers only. Let's hear from you! **EN**



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Troubleshooting VCR Tape Path Alignment

WHEN EVERYTHING IS SET UP RIGHT IN A WELL-DESIGNED VCR, IT WILL RECORD AND PLAYBACK CLEAR, SHARP PICTURES. BUT EVEN MINOR MISADJUSTMENTS IN THE TAPE PATH COULD SEVERELY IMPACT THE QUALITY OF THE

video or the audio, or both. If there are severe misadjustments in the tape path, the tape itself can be damaged.

Figure 1 diagrams the tape path in a Hitachi VHS VCR. It is typical of, though not identical to, the path that VHS recording tape follows in many modern VCRs. The five key areas in the tape path that require adjustment to ensure that the tape travels in the proper vertical plane are shown in the diagram. As we go on we will describe each adjustment point and its importance in a properly aligned tape path.

Reel Table Height

The first tape-path point in Fig. 1 is where the reel-table height is set. That setting determines the height of the tape as it is taken up or supplied from either the supply or take-up reel tables. If either table height is misadjusted, making the tape lower or higher than normal, the edge of the tape can be damaged. Figure 2 shows how a misadjustment there can cause tape curling. In that example the reel table is too high, affecting the height of the tape at the entry point to the guide. The result is tape curling at the top edge of the tape, which can permanently destroy or distort the audio or control tracks on the tape. As shown in Fig. 3, those tracks are at the top and bottom edges of the tape. That kind of problem shows up as dis-

torted audio, with level changes; intermittent speed changes; or tracking problems.

Another problem caused by improper reel-table height is that it could cause the tape to be rewound into its VHS cassette improperly. That rewinding can

cause the tape to bind, and in some instances stretch, causing symptoms similar to those of tape-edge damage.

Tape Tension

Tape tension is the applied force of the tape at some particular point along the tape path of the VCR. In VHS VCRs, tape tension is regulated to insure video signal interchangeability between VCRs. Incorrect tape tension produces a number of different playback problems. Those problems show up as:

- **Tape Skew**—flagging or bending of the picture at the top of the viewing

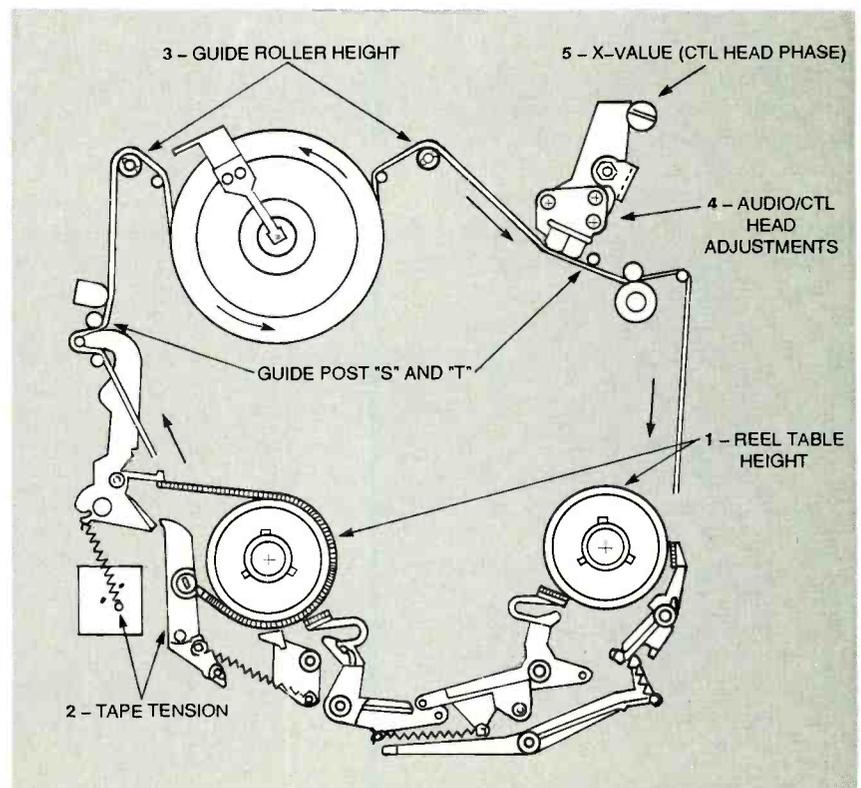


FIG. 1—THE VHS TAPE PATH shown here is from a Hitachi unit, but it is common to many VHS VCR's. Note the five major adjustment points.

*FROM HITACHI Hi-lite/Hitachi Home Electronics (America) Inc. Suwanee, GA

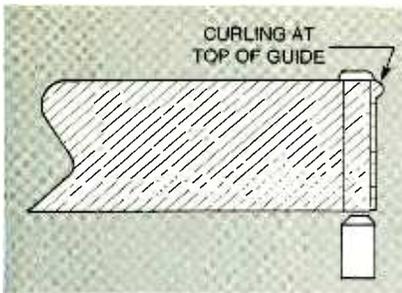


FIG. 2—TAPE CURLING AT THE TOP OF the tape guide can be caused by a misadjusted reel-table height. If severe, it can physically damage the tape.

screen. That vertical bending is caused by horizontal time-base errors in the horizontal-sync pulses on the tape. Correct tape tension reduces horizontal time-base errors.

- **Intermittent Blue Screen**—triggered by the loss or excessive distortion of the playback video-sync signals. System-control microprocessors often monitor the sync signal, sending control codes to the character generator, which activates the blue screen whenever abnormalities are detected.

- **Upper Cylinder, Tape-Guide Damage**—severe, excessive tape tension can actually damage the upper cylinder and tape guides, causing surface scarring or excessive head wear.

Proper tape tension is clearly one adjustment that must not be overlooked. It is maintained throughout the tape path by a tension band, which is wound around the supply-reel table that continuously controls the braking force applied to the table. That braking force provides a variable resistance to the rotation of the supply reel when the tape is being withdrawn from the cassette-supply hub. To change the braking

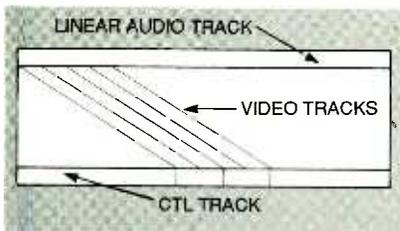


FIG. 3—THE AUDIO SIGNAL SITS ALONG the top edge of the VHS tape. Control signals are placed along the bottom edge.

force, a tension band is connected to a tension-arm assembly using a pole that is in continuous contact with the tape as shown in Fig. 4. The tape itself determines the pole position relative to the tape tension at any given point in time. As the tape is pulled from the supply-

reel table with more (or less) force, the pole position changes in proportion to the force, and the band around the supply-reel table alternately loosens (with increased tape-pull force) or tightens (with decreased tape-pull force) to maintain a constant back tension (resistance) against the tape.

Guide Rollers

Figure 5 shows two additional components that play an important part in determining the position of the tape as it travels through the tape path. Since no two VCRs have precisely the same mechanical path for tape travel, the supply and take-up guide-roller heights are adjustable to maintain interchangeability when playing back prerecorded videocassettes. The guide rollers determine the height of the tape at the entrance and exit of the video-drum assembly, and control the tape travel across its surface. That ensures the correct positioning of the video head with respect to the video signals recorded on the tape (particularly the proper placement of the video-sync signals), and the point at which the video heads were switched from CH1 to CH2 during the initial recording.

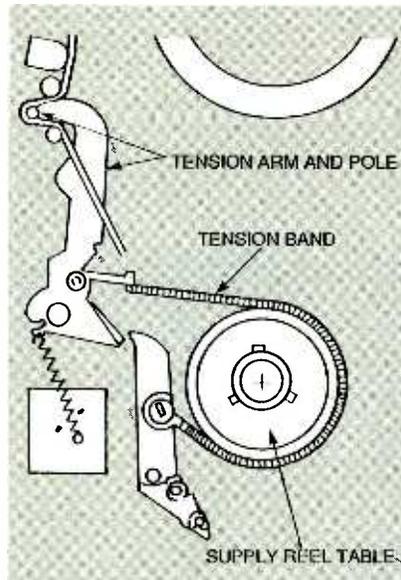


FIG. 4—TAPE TENSION MECHANICS are illustrated here. The tension band does most of the work.

Figure 6 shows what happens if a supply-guide roller is misadjusted. Note the noise bar that appears at the top of the screen. The particular guide roller that is misadjusted, and the degree of misadjustment, determines the number of noise bars and where they appear on

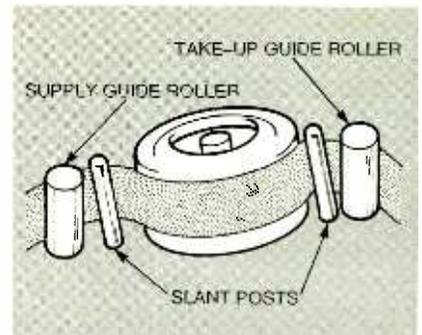


FIG. 5—TWO GUIDE ROLLERS—one before the video-drum assembly, one after—determine the tape position as it travels across the video heads.

the screen. A misadjusted guide roller can also cause tape curling, which results in distorted audio and distorted picture (noise bars, vertical jitter, and intermittent blue screen).

ACE Head

The ACE-head assembly is shown in Fig. 7. It is comprised of three heads that together support the audio and servo functions of the VCR. Those are:

- **Audio Erase Head**—a high-frequency AC bias current flows through the erase head to remove any previously recorded audio signal.
- **Linear Audio Head**—records and plays back the linear audio signal.
- **Control Track Head**—records a 30-kHz signal onto the tape to form a video-head reference. When a tape is played back, the video-head phase is aligned with respect to that recorded control signal.

The ACE head is adjusted to assure proper playback of the linear audio signal and to insure proper tracking when playing back prerecorded tapes. When adjusting the ACE head assembly, two of

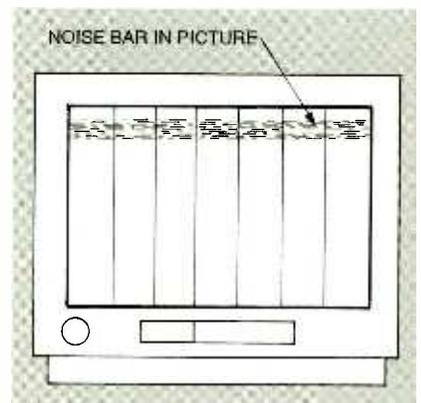


FIG. 6—THE NOISE BAR THAT APPEARS in the picture can be caused by a misadjusted guide roller.

continued on page 72 **69**

Generating Laser-Light Patterns

THIS MONTH, WE ARE GOING TO TURN OUR ATTENTION TO THE WORLD OF GEOMETRIC PATTERNS AND DESIGNS. THE LASER MARKET IS TEEMING WITH EQUIPMENT, RANGING FROM SIMPLE X-Y AXIS UNITS AND SCANNERS TO

elaborate, computerized professional controllers. All are designed to manipulate one or more laser beams into designs, patterns, moving artwork, lettering, or even sheets of light.

Such equipment is remarkable in terms of what it does, but costs start in the \$100 range for the most basic set-up and go up to \$15,000 and more for highly sophisticated machines.

While such specialized professional equipment is wonderful to work with, it is overkill for our experimentation purposes, and its cost puts it out of reach for many. But that doesn't mean that we can't experiment with laser special effects. Let's take a look at some of the simple and inexpensive equipment that can be built and methods that can be used to produce many of the same effects as the commercial units.

Simple Pattern Generators

To start, let's re-visit a set-up first discussed in the July 1996 installment of this column, and shown in Fig. 1. Mount a spring to a stand, as illustrated there, and attach a 1-inch-square piece of Mylar or top-surface mirror to the spring's free end. That set-up is the basis for several different simple pattern generators.

One tip when working with springs is that the action can be adjusted by expanding or contracting the coil. As a

general rule, a spring becomes springier when stretched. Use that principle to control the amount of reaction to touch or vibration.

Once the set-up is assembled, aim your laser so the beam reflects off the Mylar or mirror onto a flat, light-colored surface, and then give the spring a tap. That tap will make the spring oscillate, and the beam will follow suit. Thanks to the persistence-of-vision characteristics of the human eye, the

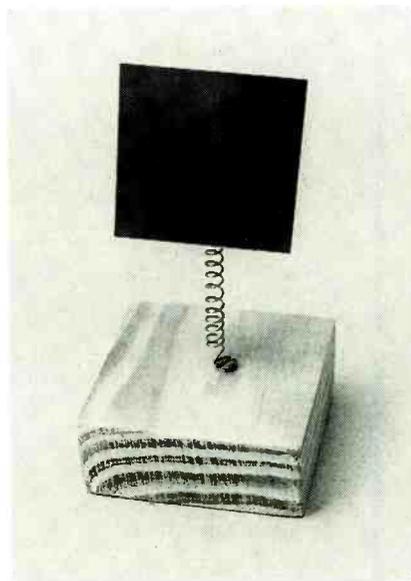


FIG. 1—A SQUARE MYLAR REFLECTOR attached to a spring that is anchored to a block of wood is one of the most basic laser-light reflectors.

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rapid movement of the spot generates random patterns and designs on the surface.

Repeat that step several times. Note that the patterns are never exactly the same twice. A blast of air or strong vibration can also vibrate the spring and create new light effects. Experiment with different forces and make note of what happens.

Electronic Pattern Generator

If you set up a small gear-reduction motor, rigged with an arm (say, a nail, for example) that will gently nudge the spring on each revolution, you'll have a way to produce more repeatable patterns for longer periods of time. The photo in Fig. 2 shows one way that can be done.

An electromagnet or solenoid can also be used to pulse the spring and move the reflector. Those devices can be driven from the output of an electronic timer that is also used to control the frequency of the pulse. Figure 3 shows a suitable circuit for a simple timer.

For more dramatic effects, use a dual timer, like the one shown in Fig. 4. In that circuit, first one electromagnet, then the other, is activated, and the sequence repeats. If the two electromagnets are placed at right angles to each other, a north-south, east-west movement can be established. That movement can produce some very interesting designs, especially if you vary the oscillation rate by changing the capacitance and resistance values.

Motorized Pattern Generators

Motors and mirrors make an excellent combination for generating graphics.

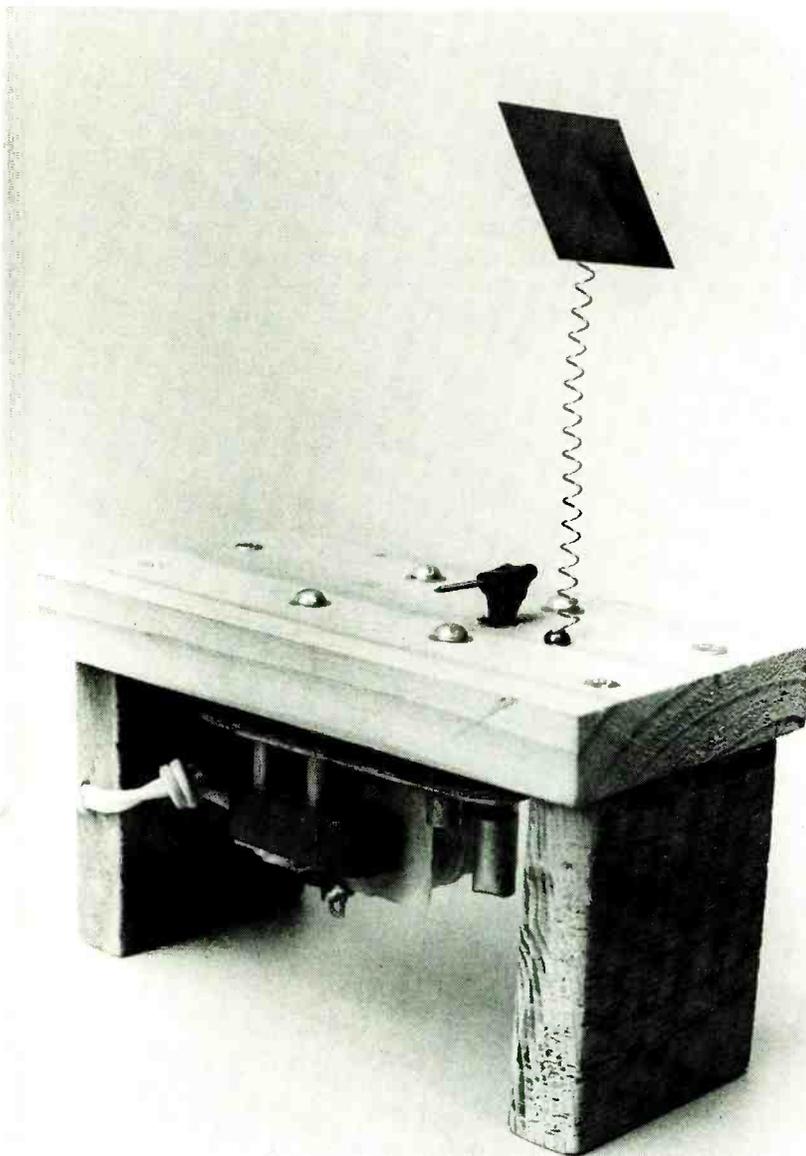


FIG. 2—FOR REPETITIVE VIBRATIONS, this simple set-up works well. A small gear-reduction motor rotates a nail, which strikes the spring one time each revolution. That rotation creates a repetitive movement in the reflector.

Attach reflective surfaces to the shafts of the motors. Then arrange the assemblies at various angles to each other. Now direct the laser beam between the mirrors and onto a screen. As the motors turn the mirrors, additional angle changes occur that vary the pattern.

Figure 5a shows a variation of the circuit in Fig. 4 that can be used to control a pair of motors. When the motors are connected to the circuit as shown in Fig. 5b, it will turn the individual motors on and off. If, on the other hand, you use the arrangement shown in Fig. 5c to control a single motor, it will make that motor first rotate in one direction and

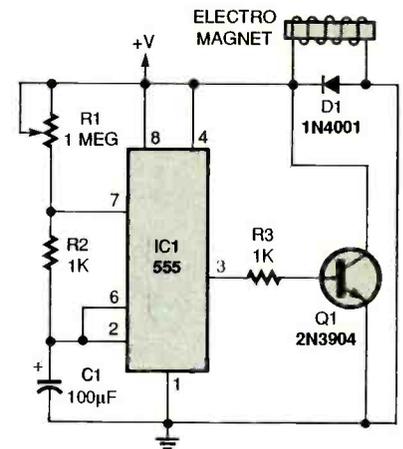


FIG. 3—A SIMPLE TIMER built around a 555 gives you a switching electromagnet to use to create laser-light patterns.

then the other. That set-up has all kinds of useful applications.

If you want to add yet another variable, you can provide a speed control by connecting a 5000-ohm potentiometer in series with the motor and power supply. Another variation would be to replace the flat mirrors with either convex or concave surfaces. One last area to consider is reflecting the laser beam off liquid surfaces such as water, oil, paint, etc. Different beam angles and vibrations of the substance being used as the

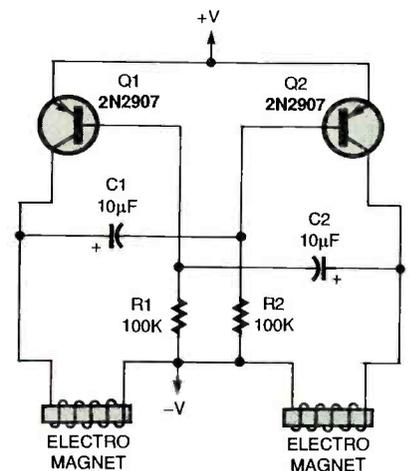


FIG. 4—IF THE ELECTROMAGNETS in this dual-timer circuit are arranged perpendicular to each other, a north-south, east-west motion can be established.

reflector can produce some delightful and interesting results.

It is obvious that a nearly endless variety of effects could be produced by making minor or more extensive

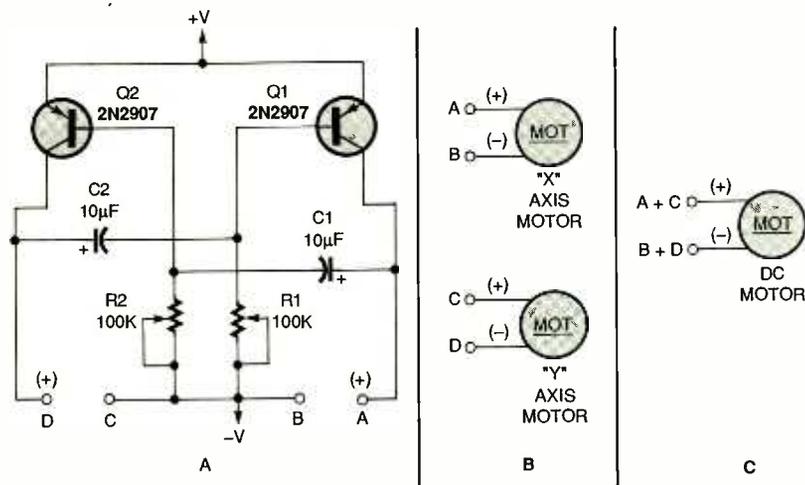


FIG. 5—THE MOTOR-CONTROL CIRCUIT (A) can be used to alternately turn two motors on or off (B). It can also be used to make one motor turn first in one direction and then the other (C).

changes to the basic set-up. Spend some time experimenting with the ideas presented, as doing so is a valuable source of knowledge.

Holiday and Other Displays

So, aside from special effects at rock concerts, what practical applications are there for what we have learned? Well, how about using lasers to create holiday displays that would be the talk of the neighborhood. Holidays, such as Christmas, Halloween, and Independence Day all lend themselves to the special effects lasers could produce. For

example, use mirrors, lenses, fiber optics, and such to uniquely personalize Christmas trees and other decorations with stunning light shows. The displays can be stationary or moving. They could spell out a holiday message. You are only limited by your imagination and the complexity of your design. If a PC is available, try setting up a program to control both the optics and mechanics for a variety of unusual results.

Halloween offers an endless opportunity for creativity. Just imagine the selection of spooky displays you could build around your laser. A spectacular demon-

stration for the Fourth of July could be assembled with the help of mirrors and motors to simulate fireworks. Let your imagination loose and when you do come up with a great idea, put it down on paper and send it to **Electronics Now**, Laser-Experiments Editor, 500 Bi-County Blvd., Farmingdale, NY 11735, or simply e-mail to lartronics@aol.com.

While on the subject of gaining attention, why not take a look at the possibilities for advertising. A swirling, pulsating light show projected on a billboard or a showroom ceiling or wall will immediately attract people passing by. In addition to the movement, there is something about the color and quality of the red light from a helium-neon laser that is difficult to ignore. The collimation not only makes the light bright, but also gives the beam and the surfaces it comes in contact with a shimmering effect that is hard to describe. For whatever reason, the experience is visually pleasant for most people. **EN**

SERVICING

continued from page 69

the adjustments affect the way the tape travels across the tape path. These are the tilt and height adjustments.

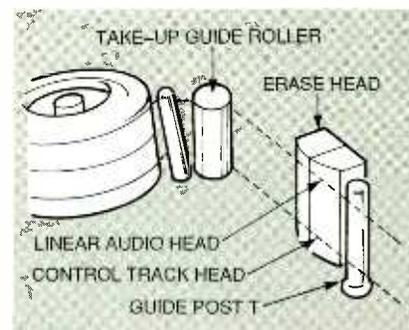
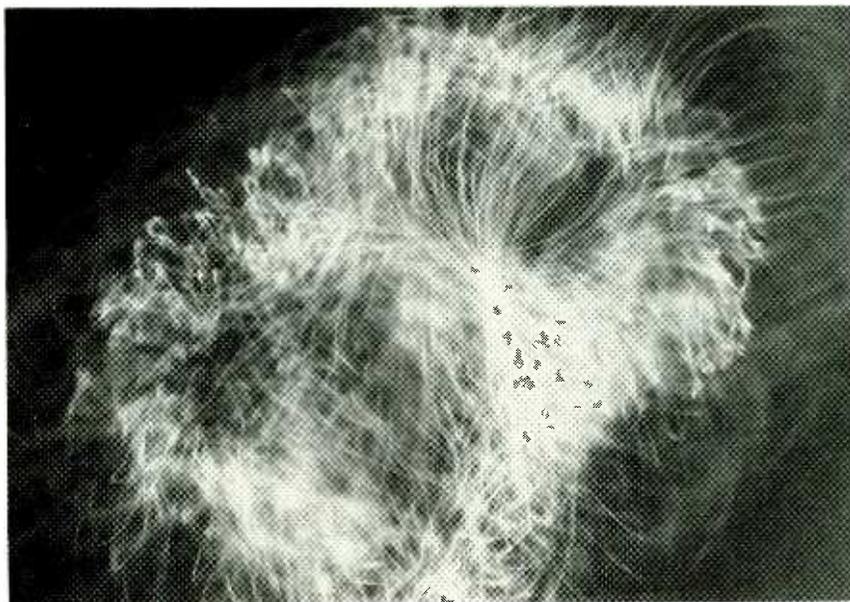


FIG. 7—ACE-HEAD ASSEMBLY is composed of three separate heads—audio erase, linear audio, and control track.

X-Value

The X-value adjustment, also known as the CTL head phase, or tape-interchangeability adjustment, is used to set the position (horizontally) of the ACE head. It insures that the recorded video signal and control-signal phase relationship is maintained when playing back tapes from different VCRs. You can be sure that tracking linearity is correct when the X-value is properly set. **EN**



THIS IS ONE EXAMPLE of the kinds of light patterns that you can create using the information in this article.

EQUIPMENT REPORTS

continued from page 18

pressure or you can enter a new user. Each new user gets their own password and set of records. If you want, you can set the upper and lower pressure limits for each measurement—the smaller the range, the quicker each measurement can be made.

With everything connected and the software running, you simply follow software prompts to wrap the cuff around your arm, tighten the air valve on the bulb, start pumping, stop pumping and wait, and then to loosen the valve and release the air. The process takes about 30 seconds. All results appear on-screen and can be saved or printed.

The DynaPulse measures blood pressure in much the same way as a physician does. The inflatable cuff presses on the artery in your arm to the point where blood stops flowing. Then, as pressure is released, blood starts flowing at some point. At that point, the blood swirls in a turbulent flow causing a sound a doctor can hear with a stethoscope, and variations in pressure that DynaPulse can detect. The point where blood starts to flow is measured as the higher pressure point (systolic). At some point as pressure is released, the turbulence ceases; that's the lower pressure point (diastolic).

While it will not (and should not) replace a physician, DynaPulse is excellent for medical screenings by qualified personnel, or for home use to keep track of your blood pressure between doctor's visits. It also makes it very easy to store your results where they will never get lost. You can display long-term trends to monitor the effects of diet, exercise, medication, and so on (again, any diet or exercise regimen should first be discussed with and approved by your physician). Whether you're keeping track of just yourself, your whole family, or an entire organization, the DynaPulse 200M simplifies the task of taking and storing blood-pressure readings. **EN**



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Microphone Basics

SOUND IS GENERATED THROUGH A SPECIFIC MECHANICAL PROCESS. THAT IS, SOME PHYSICAL DEVICE MOVES OR VIBRATES, IN TURN MOVING THE AIR AROUND IT. ONE SIMPLE EXAMPLE IS A TUNING FORK. IF YOU HIT THE TUNING FORK

with a hammer (see Fig. 1), the fork vibrates at one specific frequency determined by its size and shape. The vibrations of the fork move the air around it. When those movements reach your ear, they are converted into electrical energy and sent to your brain to be processed and interpreted. (Of course, there is a lot more going on here than what we've just outlined; but, for our purposes, this simplified explanation will suffice).

Well, that process could also be used to describe how a microphone works. Like the ear, all microphones are sound conversion devices—they take sound and change it into electrical energy. There are three basic steps in this process:

1. Sound waves move the diaphragm inside the microphone.
2. The voice coil also moves, since it is attached to the diaphragm.
3. When the voice-coil moves, electrical energy is generated in the coil since it is located inside the microphone's magnet structure (magnet and magnetic housing).

The kind of microphone just described, shown in Fig. 2, is a dynamic or moving-coil type. The sound wave that reaches the microphone must be strong enough (or, rather, loud enough) to move the mass of the diaphragm and the coil assembly. That type of microphone works well, but does have some limita-

tions. It usually generates a small peak, sometimes called presence, somewhere between 2 and 5 kHz. Extremely-low and extremely-high frequencies can also give dynamic microphones some trouble. However, dynamic microphones are very durable and do not require any special handling. That's why they are so commonly used.

The amount of electrical energy that a microphone can put out partly depends on the amount of acoustical energy that reaches its transducer. In general, the louder the sound, the greater the electrical energy the microphone will produce, but there are limiting factors—the maximum possible movement of the voice coil for one.

Sound that we hear is usually measured in dB SPL (sound pressure level). That measurement ranges from 25-dB SPL (the level in a quiet broadcasting studio for recording music) to 140-dB SPL (a 50-HP siren). An average full symphony or orchestra has a dynamic

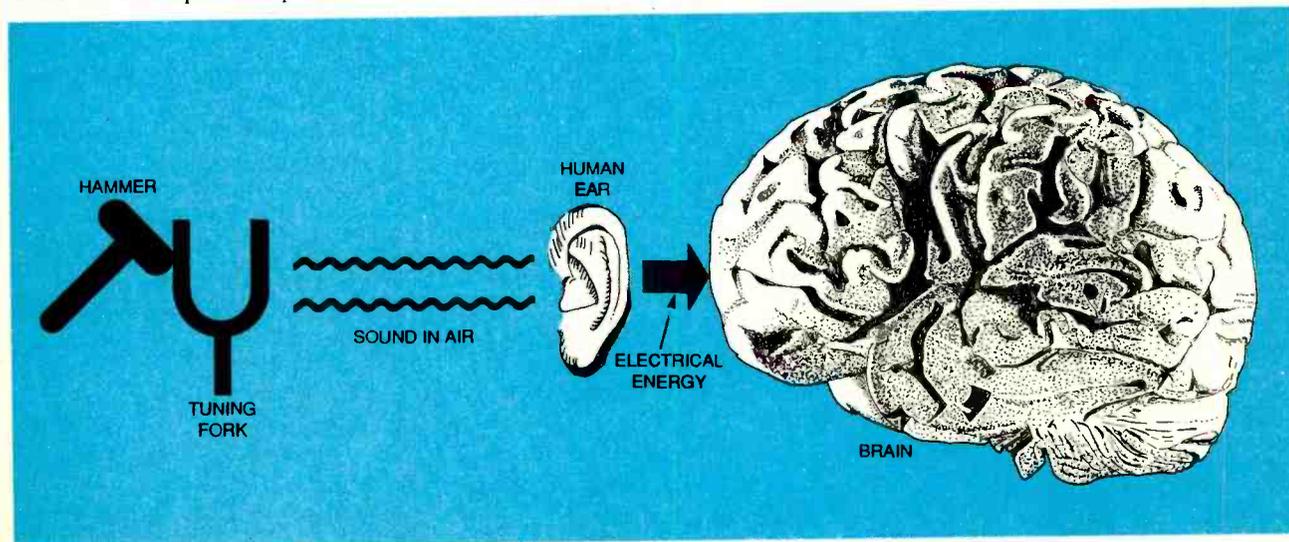


FIG. 1—HOW SOUND IS GENERATED. Striking a tuning fork is the method illustrated here.

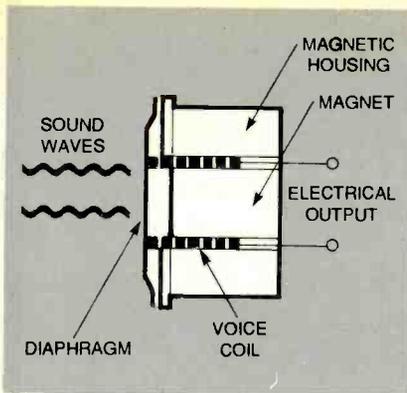


FIG. 2—MICROPHONES CONVERT sound waves into electrical signals.

range of 20 to 100 dB. The human ear has a dynamic range of about 120 dB, which is a ratio of a trillion to one. Analog recording has a 60-dB range (a million to one). Digital recording has a range of 90 dB (a billion to one).

As you can see from the above, the human ear is a very fine instrument indeed and should be treated with respect. Therefore, a microphone that can convert the air movement into an electrical signal within the very large dynamic range of the ear has a difficult job, at best.

Microphone Efficiency

Microphones work best when they are positioned as close as possible to the sound-generating source. As shown in Fig. 3, the voltage produced by a microphone falls off with the inverse square of the distance. Put another way, the voltage the microphone produces increases geometrically as the distance from the sound source decreases. However, there is a limit. If the microphone is too close to the sound source, there is a proximity effect that causes the low frequencies to

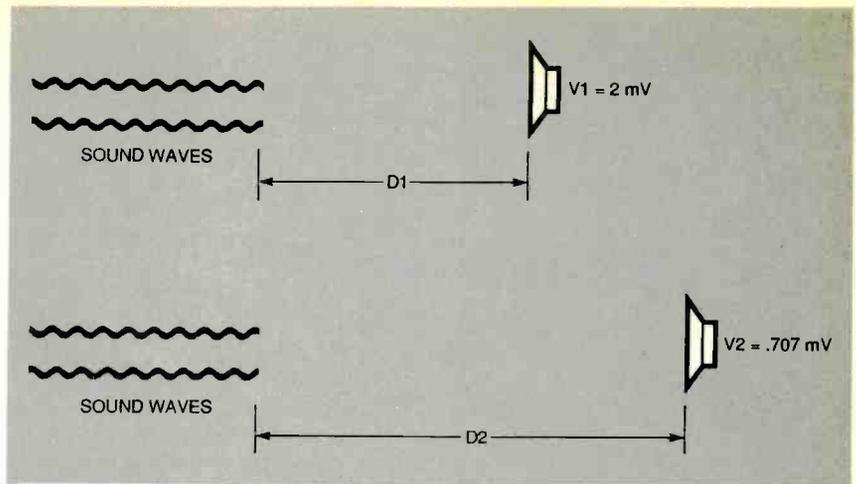


FIG. 3—A MICROPHONE'S OUTPUT FALLS OFF as it gets farther away from the source of the sound.

have a greater build-up than the high frequencies.

It is important to realize that microphones are never 100% efficient (their precise efficiency is not important to this discussion), and many factors come into play to reduce efficiency still further. For example, even temperature and humidity are important factors in the sound-reproduction process. That is one reason why studio recording is ordinarily very uniform, while remote recording can be quite variable. It is also why something that worked once might not seem right at another time. Most of those problems can be solved, but microphone users need to be aware that they can and do occur.

Types of Microphones

There are several different types of microphones. The first and most common is the dynamic microphone that we have been talking about. It has a small diaphragm with a coil of magnet wire

attached to it (see Fig. 4) that sits in the field of a permanent magnet.

The electret condenser type is the next most popular in today's marketplace. It is a permanently charged capacitor type with an FET amplifier built in. It is shown in Fig. 5.

Another type of microphones is the capacitor type; it is the forerunner of the electret type. Its major drawback is that it needs a power supply to charge its plates. An RF capacitor microphone is another quality way to convert sound waves into an electrical signal.

Acoustical Characteristics

Next, let's look at the acoustical characteristics of microphones, in order of their popularity. Figures 6, 7, and 8 are polar diagrams that show the pickup patterns of various microphone varieties. All three have some common elements and all are for a 1-kHz signal. At other frequencies the patterns might be different.

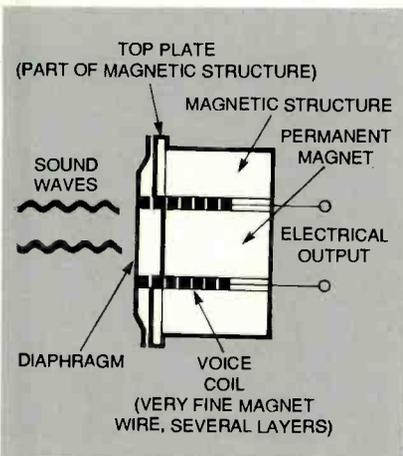


FIG. 4—THE BASIC DYNAMIC MICROPHONE. It is probably the most commonly used variety.

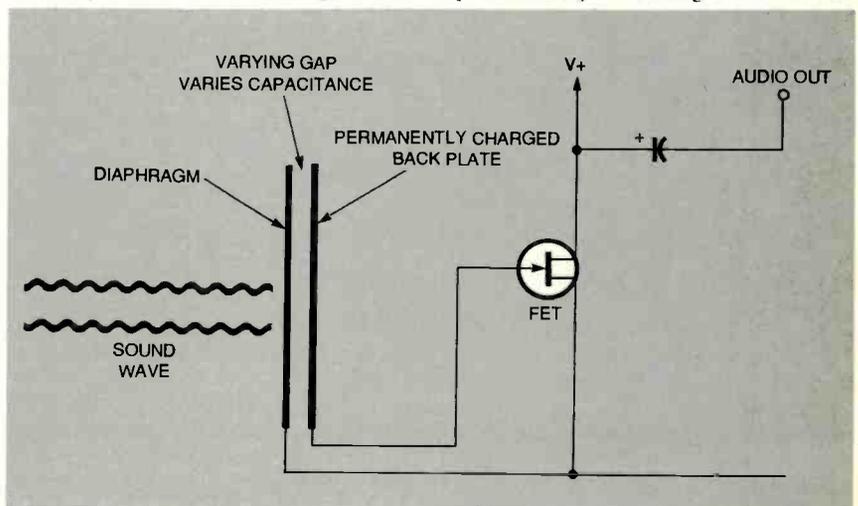
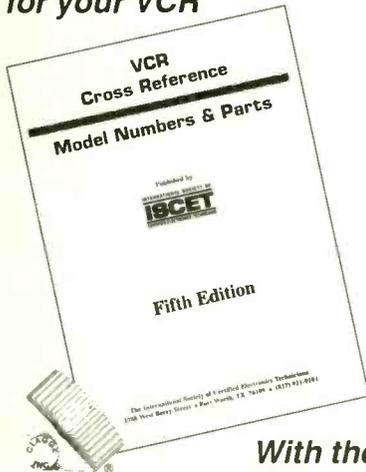


FIG. 5—AN ELECTRET CONDENSER MICROPHONE features a built-in FET amplifier.

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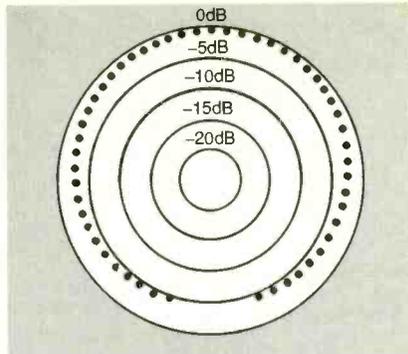


FIG. 6—A MICROPHONE WITH AN OMNI-DIRECTIONAL pattern like this one picks up sounds from all directions.

Every microphone has its own polar pattern. The manufacturer will generally supply it with the microphone, or the information might be in the catalog or other literature. The key to selecting the right microphone is to know which pattern is the correct one to use for a particular application.

The most common type is the omnidirectional. As its name implies, an omnidirectional microphone receives the acoustical waves in a pattern that is equal all around in a circular fashion. Note that the plot in Fig. 6 shows that the pickup in the rear does have some loss, but that loss is small enough to ignore.

The next type of pickup pattern is the cardioid. It has better pick-up from the front of the microphone than from the rear, as shown in Fig 7. That type of pick-up is very popular for live performances. That's because it greatly reduces the chance of acoustical feedback (although it is far from the total answer to that common problem).

The hyper-cardioid/super-cardioid microphone has some features of the cardioid microphone, but the pickup pattern is even more pronounced (see

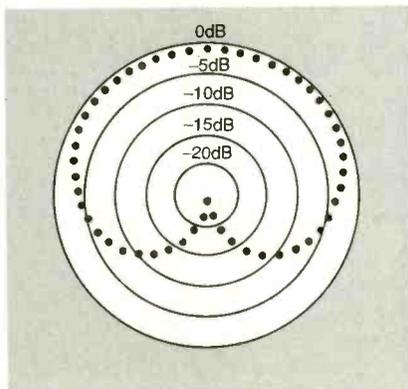


FIG. 7—A CARDIOID PICKUP PATTERN reduces the likelihood of acoustic feedback.

Fig. 8). Though that microphone is useful where feedback is likely to be a real problem, one drawback is that it might have too narrow a pickup pattern for some applications.

The last type of microphone we will discuss is the gun/interference tube. It is used to pick up sounds at a distance. That microphone has some special uses, especially in electronic newsgathering and in film and TV production, to pick up dialogue where a wireless microphone is impossible to use for some technical reason. While we have not shown a polar plot for that type, obviously, they are highly directional.

It is important to remember that

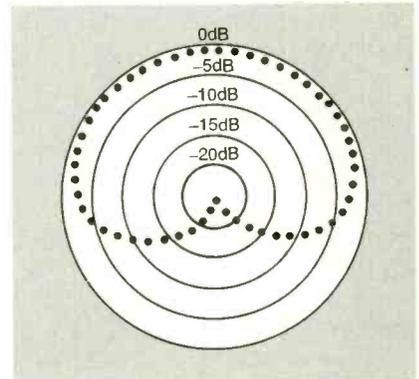


FIG. 8—WHEN FEEDBACK PROBLEMS are severe, try a hyper-cardioid type that delivers the polar pattern shown here.

there is no one microphone that can solve all acoustic problems. You must try different ones in different situations. After some practice, you will have a good understanding of what works for what situation. **EN**



IP Addressing and HTML Coding

THERE WERE SEVERAL MISLEADING AND INCORRECT STATEMENTS IN MY COLUMN ON INTERNET RESOURCES (AUGUST 1996). I THINK THAT THE TOPICS ARE IMPORTANT AND INTERESTING ENOUGH THAT WE'LL REVISIT THEM IN

somewhat greater depth for our discussion this month.

The first problem was my statement, "Thus, a textual address like jkh@acm.org eventually gets resolved to a numeric address like 127.0.0.1." Actually, the numeric address is a machine address, not some sort of user alias. As Lou Sortman pointed out, "There is a mapping between IP addresses and domain (host) names, but the user part of an e-mail address is resolved by the Mail Transfer Agent on the referenced host (or Mail eXchanger) and has nothing at all to do with any part of the IP address." Thanks also to Ron Dozier for information in this area.

Lou also clarified some details of where HTTP ends and TCP begins: "In the HTTP protocol, the client issues a request to the server and the server responds with the status, a header (which you described with the HEAD command), and any requested data (if applicable). Your description added two extra parts (client initiates "transfer" and server acknowledges the connection). Those are not part of HTTP. They are part of the transport protocol (TCP on the Internet)."

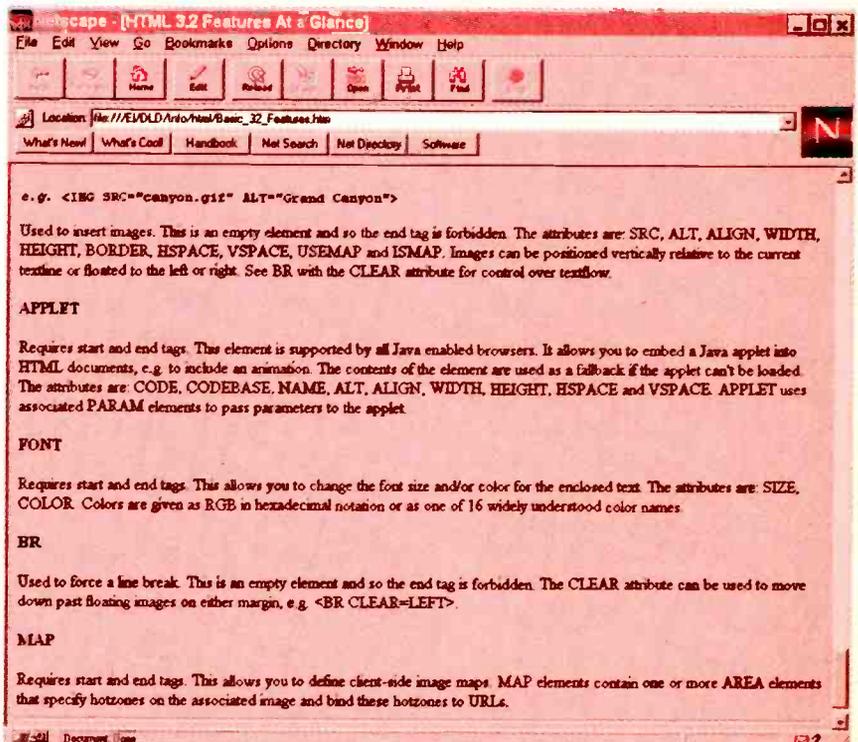
Regarding CGI (Common Gateway Interface), Lou stated, "CGI programs can be accessed with the GET method as well as the POST method. You specified that only the POST method can be

used. Later, you say that mostly what is transferred with the GET method is simple HTML files. Statistically, that is probably true, but it is also used quite a lot for other file types (sound files, images, etc.) and even CGI programs."

Lou also disagreed with my assessment of CGI: "CGI is not an awkward

hack. It is the most portable way of handling CGI programs on differing operating systems and written in differing languages, including interpreted ones such as Perl and the Bourne shell. There is a place for more efficient schemes for executing code on the server, but there are portability and resource consumption issues that would make CGI a better solution in many cases."

I agree that CGI has the virtue of portability. However, it lacks elegance and performance. As the Microsoft steamroller overtakes Internet technology, I think we'll see the company's direct-access Internet Server Application Pro-



THE HTML 3.2 SPECIFICATION adds support for Java Applets, and several new tags for specifying text formatting. HTML 4.0 should be out by the end of the year.

gramming Interface (ISAPI) become much more widely used than CGI. And even if MS were to drop dead tomorrow, other vendors (e.g., Netscape) have comparable solutions.

Lou also disagreed with my assessment of HTML. "HTML was intended to be platform independent. It was quite intentional that there were no font or color tags in the original spec. Leaving the precise manner of interpreting the document content and markup up to the browser was a good thing. The reason that people have problems with documents looking different on different browsers is that they decided that they wanted to do things that HTML was never intended for. HTML is a markup language. It is not a page description language. Ask Don Lancaster (the world's biggest PostScript proponent) about the difference. There may be a need for an open page-description language with hypertext capabilities on the WWW, but the problems that you cite are not shortcomings of HTML."

Here Lou and I have a major disagreement. I'm certainly aware of the distinction between a markup language and a page-description language. The problem is that HTML is rapidly becoming a page-description language.

HTML and SGML

HTML is an application of SGML (Standard Generalized Markup Language, defined by ISO Standard 8879:1986). SGML purposely separates document content from document structure and document formatting. An SGML "document" actually has two components: the document itself, and a Document Type Definition (DTD). The DTD is like a style sheet (in the MS Word sense). In a pure SGML document, the document has no direct formatting. Nothing is ever marked bold or italic; fonts are not specified by name, nor are colors; nor is any type of layout information (e.g., tab stops and line spacing) embedded in the document. The document never has anything but content and tags specifying format and structure. The tags are interpreted according to the DTD associated with the document.

In that way, the DTD can change without changing the underlying document. Thus, the same document can be presented in several different ways sim-

ply by associating the document with different DTDs.

That may seem like an esoteric feature, but it's not. For example, a big problem in creating software documentation is reuse of material. There are printed manuals and on-line, hypertext documents. Often, they share much of the basic content. But it is extremely rare for them to have a strict, two-way, one-for-one correspondence. The on-line stuff invariably needs something that the manual does not, and *vice versa*. Conversely, the manual invariably has stuff that you don't want in the online version, and *vice versa*. Similar types of problems are pervasive throughout every aspect of electronic publishing

LISTING 1—TEMPLATE FOR DELPHI COMMAND-LINE UTILITY

```
program Test;  
{ $APPTYPE CONSOLE }  
begin  
  writeln('Howdy, world...')  
end.
```

The problem with Web pages that look different on different browsers is that the details of the HTML DTD are interpreted differently by different browsers. Netscape interprets the DTD one way, Microsoft another, and so on. If it were just a question of fonts and colors, the graphics designers might be unhappy, but things would still work. It's when Microsoft and Netscape each goes off and defines new tags to accomplish special feats (e.g., frames, tables, embedded applications, and so on) that both page designers and end users end up suffering.

Some of the latest format-related HTML features (e.g., font tags, color tags, and cascading style sheets) in effect embed the DTD directly within the document, and that is directly contrary to both the letter and the spirit of SGML.

It's also true that some of the very oldest HTML tags do the same things. For example, HTML has tags for directly marking text as boldface, , and italic, <I>. However, directly marking text in any fashion is counter to the SGML model. There are more general tags that are usually, but not necessarily, rendered as bold and italic: and , respectively. Those are the correct tags to use.

Theory and Practice

Is this a theoretical discussion with no practical application? No. Many Internet citizens still browse with text-only browsers. And as the technology continues to infiltrate other areas (e.g., pagers, cell phones, PDAs), consistent understanding and interpretation of tagging conventions is important. By thinking at a more abstract, general level (e.g., emphasized rather than italic), page designers will better be able to serve a wider audience.

At the bottom of what I dislike about HTML is that it was not designed with a broad set of capabilities and long-term interests in mind. Rather it was a hack thrown together to prove a concept. The creators then lost control, and market evolution took over. Long term, that's probably best. But short term, it makes life difficult for end users, page developers, browser vendors, and new technologies, such as alphanumeric pagers. PostScript, though proprietary, was designed with a full set of capabilities. It has not shown the need to evolve every few months. But that's moot, because HTML is the standard for the Internet. How long will it be before we see HTML-based laser printers?

Delphi Tip

Delphi is a Pascal-based visual development environment for Windows 32 (Win95 and NT). I compared it in some depth with MS Visual Basic in last month's column. Delphi can also be used to create traditional command-line utilities, although Borland has certainly deemphasized that capability, and has hardly documented how to do it.

Listing 1 shows a shell for such an application. The key is line 2, which tells the compiler that this is to be a console app, not a GUI app. To compile the program, use DCC32.EXE, which is located in Delphi's \.BIN directory. Also, the compiler must be able to find SYSTEM.DCU, which is located in the \.LIB directory. To do some really retro non-GUI command-line based development, all you need is the compiler, the system unit, and your favorite text editor. It'll all actually fit on a floppy disk with plenty of room to spare!

That's all for now. Until we meet again next time, you can stay in touch via jkh@acm.org.

EN

USING THE 7107

(Continued from page 60)

Hz. While it is not well-suited for frequency counters, it is an excellent choice for automobile tachometers, audio-frequency meters, pulse- and function-generator displays, and other such applications. The 2917 interfaces directly with the 7107, but might require a simple op-amp buffer at the input. If the output is erratic, a 0.1- μ F Mylar capacitor connected in series with the positive input will usually correct the problem.

For frequency counting, the LM555 timer is a better choice, as that chip will handle higher frequencies. Figure 12 is the schematic for a 555 frequency-to-voltage converter that can display up to a maximum of 1.999 MHz. The 100,000-ohm potentiometer (R4) functions as calibration, and S1 selects one of three resistors that determines range.

The display reading is multiplied by 10 for range 1, 100 for range 2, and 1,000 for range 3. A 1999 reading in range 2 would be equivalent to an input frequency of 199,900 Hz. A display of 0865 in range 3 would represent 865,000 Hz.

The range of the counter can be further expanded through the use of input pre-scalers. Those ICs will divide an input frequency, usually by 10, before applying it to the counter. A single pre-scaler would increase the input capability to 19,990,000 Hz, while cascading two pre-scalers would take it up to 199,900,000 Hz. Again, there is the multiplication factor to consider. When using pre-scalers, the displayed value is multiplied first by the range factor, then by the pre-scale factor to get the actual measurements.

The 11C90 and 95H90 ICs are two common pre-scalers, but the drawback with them is their expense. Those chips are not exactly economical, although the 95H90 can sometimes be found on the surplus market for as little as \$6 to \$10.

Other applications. Now that you're an expert on the 7107, the knowledge gained will perhaps prompt you to expand projects, designs, or equipment, and possibly inspire ideas for future projects. LED and LCD displays are highly informative, and can add

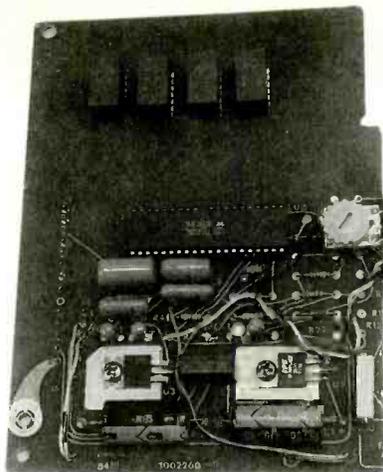


Fig. 13. A section of an alarm board, bought through surplus, that contains a 7107. This particular board also contains the ± 5 -volt power supply.

to the functionality of many types of electronic equipment. A project that takes advantage of the 7107's voltage-measuring capabilities is the author's "Versatile Power Supply" article in the December, 1995 issue of **Electronics Now**. That project is a bench-type power supply with a 7107-driven LED readout that displays the level of the output voltage.

Only a few applications were covered in this article. With a little thought or as practical needs arise, many other ideas will present themselves. For example, the Intersil data book illustrates a circuit for a digital torque meter, using a resistance-dependent strain gauge.

One area to watch for an economical source of devices is the surplus market, as the 7107 and 7106 can be found on many circuit boards. The surplus circuit board in Fig. 13 is an example of that type of source. The chip is usually mounted in a socket, and can be removed for use in one of your own projects. Frequently, the basic meter circuit is intact, and can be used as is with minor modifications. The 7107 can be found in some alarms, satellite receivers, antenna-positioning units, salvaged digital panel meters, counters, controllers, and a variety of other equipment. Be sure and keep an eye out for them when surplus "bargains" are advertised.

So, pick up a couple of 7107s and try adding one to your next project. The chip is quite easy to work with, and the results you could achieve can be very gratifying. Ω

MILLI-OHM ADAPTER

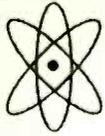
(Continued from page 42)

Run a wire directly from the ground connection of C1 on the board to a lug on the 10-32 stud supporting the swing arm. The common connection including C10, C11, C12, R9, and J1 is the negative Kelvin lead, which is *not* to be connected to ground on the board. Connect the Kelvin lead in this fashion: Run an insulated lead from the common connection of C10, C11, and C12 through a grommet located in the top of the cabinet near the stud, then through an "eyelet" located on the stud itself, and finally make the connection to the lug on BP2.

Mount the completed board on a pair of 1/2-inch spacers in the bottom of the cabinet and connect the remainder of the panel components to the board. Install the ICs in their sockets and close the cabinet. Prepare an output cable using a twisted pair of wires (do *not* use coaxial cable) with an RCA phono plug on one end, and a suitable plug for your DVM on the other end. A 12-inch length is sufficient.

Calibration. Power up the adapter and allow it to warm up for about five minutes, allowing the temperature to stabilize in the cabinet. Connect the adapter to your DVM, open the cabinet, and connect a clip-lead jumper from the base lead of Q1 to its emitter lead. The resulting voltage, which can now be read on your DVM, is the *offset voltage* of IC3; make a note of that voltage, which can be anywhere from 0 volt to ± 10 millivolts. Remove the clip lead. Using your DMM, measure the exact value of R_C (4.02 ohm, 1%), minus your test lead resistance. Connect R_C to BP1 and BP2, push the TEST switch, S1, and adjust CAL potentiometer R4 so that the output from J1 (about 4.02 volts) indicates the exact value of R_C added to IC3's offset voltage. Re-assemble the cabinet and the milli-ohm adapter is complete and ready for use.

In actual use, connect the unknown resistance (R_x) at the exact points on its leads from which you want to measure, take the reading, and *subtract* IC3's offset voltage for the proper value at 1 ohm/volt. That procedure will ensure the best possible accuracy. Ω



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LASER SCANNER ASSEMBLY \$29.⁰⁰

Assembly intended for a laser printer. Includes laser diode, polygon motor (6 sided) and misc. optics and lenses.

LASER DIODE (5mW) with collimator \$20.⁰⁰

VISIBLE LASER DIODE: 5mw at 670nm \$15.⁰⁰

Index guided. Threshold current 40 ma typical.

POLYGON MOTOR UNIT & DRIVER \$79.⁰⁰

Ten-sided first surface mirror mounted on an armature that spins at 125 revolutions per second yielding a beam sweep rate of 1250 sweeps per second. The driver for the polygon unit requires 24 volts and minus 12 volts to operate. There is also an f-beta lens in front of the polygon scanning mechanism with a three inch diameter. Great for optical experiments, etc. Very high quality units. (MFR: JAPAN ELECTRONICS)

NETWORK

Proton ProNet-4 Model p1347 Token Ring Board \$49.⁰⁰

16 bit • 4 Mbps • IEEE 802.2 and 802.5 compatible • twisted pair • interoperable with IBM Token Ring network

POS & BAR CODE

MAGNETIC CARD READER \$25.⁰⁰

Includes: • 20 character dot matrix display with full alpha-numeric capability • keypad with full alpha-numeric entry • separate 7.5 VDC/0.5 Amp power supply • standard telephone interface extension cord • lithium battery and flat-cone speaker.

HP bar code wand (HBCS 2300).....\$25.00

POWER SUPPLYS

SWITCHING POWER SUPPLYS \$12.00 or 2 for \$20.00 115/230 Volts

73 WATT (2) 4 pin power connectors attached • Dim: 8.5" L x 4.5" W x 2" H

Output: +5V @ 2-9.75 A, +12V @ 0-1.5 A, -5V @ 0-0.4 A, -12V @ 0-0.5 A

68 WATT Dim: 5.5" L x 3.2" W x 1.7" H • Output: 5V @ 4 A, 12V @ 4A

60 WATT Dim: 8 1/2 x 4 1/2 x 3 • Output: 5V @ 6A + 12V @ 1A - 5V @ 1A - 12V @ 1A

CHARGE COUPLED DEVICES



"The Spy In The Sky" \$29.⁰⁰

MATRIX TYPE

Sony CCD Imager - designed for black and white composite video cameras. Picture elements: 384 (H) x 491 (V)
Chip size 10.7 (H) x 9.3 (V) mm² • Unit cell size 23.0 (H) x 13.4 (V) um².
Ceramic 24 pin DIP package • Mfr: Sony, Part# O16AL

4096 element CCD \$19.00

1024 element CCD \$15.00

2048 element CCD \$15.00 • 1728 element CCD \$15.00

LINEAR TYPE

23605 Telo Ave., Torrance, CA 90505

Order desk only: USA: (800) 872-8878 CA: (800) 223-9977

L.A. & Technical Info: (310) 784-5488 Fax: (310) 784-7590

OEM INQUIRIES WELCOME

MONITORS

Non-Enclosed TTL

Comes with pinout. 12V at 1.4 Amp input • Horizontal frequency 15KHz. • Ability to do 40 and 80 column.

5 inch Amber \$29.00 • 7 inch Amber \$39.00

9 inch Amber or Green \$29.95

5" COLOR MONITOR \$49.⁰⁰

• Flat Faceplate • 320 x 200 Dot Resolution • CGA & Hercules Compatible

• 12 VDC Operation • 15.75 KHz Horiz. Freq. • 60 Hz Vert. Sync. Freq.

• Open Frame Construction • Standard Interface Connector • Degaussing Coil included • Mfr. Samtron



MISCELLANEOUS

ADAPTEC 4070A (RLL) OR 4000A (MFM), SCSI Controller, your choice \$25.⁰⁰

IBM 370 option XT and AT emulation boards \$35.⁰⁰

HACKER CORNER

POINT OF SALE BANK TERMINAL \$49.⁰⁰ or 2 for \$89.⁰⁰

• LCD Display 20 Char. x 4 Line • Printer 16 Column Dot Matrix • Epson • 24 Key Domed Membrane

Keypad • Intel 80C32 Processor • 2 PCMCIA Sockets (ICC Slots) • Dallas DS1287 Realtime Clock •

2 Solid State Buzzers (Piezo Electric) • 4 Crystals • Rockwell Modem Chip • Telephone Line Interface

(4 Pin "RJ" Connector) • RS-232 Interface (8 Pin "RJ" Connector) • NI-CAD Battery Pack Inside

Note: We have not been able to bypass an access code in the software. Thus, while time of day and other

introductory things are displayed on LCD, the full original capabilities of this unit cannot be guaranteed. Also,

we do not have a source for the smart cards that were to go in the PCM CIA sockets. Requires 12 volt adapter

for power. (Not included) Dimensions: 9-1/2 L x 6-1/4 W x 2-1/2 D • Original cost over \$450.00

CAMERA BLOCK \$149.⁰⁰

FOR ROBOTICS AND EVERYTHING ELSE

Unit is for Hi Band 8mm CamCorders, includes 8X zoom lenses, D/D converters, built-in CCD

2/3 in. 420 thousand picture elements, complementary mosaic filters. Excellent performance.

High resolution, high sensitivity, low lag, low smear, good color reproduction, no distortion,

1/60-1/10000sec variable speed digital shutters, TTL auto focus, auto white balance, one-push

auto white balance, auto/manual iris and gain up switch. Can be controlled by a 4bit micro

computer. Remote controlling is possible for zoom and focusing. NOTE: These are PAL

(European Standard) Units. SONY PART #EVI-101 (PAL)

CELL SITE TRANSCEIVER \$79.⁰⁰ 2 for \$149.⁰⁰

These transceivers were designed for operation in an AMPS (Advanced Mobile Phone Service) cell site. The

20 MHz bandwidth of the transceiver allows it to operate on all 666 channels allocated. The transmit

channels are 870.030-889.980 MHz with the receive channels 45 MHz below those frequencies. A digital

synthesizer is utilized to generate the selected frequency. Each unit contains two independent receivers to

demodulate voice and data with a Receive Signal Strength Indicator (RSSI) circuit to select the one with the

best signal strength. The transmitter provides a 1.5 watt modulated signal to drive an external power

amplifier. channel selection is accomplished with a 10 bit binary input via a connector on the back panel.

Other interface requirements for operation are 26 VDC (unregulated) and an 18.990 MHz reference

frequency for the digital synthesizer. The units contain independent boards for receivers, exciter, synthesizer,

tunable front end, and interface assembly (which includes power supplies and voltage-controlled oscillator).

Service manual, schematics and circuit descriptions included.

Encased Black & White Composite CCD Camera with Adapter

IR viewing to 1000 nm 7 1/2 L x 2 1/2 W x 1 1/2 H

Comes complete with CCD camera, mounting nut on bottom of casing, \$89.00

12VDC power supply. Excellent low light capability, standard RCA NTSC video out.

Great for: entryway security/remote monitoring, 2 for \$159.00

video conferencing/desktop video conferencing

This miniature camera is perfect for multimedia computer applications as well as security and

surveillance. NTSC output allows use with all popular video digitizing boards for Apple

Macintosh and Microsoft video for Windows. Connects directly to any composite monitor or

VCR with "video" input. Its razor-sharp wide-angle lens focuses from two inches to infinity and

its state-of-the-art CCD technology accurately captures 16 level grayscale images for Quick

Time movies and still pictures. Records at 30 frames per second and 260 lines resolution with

excellent low light capability. Uses 12VDC (adapter supplied) and standard RCA video cable.

Portable Micro Terminal \$99.⁰⁰ or 2 for \$149.⁰⁰

Flip up LCD display (9-16 VDC) • Can communicate with any computer having RS 232 port • Can communicate

with another Microterminal • Easy to use clear view numeric keypad • On-board microprocessor, data RAM (32K)

and Video RAM (64K) • 16 character alphanumeric keys and set up capabilities • Original intention for POS

applications • display size 4016 (256 x 128 pixels) Dimensions: 6.3" W, 11" L, 7" H. (With LCD up height is 7.1")



BAREBONES 286-12 COMPUTER \$49.00 (2 FOR \$79.00)

Slimline desktop case, 100 watt supply, math co-processor support. On board IDE, & Floppy controllers. 2

COM ports and 1 parallel port with software setup. Supports up to 8 Megs using standard 30 PIN SIMMs.

Internal room for (1) 3 1/2 inch IDE hard drive and (2) 3 1/2 inch floppies. Four 16 BIT ISA slots, accepts

full length AT size cards. Keyboard can be set to no test at boot. Case size is 15.5" W x 16" D x 4" H.

(Motherboard can be purchased separately: \$29.00 or 2 for \$49.00)

.6" COMPOSITE MINIATURE COLOR DISPLAY \$149.⁰⁰

Fully encased. Dim: 1.3" x 1.3" x 4". 12 Volts DC power. NTSC signal.

250 H x 300 V resolution. Focus adjustable eyepiece. Applications include camcorder

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**HOT
NEW
ITEM!**



#EN-219-055 **\$12⁹⁰**

Cable TV Stereo Decoder

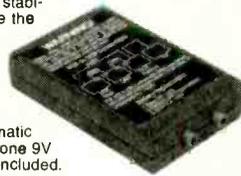
When used in conjunction with a cable TV converter or cable ready VCR, this handy device allows you to get the cable TV stereo signal into your home sound system for superb audio reproduction of your favorite shows, movies, and sporting events.



#EN-189-110 **\$19⁹⁰**

Digital Video Stabilizer

The digital video stabilizer will eliminate the constant picture distortion caused by the copyright protection on movie videotapes. This unit is fully automatic and operates on one 9V battery which is included.

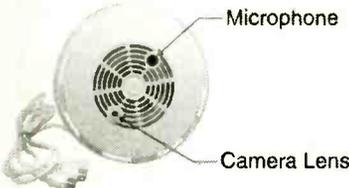


#EN-180-320 **\$17⁹⁵**

Decoy Cameras

These 1/3" CCD cameras offer a clever means of disguise. Both feature a 3.6mm wide angle lens, built-in electronic shutter, and a 12 VDC power supply. Minimum illumination: 0.3 lux. 400 line resolution. Smoke detector decoy camera includes an audio output.

**AFFORDABLE
HIGH TECH
SURVEILLANCE!**



Part #	Description	Price
EN-335-535	Smoke detector decoy	\$249.50
EN-335-540	Decoy clock camera	299.95



**"The Sound Bridge"
FM Stereo Wireless Transmitter**

The Sound Bridge is a mini FM wireless transmitter that can be used to broadcast stereo sound from any audio source like portable CD players, TVs, electronic games, CD-ROM, even computer soundcards, to your home stereo receiver! Adjustable from 89 to 95.5 MHz.



**HOT
NEW
ITEM!**

#EN-249-220 **\$14⁹⁵**

**Portasol/Weller Butane
Soldering Tool**

**NO CORDS,
NO BATTERIES!**



This cordless, refillable, butane powered soldering tool is ideal for any on-site soldering job. Provides up to 35 watts with a temperature range up to 700 degrees F. Includes flint igniter in plastic case, safety cut off switch, and C-2 chisel tip.

#EN-372-150 **\$25⁹⁵**

**150 MHz Oscilloscope Probe
Kit**

Deluxe probe kit features a modular design for longer life, switchable 10:1 probe with 150 MHz bandwidth, 2.8 ns rise time, and adjustable capacitance from 10-35 pF. 60" in length.

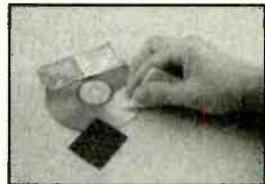


**GREAT
VALUE!**

#EN-390-100 **\$29⁹⁵**

**Memorex CD Repair And
Maintenance Kit**

Don't throw away expensive CDs because of annoying mistracking and skipping errors! The Memorex CD Repair kit contains enough solution and materials to clean and repair 12 compact discs.



#EN-249-032 **\$1⁹⁵**

5" Sealed Back Midrange

5" heavy duty sealed back midrange with deluxe mesh grill. 1" aluminum voice coil. Popular midrange for auto sound installations. ♦Power handling: 35 watts RMS/50 watts max ♦Voice coil diameter: 1 inch ♦Impedance: 8 ohms ♦Frequency response: 800-10,000 Hz.



#EN-280-030 **\$7⁵⁰**

3 Channel Color Organ Kit

This sound to light unit features three separate outputs, which can be controlled independently. Each output reacts to three different bands of the musical spectrum: bass, midrange, and treble. Has built-in microphone, so no connection is required to music source, but a line input is provided.



**SUPER
QUALITY
KIT!**

#EN-320-210 **\$59⁹⁵**

1", Titanium Dome Tweeter

Features a ferro fluid cooled Kapton voice coil and a rubber surround. Very natural sounding high frequency reproduction with extended response to 30KHz. ♦Power handling: 50 watts RMS/75 watts max ♦Voice coil diameter: 1" ♦Impedance: 8 ohms ♦Frequency response: 2500-30,000 Hz.



**RESPONSE
TO 30KHz!**

Dayton Loudspeaker Co.®

#EN-275-050 **\$16⁵⁰**

6-1/2" Woofer

Polymer resin treated paper cone with poly foam surround. Long throw voice coil design helps to deliver powerful bass output. Perfect for bookshelf type speakers. Mfg. #C16L020-51F. ♦Power handling: 60 watts RMS/120 watts max. ♦Voice coil diameter: 1-1/4 inches ♦Impedance: 8 ohms ♦Frequency response: 57-7000 Hz.



PIONEER

#EN-290-023 **\$19⁹⁵**



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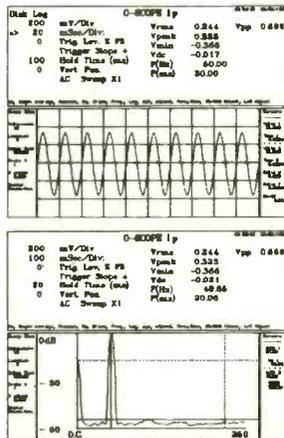
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Describes in detail how Pagers work, different types and uses, frequencies, advantages over and uses with cell-phones, and tips and tricks. And how Pagers are hacked and countermeasures. Includes the plans for your own Personal Pocket Paging System (transmitter and receiver) \$49

HACKING FAX MACHINES

Describes in detail how Fax machines are hacked and countermeasures (hacking Faxes is much more complex than just connecting a third Fax to the phone line). Includes Fax protocols, commo parameters, and 2- and 4:1 compression. And insights into designing Fax interception devices and modifying existing Faxes into Stealth Faxes do the job. \$49.

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How Voice Mail Box (VMB) systems are used and the specific ways they are hacked. Includes ASPEN, MESSAGE CENTER, BIX, GENESIS, EZ, SYDNEY, PHDNE, MAIL, AUDIX, CINDY, CENTAGRAM, SPERRY LINK, RSVP, etc. Absolutely required for all users, sysops and security personnel! \$29.

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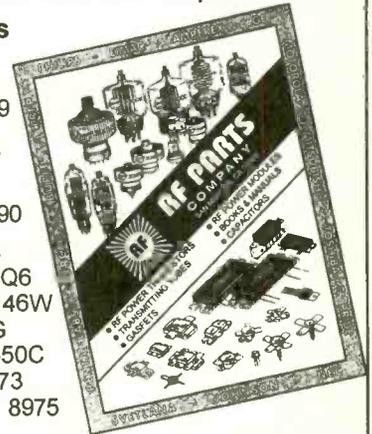
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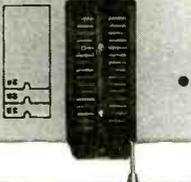
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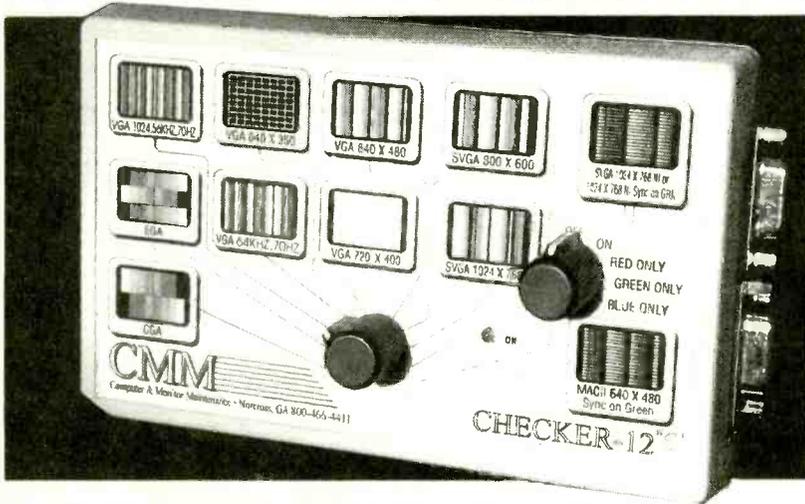
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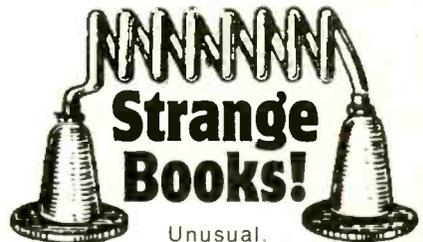


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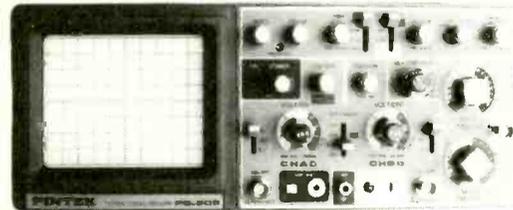
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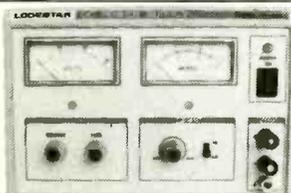


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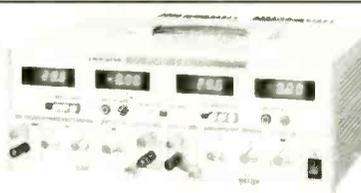
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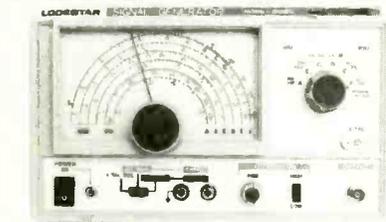
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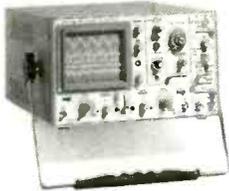
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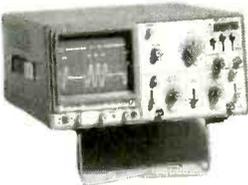
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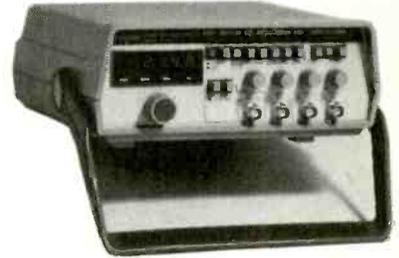
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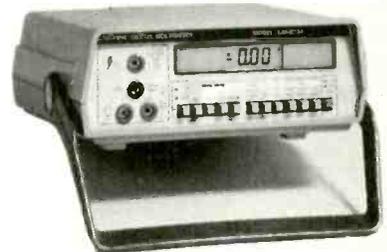
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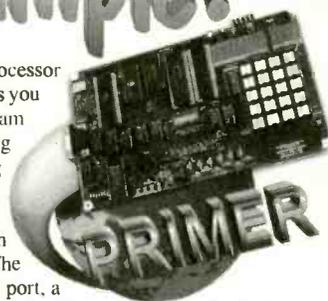


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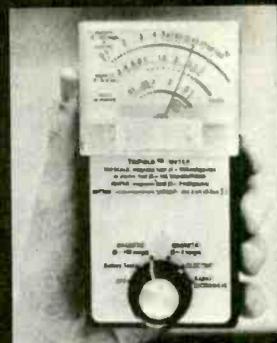
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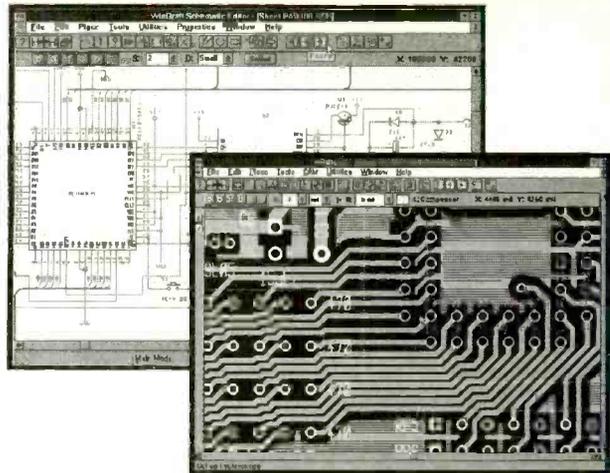
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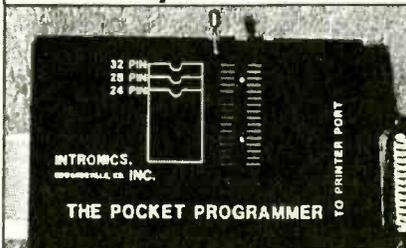
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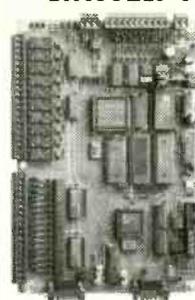
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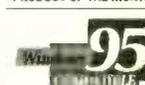


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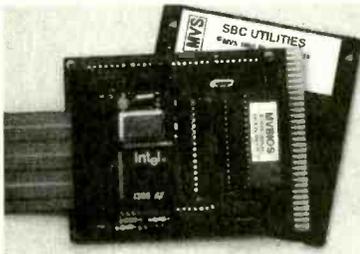
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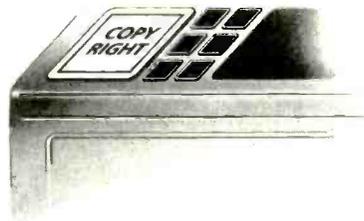


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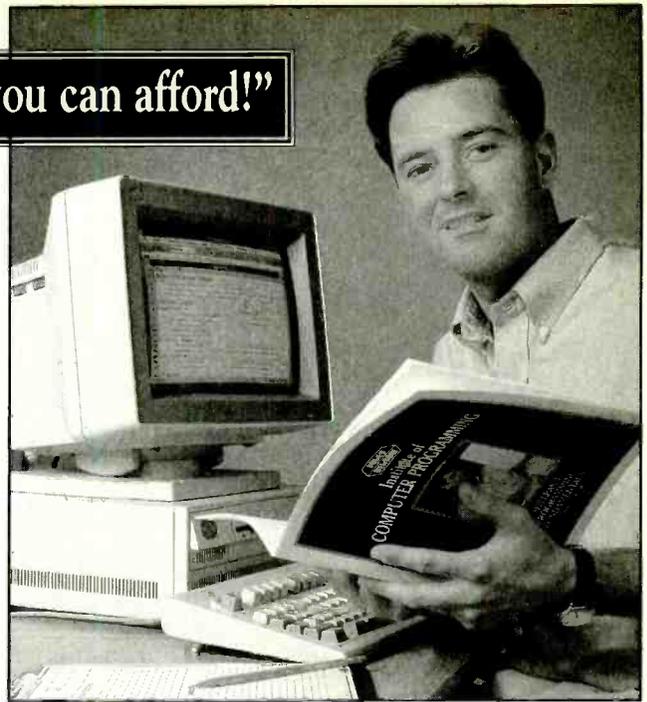
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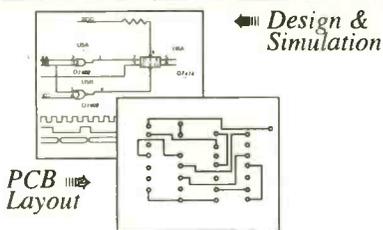
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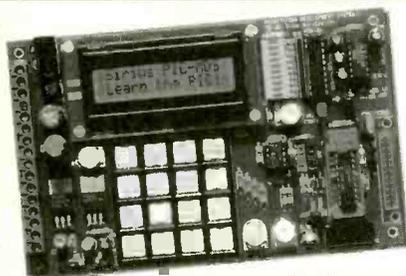
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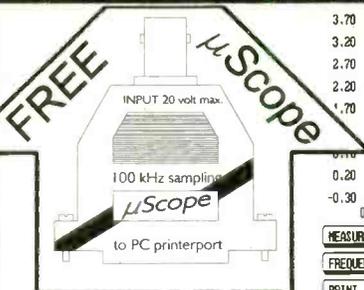
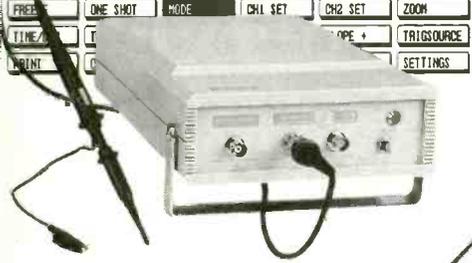
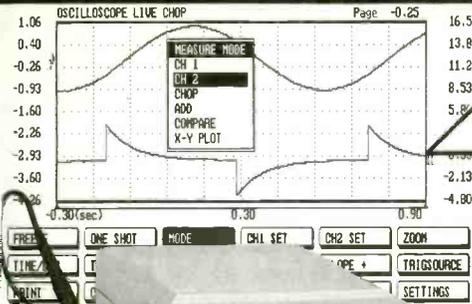


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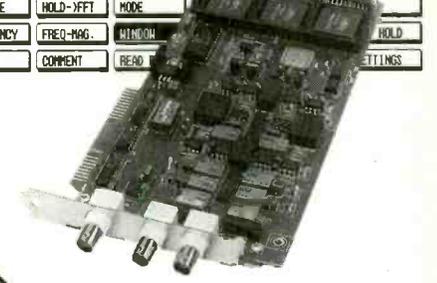
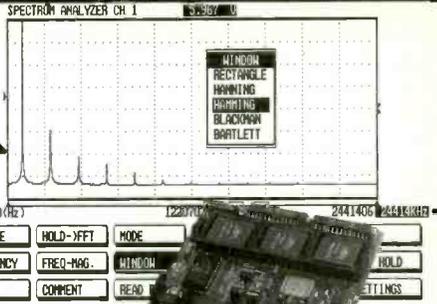
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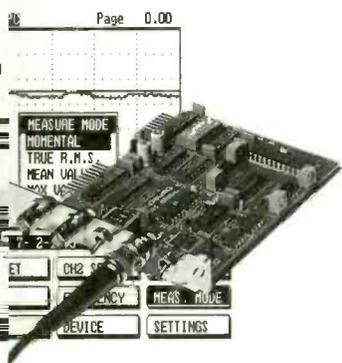
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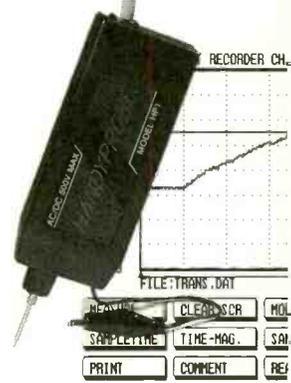
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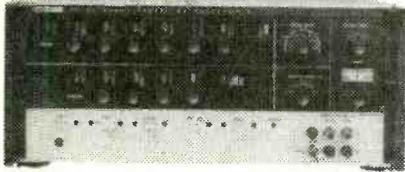
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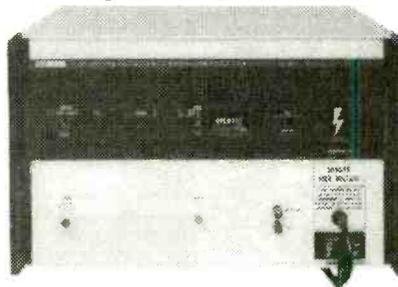
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Variable Resistor, 6 decades, 11,111,100 Ω , 10 M Ω max in .01 Ω steps.

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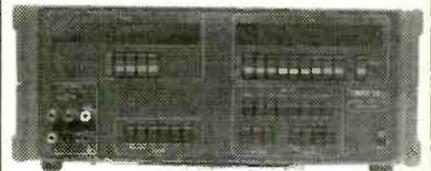
Voltmeter/ Null Detector, high input impedance, 1 μ V to 1000V in 19 ranges, input resistance 100 M Ω on 300 mV and above, 10 M Ω on 100 mV and below.

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Display: 3-1/2 Digit LCD, 21mm Figure Height with Automatic Polarity
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Temperature for Guaranteed Accuracy: 23°C±5°C RH<75%
Temperature Ranges:
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Storage: -10°C to 50°C (14°F to 122°F)
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200mV 100µV
2000mV 1mV ±(1%rdg+2dpts)
20V 10mV
200V 100mV
1000V 1V
Maximum Allowable Input: 1000V DC or Peak AC.

DC Current (DCA)

Range: Resolution: Accuracy:
200µA 100nA
2000µA 1µA ±(1.2%rdg+2dpts)
20mA 10µA
200mA 100µA
10A 10mA ±(1.2%rdg+2dpts)
Overload Protection: mA Input: 2A/250V fuse.

AC Voltage (ACV)

Range: Resolution: Accuracy:
200V 100mV ±(1.2%rdg+10dpts)
750V 1V

Frequency Range: 45Hz-450Hz
Maximum Allowable Input: 750V rms
Response: Average Responding. Calibrated in rms of a Sine Wave.

Resistance (Ω)

Range: Resolution: Accuracy:
200Ω 100mΩ
2000Ω 1Ω ±(1.2%rdg+2dpts)
20KΩ 10Ω
200KΩ 100Ω
2000KΩ 1KΩ
20MΩ 10KΩ ±(2%rdg+10dpts)
Maximum Open Circuit Voltage: 2.8V

Diode Test

Measures forward voltage drop of a semiconductor junction in mV test current of 1.5mA Max.

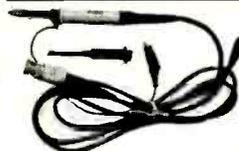
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Measures transistor hFE.

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9300G	Rugged High Quality DMM with Rubber Boot	\$19.00

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CAT NO	DESCRIPTION	1	10	100
HP-9060	Scope Probe Set DC~60MHz	\$16.49	\$14.49	\$11.58
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These pre-sensitized printed circuit boards are ideal for small production runs. They provide high resolution and excellent line width control. High sensitive positive resist coated on 1oz. copper foil allows you to go direct from your computer plot or art work layout. No need to reverse art.

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CAT NO	DESCRIPTION	PRICE EACH		
		1	10	50
PP101	100mm x 150mm/3.91" x 5.91"	\$2.55	\$1.90	\$1.70
PP114	114mm x 185mm/4.6" x 6.6"	2.98	2.45	1.98
PP152	150mm x 250mm/5.91" x 9.84"	5.40	3.98	3.60
PP153	150mm x 300mm/5.91" x 11.81"	6.15	4.48	4.10

Single-Sided, 1oz. Copper Foil on Fiberglass Substrate

CAT NO	DESCRIPTION	PRICE EACH		
		1	10	50
GS101	100mm x 150mm/3.91" x 5.91"	\$ 3.90	\$2.98	\$2.60
GS114	114mm x 185mm/4.6" x 6.6"	4.80	3.49	3.20
GS152	150mm x 250mm/5.91" x 9.84"	8.69	5.98	5.78
GS153	150mm x 300mm/5.91" x 11.81"	10.20	7.20	6.80

Double-Sided, 1oz. Copper Foil on Fiberglass Substrate

CAT NO	DESCRIPTION	PRICE EACH		
		1	10	50
GD101	100mm x 150mm/3.91" x 5.91"	\$ 5.07	\$3.68	\$3.38
GD114	114mm x 185mm/4.6" x 6.6"	5.95	4.29	3.99
GD152	150mm x 250mm/5.91" x 9.84"	10.47	7.39	6.98
GD153	150mm x 300mm/5.91" x 11.81"	11.95	8.69	8.30

Etching Chemicals/Ferric Chloride

A dry concentrate that mixes with water to make 1 pint of etchant, enough to etch 400 sq. inches of 1oz board.

CAT NO	DESCRIPTION	PRICE EACH	
		1	5
ER-3	Makes 1 pint	\$3.50	\$2.75



Developer This product is used as the developer on our positive photo-resist printed circuit boards. Includes instructions. 50 gram package, mixes with water.

CAT NO	DESCRIPTION	PRICE EACH		
		1	10	25
POSDEV	Positive Developer	\$.95	\$.80	\$.50



Etching Tank This handy etching system will handle PC boards up to 8" x 9", two at a time. Ideal for etching your PCB's! System includes an air pump for etchant agitation, a thermostatically controlled heater for keeping etchant at optimum temperature and a tank that holds 1.35 gallons of etchant. A tight fitting lid is also supplied to prevent evaporation when system is not being used. Typical etching time is reduced to 4 minutes on 1oz. copper board!

REDUCES ETCHING TIME!

CAT NO	DESCRIPTION	PRICE
12-700	Etch Tank System	\$37.95

Desoldering Pumps

These powerful plastic body desoldering pumps are designed for easy one hand operation for fast, efficient desoldering. Double O-ring piston seals for maximum suction.



CAT NO	DESCRIPTION	PRICE EACH		
		1	5	10
08-366S	Large Desoldering Pump	\$15.89	\$13.49	\$11.95
08-366E	Regular Desoldering Pump	10.89	8.59	7.39
08-366TIP	Replacement Tip	1.95	1.95	1.95

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Electronic Soldering System

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CAT NO	DESCRIPTION	PRICE EACH	
		1	5
SL10	Temp Controlled Soldering Iron	\$56.00	\$50.00
SL24V	Spare 24V Soldering Iron	10.50	7.50



Electronic Soldering System with LED Display

Deluxe temperature controlled system with LED display for maximum accuracy. Temperature is adjustable from 160°-480°C (320°-900°F). Iron heating power is 48 Watts. Runs on 24V from controller unit. Replacement irons and tips are available. Tip size is 5.3mm.

CAT NO	DESCRIPTION	PRICE EACH	
		1	5
SL30	Deluxe Soldering System w/LED	\$86.00	\$75.00
SL24V	Spare 24V Soldering Iron for SL10 or SL30	10.50	7.50



Replacement Tips for SL10/SL30

We now offer a variety of replacement tips for the SL10/SL30 soldering stations.



CAT NO	DESCRIPTION	PRICE EACH		CAT NO	DESCRIPTION	PRICE EACH	
		1	5			1	5
821	1/32" Pencil Tip	1.39	1.19	825	1/8" Chisel Tip	\$1.49	\$1.29
822	1/32" Pencil Tip	1.39	1.19	826	3/64" Chisel Tip	1.49	1.29
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Specifications

CAT NO	DIMENSIONS (MM)	RATED VOLTAGE (V)	START VOLTAGE (V)	INPUT CURRENT (A)	AIR FLOW (CFM)	STATIC PRESSURE (INCH-H ₂ O)	SPEED (RPM)	NOISE LEVEL (dB)	WEIGHT (g)
CSD 4010-12	40x40x10mm	12	7	0.06	5.1	0.19	5,500	26	20
CSD 6025-12	60x60x25mm	12	5	0.13	13.7	0.165	4,500	28	65
CSD 8025-12	80x80x25mm	12	5	0.16	37.8	0.177	3,000	31	80
CSD 9225-12	92x92x25mm	12	5	0.32	42	0.18	2,800	37	95
CSD 1225-12	120x120x25mm	12	5	0.35	62	0.180	2,500	42	135

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RH60-4	4.4-lb. Spool, .031", 60/40	24.00	21.90	17.92
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CAT NO	DESCRIPTION	PRICE EACH	
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CA-H34A	PCB Mounted IRCCD Camera	\$125.00	\$109.00

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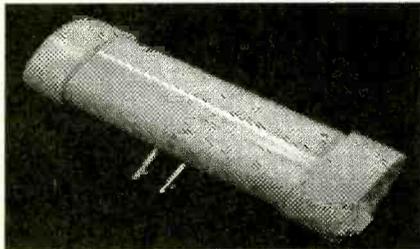
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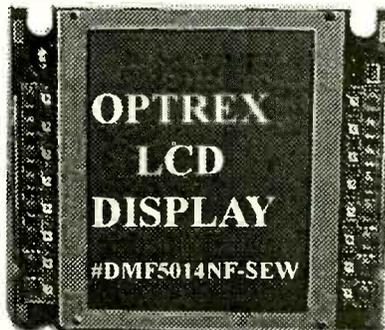
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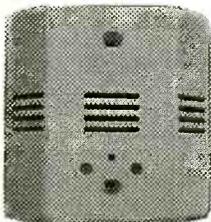
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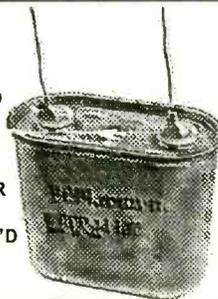


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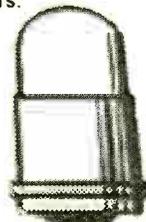
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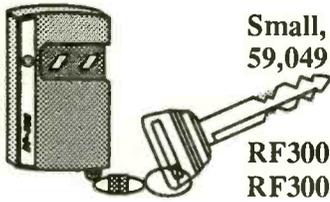
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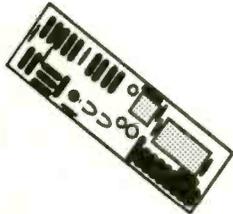
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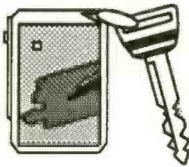
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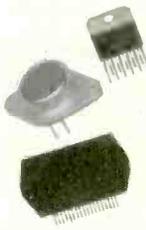


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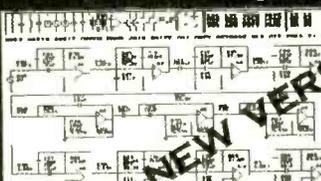
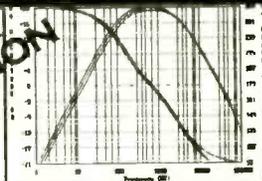
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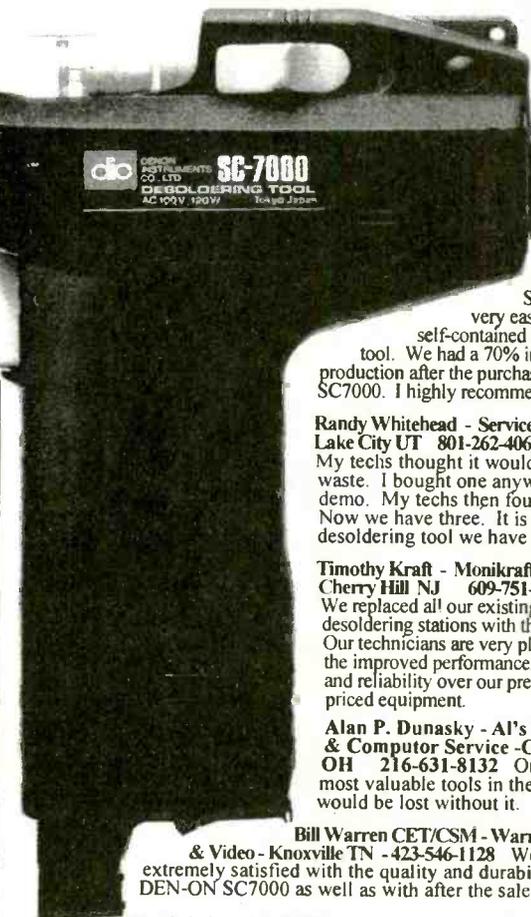
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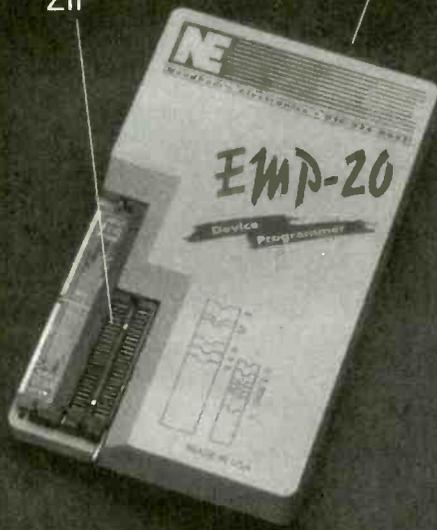
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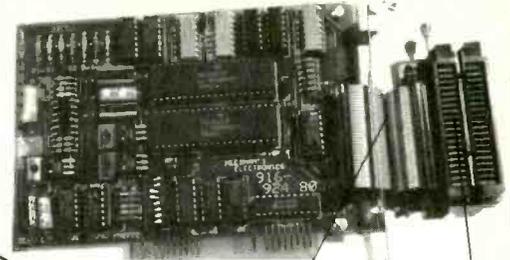
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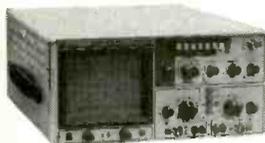
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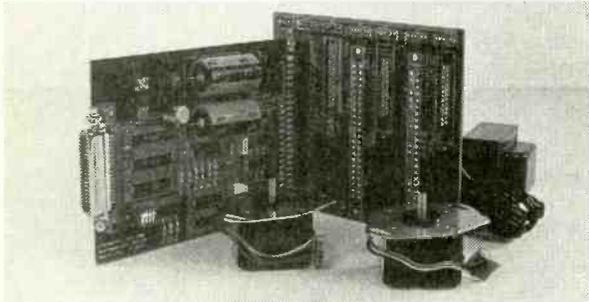
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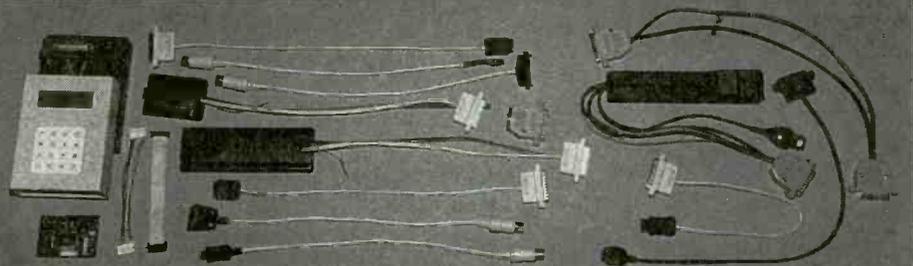
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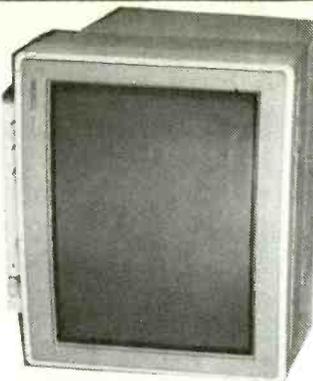
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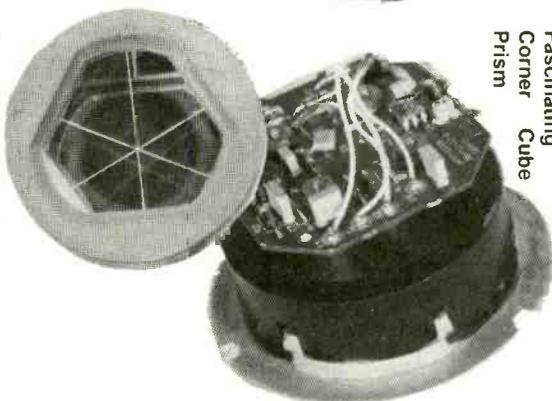
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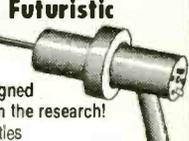
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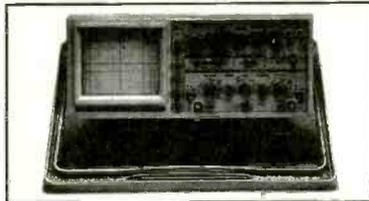
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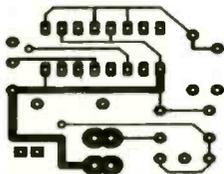
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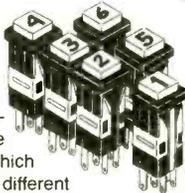
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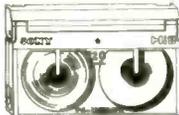
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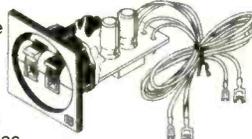
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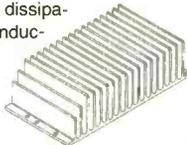


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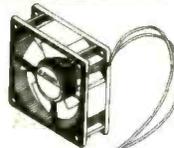
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center positive.

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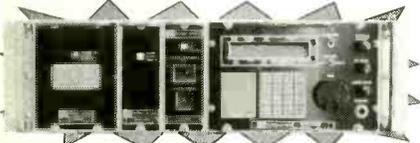
*****SHIPPING IS NOT INCLUDED IN THESE PRICES, PLEASE CALL FOR RATES*****



CUBIC COMMUNICATIONS DUAL VLF/HF RECEIVER

This High-Tech surveillance receiver features two fully independent high performance radios in one rack cabinet. Covers 5kHz-30MHz with a full compliment of filters incl. USB/LSB plus RS-232 remote control. The units we have in stock are in very nice condition.

Price: \$2395.00 ea.



WATKINS JOHNSON WJ-9040 SERIES RECEIVER

This awesome radio covers 200Hz-1400MHz in 13 bandwidths of AM, AM Slideback, FM, CW and SSB demodulation modes. Contains lots of features and you can bet this is a super-rare find in the used market. Price: \$5450.00 **CALL for DETAILS!!!**



HEWLETT PACKARD 8640B SIGNAL GENERATOR

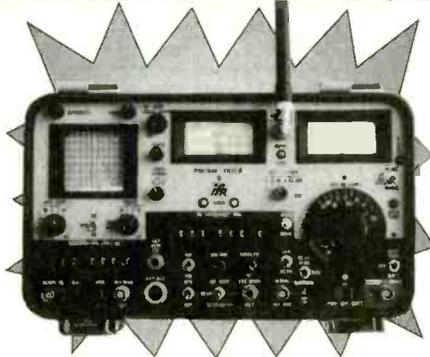
Industry Standard sig-gen 500KHz-512Mhz features internal phase lock/synchronizer and digital freq. readout. +19 to -145 dBm output. AM, FM, Ext and Pulse modulation.

Price: \$1695.00 OPT 001 add \$100.00
OPT 003 add \$150.00



HEWLETT PACKARD HP3312 SWEEP/FUNCTION GENERATOR

Well designed and easy to use, this function generator combines economy and quality in one compact unit. Freq range is 0.1Hz-13MHz output is 10.0VP-P into 50ohms. Sweep, CW, AM, FM, or tone burst. This unit features-sync. out, trig. phase, symmetry, offset and more. Price: \$935.00 ea. Fully checked.



IFR 1100S COMMUNICATIONS MONITOR

FM/AM-1100S is a synthesized AM/FM/SSB receiver/signal generator. Frequency range is 300KHz-1Ghz, it contains a 60 watt RF power meter, deviation/modulation meter, oscilloscope, spectrum analyzer, tone generator and internal high stability freq.-standard. It's a radio repair shop in one cabinet.

Price: \$4250.00 Fully Checked.

IFR 1000SA as above except without spectrum analyzer. Price: \$2750.00 Fully Checked.

-NEW IFR 1000 Instrument covers with sinad meter and scope probe (new unused). \$275.00

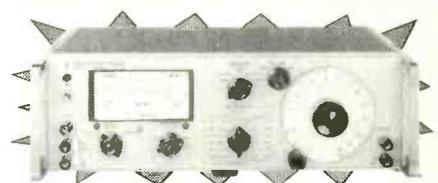


PRC 25 - MILITARY TACTICAL TRANSCEIVER

Fabulous quality and design are standard in this 30Mhz-75.95 Mhz tactical transceiver. Output power level from 1.1-2 watts 150Hz squelch. The units we just received are reconditioned (newly painted) ready for issue and include the battery box. Price: \$245.00

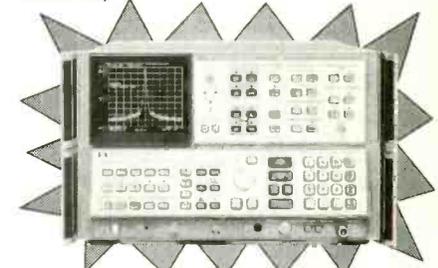
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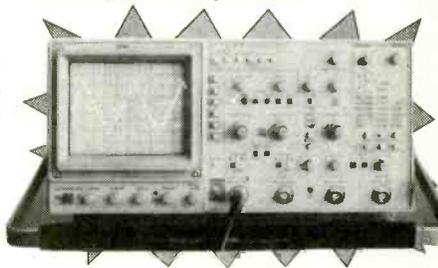
HEWLETT PACKARD HP 331A DISTORTION ANALYZER

Industry Standard unit covers 5Hz-600kHz & measures total harmonic distortion down to .1% full scale. We are blowing these out as-is, untested but, most we've shipped in the past have worked. Price: \$99.00 (units are scratched).



HEWLETT PACKARD 8568B SPECTRUM ANALYZER OPT-E96

This High Performance instrument features 3 Hz video bandwidth over the 1kHz - 1.5Ghz frequency range. Automatic zoom, signal track, multiple store/recall are only a few of the very powerful functions you will find coupled with a high performance synthesized LO and built in freq counter. Price: \$16995.00 Fully Checked

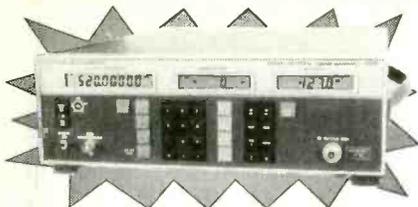


TEK 2246 OSCILLOSCOPE

This user friendly oscilloscope features, 100MHz bandwidth on four channels, on screen scale factors, versatile triggering, 2mV/Div vert sensitivity, delayed sweep, hands-off voltmeter and smart cursors.

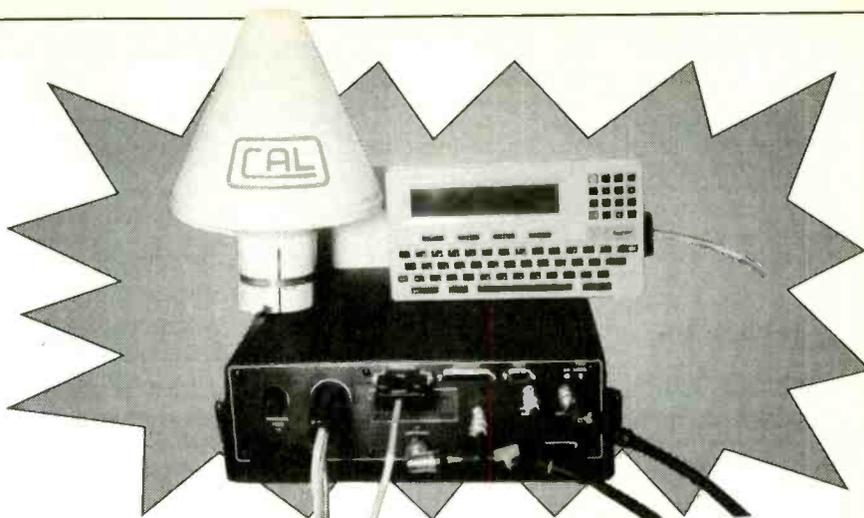
Looks very clean. Price: \$1950.00

(No catalog available yet!)



**MARCONI SYNTHESIZED
SIGNAL GENERATOR Model 2018**

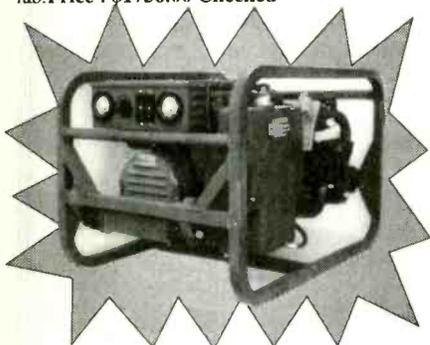
Freq range 80Khz-520Mhz with calibrated output levels from -127 dBm to +13dBm. Resolution 10Hz. It can be freq, phase or amplitude modulated from ext or int modulation sources. RF output resolution is 0.1dB, reversepower protection of up to 50W is possible without damage to the instrument. This instrument is microprocessor controlled and very easy to use, a must for any serious repair or development
lab.Price : \$1750.00 Checked



**"CAL" ASTRONAUTICS
MOBILE SATELITE
COMMUNICATIONS STATION**

This is a box chock full of "current" high-end communications technology. These units were designed so that mobile land based vehicles could keep in touch (via Geostationary Inmarsat satellite network) with home base using an intelligent data terminal. The terminal features a back-lit 4 line LCD display and illuminated keys; one of the transceiver's most impressive features is an "L" Band 1.2-1.55GHz 60 watt amplifier. The fabulous helix antenna (with LNA built-in) is an amazing design with all kinds of active and passive devices surface-mounted on to the antenna reflector. We consider this the "ultimate gadgeteers goodie pack" with all kinds of up-to-date RF satellite ground technology. These systems come complete in their original shipping container with all cables and mounting bracket. Best of all they operate on 12 VDC. Operators manual supplied (but, there isn't any subscriber data).

(NOT TESTED) IN GOOD CONDITION.....\$345.00



**MILITARY STANDARD D.C.
GENERATOR**

Superior QUALITY plus rugged design are features of this deluxe 2 cylinder 4 stroke gasoline generator. The control panel contains meters for voltage & current indication, main circuit breaker and voltage adjustment. Shielded wires and plugs comprise the RFI suppression ignition system eliminating most radio noise. These units are "new" in the original carton complete with operators manual and only require fuel and oil for operation; output voltage is adjustable approx. 10-32v (28v nom) @ 53.3A (1.5Kw) continuous duty load.

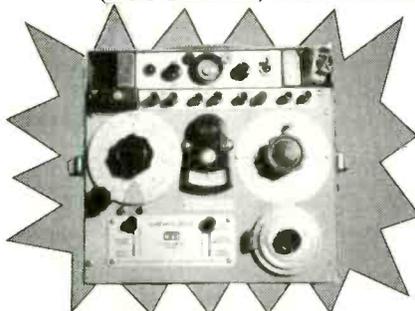
Price: \$379.00 New in Orig. Carton.

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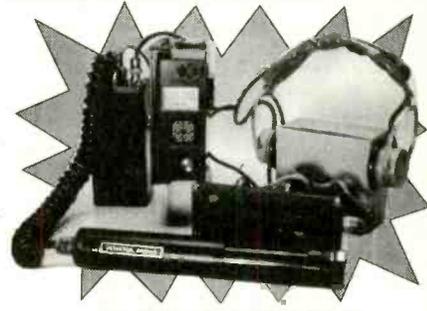
Great collectors item for the ham shack, fifties vintage func/chkd.



**ESI MODEL 250 DA
IMPEDANCE BRIDGE**

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Used, not functionally checked.....\$95.00
Functionally checked.....\$165.00



**PDR-63 PORTABLE
RADIAC METER**

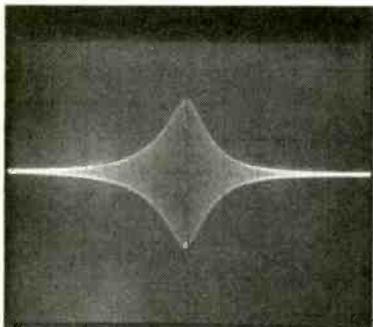
This portable radiac set is loaded with all kinds of extras featuring six ranges of sensitivity for both Gamma or Beta radiation measurements.

The 1st scale 0-1 rad/hr up to 0-5000 rad/hr. The unit comes supplied with headset & bat/charger. Req's only 4 AA Batteries. Price: \$149.95

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-ENI MOD 406L 150 KHz-250MHz @ 40db GAIN	-HP 8505 NETWORK ANALYZER SYSTEM	\$4,980.00	-GRT-22 UHF POWER AMPLIFIER	\$ 200.00
-FLUKE 5100A CALIBRATOR	-HP 8558B SPECTRUM ANALYZER 0.1-1.5GHz	\$2,350.00	-R392 RECEIVER 5-30MHz	\$ 165.00
-FLUKE 7261A FREQ. COUNTER 520MHz	-HP 8559A SPEC ANALYZER 0.1-22GHz	\$3,995.00	-TI95 100w COMPANION XMTR TO 392	\$ 85.00
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-GOULD RS 3800 PROGRAMABLE CHART RECORDER/w	80KHz - 520MHz	\$1,750.00	5KHz-30 MHz MIL-SPEC communications receiver	\$3,950.00
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-HP 204D LOW DIST. OSCILLATOR	-TEK 465 OPT 5 TV-TRIG	\$ 849.00	four stage compressor and 4 cyl wisconsin engine on a cart with	
-HP 3551A TRANSMISSION TEST SET	-TEK 465B 100mhz OSCILLOSCOPE	\$ 895.00	storage tanks and controls or electric version avail	\$3,500.00
-HP 3581A WAVE ANALYZER	-TEK 465M 100mhz OSCILLOSCOPE	\$ 695.00	-BAUER K14 3500 PSI COMPRESSOR SYSTEM same as above	
-HP 4260A LCR BRIDGE	-TEK 485 350 MHz OSCILLOSCOPE	\$ 1195.00	except uses briggs & straton 9hp motor	\$2,750.00

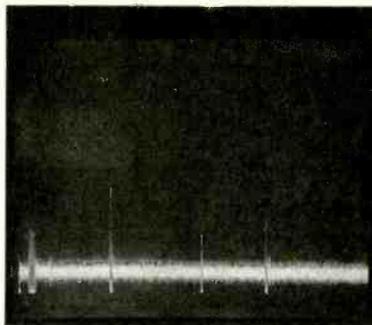
SPECTRUM ANALYZER

(Continued from page 52)



THE OSCILLOSCOPE'S VIEW of the bubble sampled from the preamplifier assembly's test point after the 145-MHz IF filter alignment. The oscilloscope's 10× time-base magnifier is switched on. You should be able to see the zero beat at the center of the bubble.

For example, EMI on cables might be best observed by passing the cable through a toroid ferrite. Wrap a few turns of finer wire as a secondary and



THE OSCILLOSCOPE'S DISPLAY of the HSA output when a short-wire antenna is connected to the BNC connector. The extreme left burst is an unknown signal. Local radio-control signals from left to right are at 27.995 MHz, 53.4 MHz, and 72.280 MHz.

connect to the HSA. This allows examination of what is on a suspect cable but avoids electrostatic pickup.

It is also possible to extend the reach of the HSA with a length of coax cable with a one or two turn sniffer loop on the pickup end. In all cases, be careful when working around

power lines or line-powered equipment.

Parts and Supplies Hints. All parts and supplies for the Hobby Spectrum Analyzer came from electronics parts mail-order suppliers listed in the sidebar and from local hardware, model hobby, craft, and RadioShack stores. No single parts source can supply everything needed. A very few parts such as slide switches and beads came only from Digi-Key. The NE602 IC came from Ocean State Electronics and DC Electronics. The MV209 varactor comes from DC Electronics or Hosfelt. Many catalogs list ceramic disc capacitors; however, the RadioShack capacitor assortment #272-806 has all the smaller picofarad values on the RF circuit module. Consider using cut-to-length plastic ball pen handles for spacers. Metal and plastic tubing of many sizes as well as brass, aluminum, tin plate, and copper sheet is available at model hobby shops. Ω

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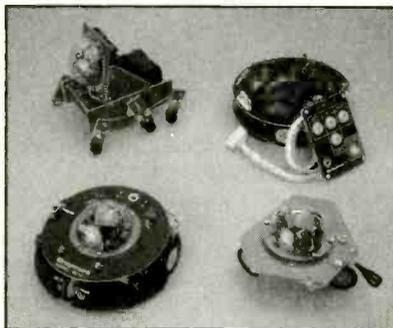
Robot This 6-legged Robot walks over rough terrain. High-tech infrared beam senses and avoids objects in its path. 32 page Book.

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HEWLETT-PACKARD 200CD OSCILLATOR, popular tube-type audio generator covers 5 Hz to 600 KHz in five bands; output 10 volts into 600 ohms or 20 V open circuit. Requires 115/230 VAC 50-400 Hz. 7"Wx10.8"Hx12.5"D, 20 lbs sh.

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TA-838/PT FIELD PHONE



MILITARY TELEPHONE has push-button numeric tone pad and is designed for 2- or 4-wire communications; replaces old EE-8 and TA-43/312 field phones. Ringing signal possible only in 4-wire hook-up. TA-838 can also be operated over standard telephone lines. Rugged thermoplastic construction; requires four C-cell batteries. 6.9.8x5, 8 lbs. sh

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Operators Manual \$10.00

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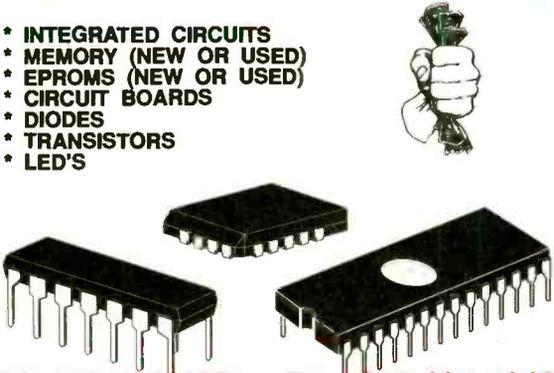
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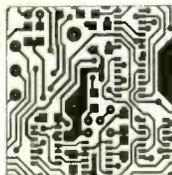
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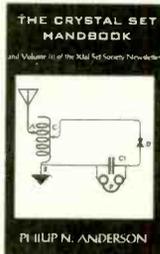
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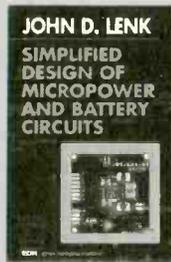
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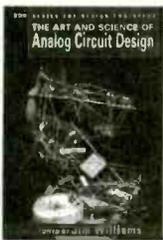


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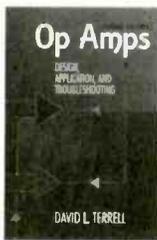


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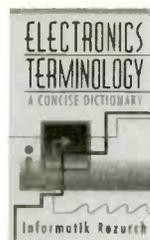
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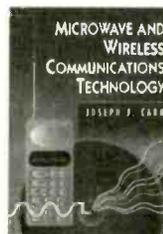
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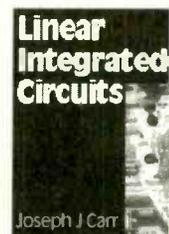
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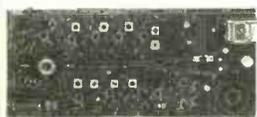
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Model	Bandwidth MHz								
S-1360	60	1mV/div	2	10ns/div	Yes	Yes	Yes	Yes	2
S-1345	40	1mV/div	2	10ns/div	Yes	Yes	Yes	Yes	2
S-1340	40	1mV/div	2	10ns/div	No	Yes	No	No	1
S-1330	25	1mV/div	2	10ns/div	Yes	Yes	Yes	Yes	2
S-1325	25	1mV/div	2	10ns/div	No	Yes	No	No	1
DIGITAL STORAGE		Analog Sen (max)	No. of Channels	Sampling Rate	Memory Channel	Internally Backed Up	Pretrigger %	Output	
Model	Bandwidth MHz								
DS-303	30	1mV/div	2	20MS/S	2K	Yes	0, 25, 50, 75	RS232	
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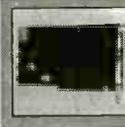
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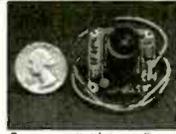
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Tone-Grabber Touch Tone Decoder / Reader



Diald phone numbers, repeater codes, control codes, anywhere touch tones are used, your TG-1 will decode and store any number it hears. A simple hook-up to any radio speaker or phone line is all that is required, and since the TG-1 uses a central office quality decoder and microprocessor, it will decode digits at virtually any speed! A 256 digit non-volatile memory stores numbers for 100 years - even with the power turned off, and an 8 digit LED display allows you to scroll through anywhere in memory. To make it easy to pick out numbers and codes, a dash is inserted between any group or set of numbers that were decoded more than 2 seconds apart. The TG-1 runs from any 7 to 15 volt DC power source and is both voltage regulated and crystal controlled for the ultimate in stability. For stand-alone use add our matching case set for a clean, professionally finished project. We have a TG-1 connected up here at the Ramsey factory on the FM radio. It's fun to see the phone numbers that are dialed on the morning radio show! Although the TG-1 requires less than an evening to assemble (and is fun to build, too!), we offer the TG-1 fully wired and tested in matching case for a special price.

TG-1, Tone Grabber Kit \$99.95
CTG, Matching Case Set for TG-1 Kit \$14.95
TG-1WT, Fully Wired Tone Grabber with Case \$149.95
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Mini-Peeper Micro Video Camera

Super small, high quality fully assembled B & W CCD TV camera the size of an ice cube! Provides excellent pictures in low light (2 lux), or use our IR-1 Infra-Red light source to invisibly illuminate an entire room on a pitch black night! Imagine the possibilities... build it into a smoke detector, wall clock, lamp, book, radio. Exact same camera that's in big buck detective catalogues and stores. Kit includes: fully assembled CCD camera module, connectors, interface PC board kit with proper voltage regulation and filtering, hook-up details, even a mini microphone for sensitive sound! Two models available: Wide Angle Lens 3.6mm/f2, adjustable focus lens, 92 degree view; Pinhole Lens 5.5mm/f4.5, 60 degree view. The Pinhole Lens is physically much flatter and provides even greater depth of focus. The camera itself is 1.2" square. The Wide Angle Lens is about 1" long. Pinhole Lens uses about 1/2", interface PC board is 1" x 2" and uses RCA jacks for easy hook-up to VCRs, TVs or cable runs. Power required is 9 to 14 VDC @ 150 mA. Resolution: 380 x 350 lines. Instruction manual contains ideas on mounting and disguising the Mini-Peeper along with info on adding one of our TV Transmitter kits (such as the MTV-7 unit below) for wireless transmission!

MP-1, Wide Angle Lens CCD TV Camera Outfit \$169.95
MP-1PH, Pin-Hole Lens CCD TV Camera Outfit \$189.95

MicroStation Synthesized UHF TV Transmitter



Now you can be in the same league as James Bond. This transmitter is so small that it can fit into a pack of cigarettes - even including a CCD TV camera and battery! Model airplane enthusiasts put the MTV-7A into airplanes for a dynamic view from the cockpit, and the MTV-7A is the transmitter of choice for balloon launches. Transmitter features synthesized, crystal controlled operation for drift-free transmission of both audio and video on your choice of frequencies: Standard UHF TV Channel 52 (which should only be used outside of the USA to avoid violating FCC rules), and 439.25 MHz or 911.25 MHz which are in the amateur ham bands. The 439.25 MHz unit has the nifty advantage of being able to be received on a regular 'table-ready' TV set tuned to Cable channel 68, or use our ATV-74 converter and receive it on regular TV channel 3. The 911.25 MHz unit is suited for applications where reception on a regular TV is not desired, an ATV-79 must be used for operation. The MTV-7A's output power is almost 100 mW, so transmitting range is pretty much 'line-of-sight' which can mean many miles! The MTV-7A accepts standard black and white or color video and has its own, on-board, sensitive electret microphone. The MTV-7A is available in kit form or fully wired and tested. Since the latest in SMT (Surface Mount Technology) is used to provide for the smallest possible size, the kit version is recommended for experienced builders only. Runs on 12 VDC @ 150 mA and includes a regulated power source for a CCD camera.

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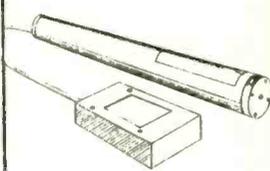
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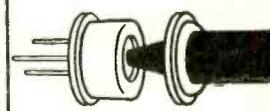
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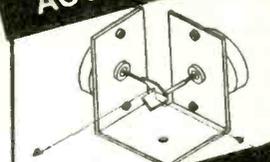
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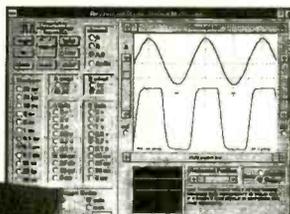
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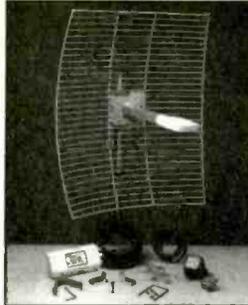
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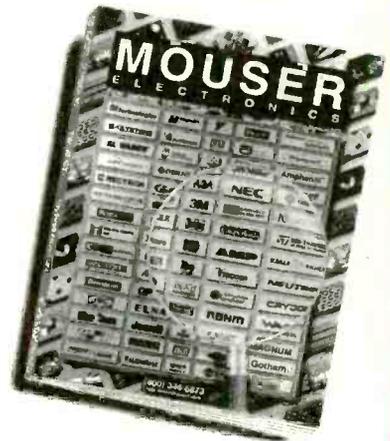
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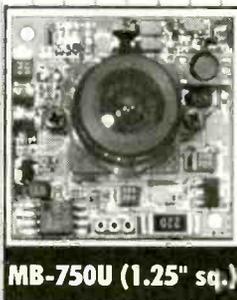
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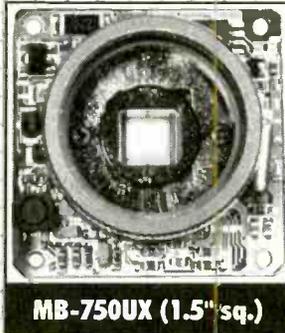
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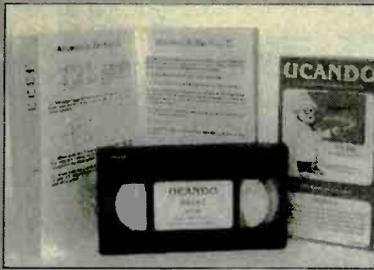
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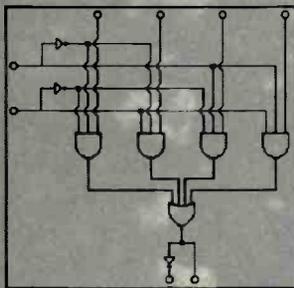
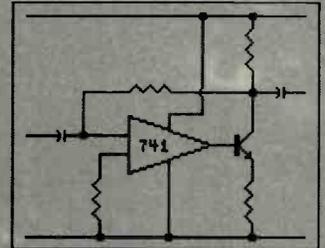
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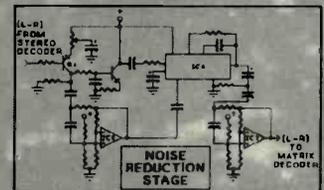


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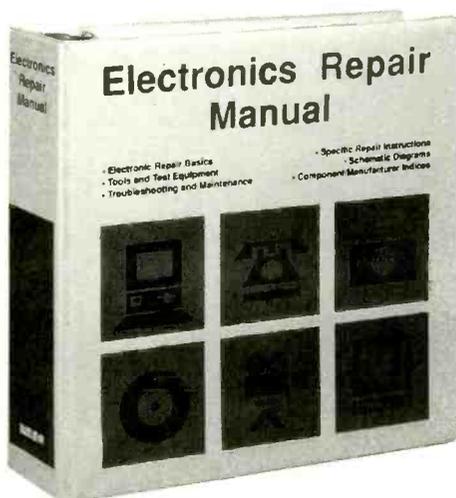


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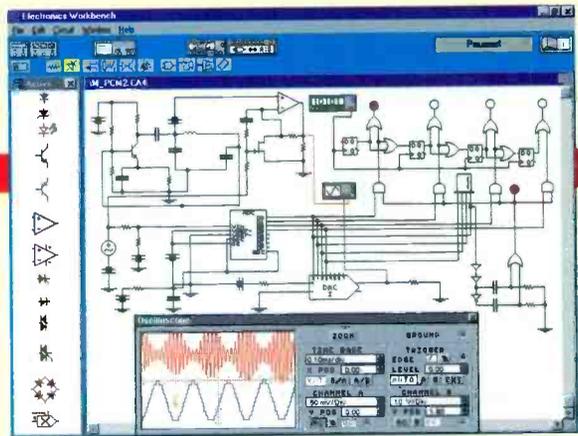
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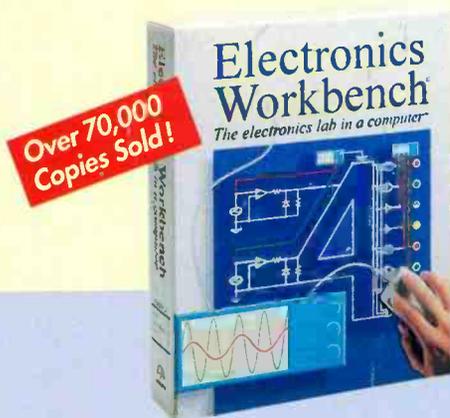
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